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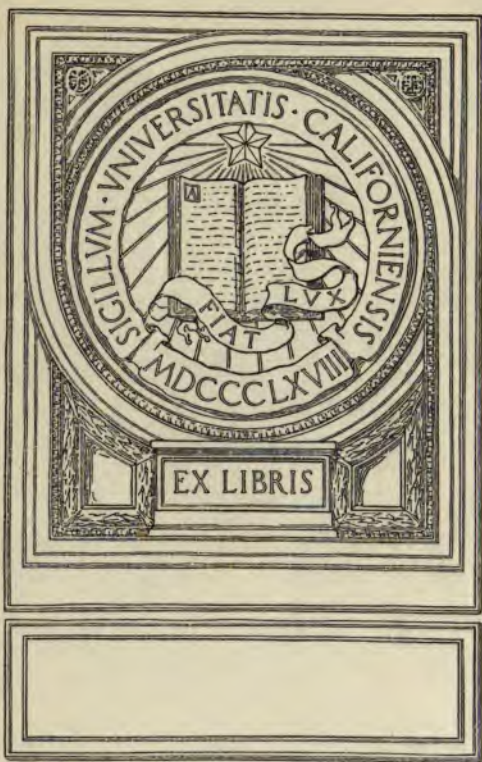
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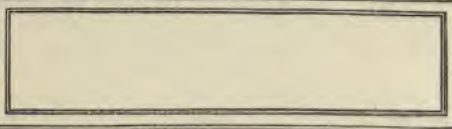
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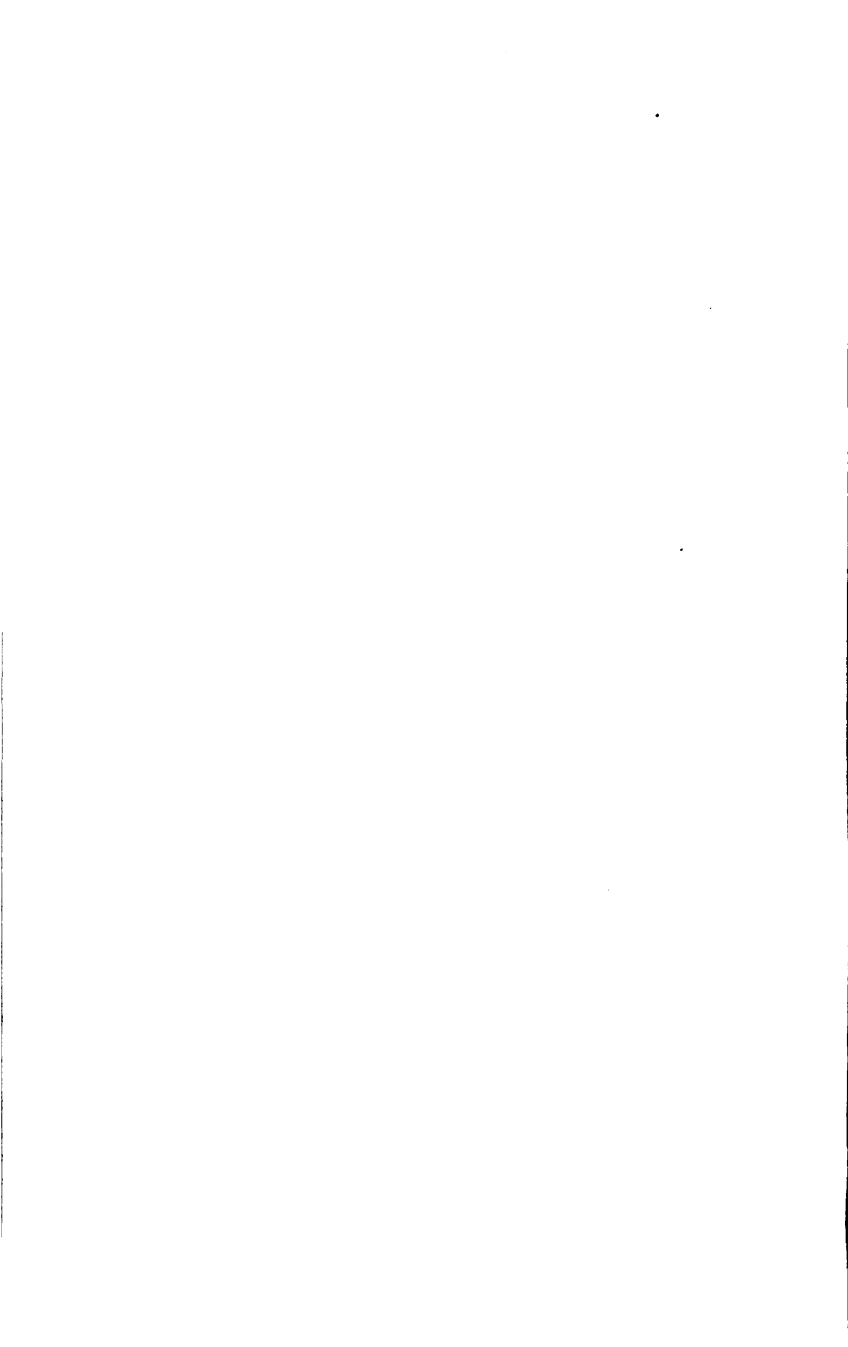
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TECHNICAL CHEMISTS' HANDBOOK.

TABLES AND METHODS OF ANALYSIS FOR
MANUFACTURERS OF INORGANIC CHEMICAL
PRODUCTS

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THE AMERICAN CHEMICAL SOCIETY

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GENERAL

PREFACE

IN 1883 I published in German a collection of tables and analytical methods for manufacturers of sulphuric acid, nitric acid, soda, potash, and ammonia.

In 1884 an English edition of that work was published by me, with the co-operation of the late Dr Ferdinand Hurter, under the title, *The Alkali Makers' Pocketbook*. A second, enlarged edition was published by us in 1891 as *The Alkali Makers' Handbook*. Subsequently a third, thoroughly revised German edition was published by me, but the death of Dr Hurter, and lack of time on my part, prevented the publication of a corresponding English edition.

When the need of a further German edition arose, I resolved, not merely, as in the past, to bring both the numerical data and the analytical methods up to date, which meant replacing many of the tables by new ones and changing a great part of the text, but also to enlarge the scope of the book, so as to include a number of additional important inorganic chemical industries. New chapters were accordingly added, treating of feed-water for boilers, of the manufacture of coal-gas, of calcium carbide and acetylene, of the raw materials and products in the manufacture of fertilisers, of aluminium salts and the manufacture of alumina, and of the manufacture of calcareous cements. In the preparation of this edition, I availed myself of the assistance of Dr Berl.

The additions thus included, and the general revision of the work, made it, to all intents and purposes, a new book, and the

title of that German book was accordingly changed to a *Handbook for the Inorganic Chemical Industries*.

It was natural that this book should also be offered to English and American chemists, and this is done in the present *Handbook*. Its aim, like that of its predecessor, *The Alkali Makers' Handbook*, is to effect, as far as possible, the most important task of establishing uniformity among practical chemists, buyers and sellers, and analysts, in regard to both the numerical data employed in their work and the analytical methods used for the control of processes, and for the testing of the resulting products.

The importance of making use of the most reliable numerical data has been fully recognised in the preparation of this edition, and all the analytical factors have been recalculated on the basis of the atomic weights published by the International Committee for 1908. Also, all the tables of specific gravities and other tables have been selected from among the most recent and reliable determinations.

In regard to the analytical methods, they are again chosen as before, on the principle agreed to by the German Society of Alkali Makers, that only *one* method should be given for each analytical operation, as well as for the preparation of standard solutions and for sampling the materials, in order to avoid discrepancies such as might arise should two or more methods be included. The method chosen should always, of course, be that which permits the greatest degree of accuracy possible that can be attained in a well-appointed works laboratory by a properly trained chemist. In cases where there was a choice between equally accurate methods, that occupying least time or least apparatus, or which was already widely known and employed, has been preferred. Many new methods have accordingly had to be omitted, but in all cases such omission has been justified by means of a careful examination of the relative merits of the processes under consideration, and only such methods as were found thoroughly reliable have been included. Also, a considerable number of tables of specific gravities of solutions not previously

worked out, or which were unsatisfactory, have been very carefully checked and extended.

Where necessary, reference is made to the more complete treatment of the subject matter in my larger treatise, published in German as *Chemisch-technische Untersuchungsmethoden* (5th edition, 3 vols., 1904-5). Of the English edition of this work, edited by Dr Charles A. Keane, under the title *Technical Methods of Chemical Analysis*, the first volume is now being published, and is referred to in the text as *Tech. Meth.*

My special thanks are due to Dr Keane for linguistically revising the text of this English edition, a task which has been rendered necessary through my absence from England for more than thirty years.

THE AUTHOR.

ZÜRICH, 1909.



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GENERAL TABLES

NOTE

All temperatures are given in degrees Centigrade, unless otherwise stated.

The *atomic weights* are those adopted by the International Committee on Atomic Weights for the year 1909, as given in Table No. 1 referred to. Oxygen = 16.

TABLE 1.—INTERNATIONAL ATOMIC WEIGHTS

According to the Table issued by the International Committee
on Atomic Weights for 1909.

Al	Aluminium . . .	27·1	Nd	Neodymium . . .	144·3
Sb	Antimony . . .	120·2	Ne	Neon . . .	20
Ar	Argon . . .	39·9	Ni	Nickel . . .	58·68
As	Arsenic . . .	75·0	Nb	Niobium . . .	93·5
Ba	Barium . . .	137·37	N	Nitrogen . . .	14·01
Be	Beryllium . . .	9·1	Os	Osmium . . .	190·9
Bi	Bismuth . . .	208·0	O	Oxygen . . .	16·00
B	Boron . . .	11·0	Pd	Palladium . . .	106·7
Br	Bromine . . .	79·92	P	Phosphorus . . .	31·0
Cd	Cadmium . . .	112·40	Pt	Platinum . . .	195·0
Cs	Cæsium . . .	132·81	K	Potassium . . .	39·10
Ca	Calcium . . .	40·09	Pr	Praseodymium . . .	140·6
C	Carbon . . .	12·00	Ra	Radium . . .	226·4
Ce	Cerium . . .	140·25	Rh	Rhodium . . .	102·9
Cl	Chlorine . . .	35·46	Rb	Rubidium . . .	85·45
Cr	Chromium . . .	52·1	Ru	Ruthenium . . .	101·7
Co	Cobalt . . .	58·97	Sm	Samarium . . .	150·4
Cu	Copper . . .	63·57	Sc	Scandium . . .	44·1
Dy	Dysprosium . . .	162·5	Se	Selenium . . .	79·2
Er	Erbium . . .	167·4	Si	Silicon . . .	28·3
Eu	Europium . . .	152·0	Ag	Silver . . .	107·88
F	Fluorine . . .	19·0	Na	Sodium . . .	23·00
Gd	Gadolinium . . .	157·3	Sr	Strontium . . .	87·62
Ga	Gallium . . .	69·9	S	Sulphur . . .	32·07
Ge	Germanium . . .	72·5	Ta	Tantalum . . .	181·0
Au	Gold . . .	197·2	Te	Tellurium . . .	127·5
He	Helium . . .	4·0	Tb	Terbium . . .	159·2
H	Hydrogen . . .	1·008	Tl	Thallium . . .	204·0
In	Indium . . .	114·8	Th	Thorium . . .	232·42
I	Iodine . . .	126·92	Tu	Thulium . . .	168·5
Ir	Iridium . . .	193·1	S n	Tin . . .	119·0
Fe	Iron . . .	55·85	Ti	Titanium . . .	48·1
Kr	Krypton . . .	81·8	W	Tungsten . . .	184·0
La	Lanthanum . . .	139·0	U	Uranium . . .	238·5
Pb	Lead . . .	207·10	V	Vanadium . . .	51·2
Li	Lithium . . .	7·00	X	Xenon . . .	128
Mg	Magnesium . . .	24·32	Yb	Ytterbium . . .	172
Mn	Manganese . . .	54·93	Y	Yttrium . . .	89·0
Hg	Mercury . . .	200·00	Zn	Zinc . . .	65·37
Mo	Molybdenum . . .	96·0	Zr	Zirconium . . .	90·6

TABLE 2.—SYMBOLS, MOLECULAR WEIGHTS, AND PERCENTAGE COMPOSITION

Of Compounds which are of importance in the Inorganic Chemical Industries and in Technical Analysis.

Note.—The salts are arranged alphabetically according to their cations. The H₂O given in the percentage composition includes the water formed by the decomposition of hydrates and of the ammonium-ion.

Compounds.	Formula.	Molec. weight. O = 16.	Percentage Composition.
Alum, <i>cf.</i> Ammonium & Potassium			
Aluminium chloride	AlCl ₃	133.45	Al 20.31; Cl 76.69.
hydroxide	Al(OH) ₃	78.13	Al ₂ O ₃ 65.40; H ₂ O 34.60.
oxide (alumina)	Al ₂ O ₃	102.20	Al 53.03; O 46.97.
sulphate	Al ₂ (SO ₄) ₃	342.38	Al ₂ O ₃ 29.85; SO ₃ 70.15.
cryst.	Al ₂ (SO ₄) ₃ + 18H ₂ O	666.67	Al ₂ O ₃ 15.38; SO ₃ 36.03; H ₂ O 48.64.
Ammonia	NH ₃	17.03	N 82.26; H 17.74.
alum	Al(NH ₄)(SO ₄) ₂ + 12H ₂ O	453.45	Al ₂ O ₃ 11.27; NH ₃ 3.76; SO ₃ 36.31; H ₂ O 49.66.
Ammonium carbonate	(NH ₄)HCO ₃ + (NH ₄)CO ₃ (NH ₄)	157.12	NH ₃ 32.52; CO ₂ 56.01; H ₂ O 11.47.
chloride	NH ₄ Cl	53.49	NH ₃ 31.85; HCl 68.15.
magnesium arsenate	(NH ₄)MgAsO ₄ + ½H ₂ O	190.41	MgO 21.20; As ₂ O ₅ 60.40; NH ₃ 8.95; H ₂ O 9.45.
magnesium phos- phate, cryst.	(NH ₄)MgPO ₄ + 6H ₂ O	245.50	MgO 16.44; NH ₃ 6.94; P ₂ O ₅ 28.92; H ₂ O 47.70.
nitrate	(NH ₄)NO ₃	80.05	NH ₃ 21.27; N ₂ O ₅ 67.48; H ₂ O 11.25.

TABLE 2—Continued.

Compounds.	Formula.	Molec. weight, O=16.	Percentage Composition.
Ammonium phosphate	$(\text{NH}_4)_2\text{HPO}_4$	132.09	NH_3 25.79; P_2O_5 58.75; H_2O 20.46.
sodium phosphate	$(\text{NH}_4)\text{NaPO}_4 + 4\text{H}_2\text{O}$	209.16	NH_3 8.14; Na_2O 14.85; P_2O_5 38.95; H_2O 43.06.
platinum chloride	$(\text{NH}_4)_2\text{PtCl}_6$	443.58	NH_3 7.68; Pt 43.92; Cl 47.95; H_2O 0.45.
sulphate	$(\text{NH}_4)_2\text{SO}_4$	132.14	NH_3 25.78; SO_3 60.59; H_2O 13.63.
thiocyanate	$(\text{NH}_4)\text{CNS}$	76.11	NH_3 22.38; H 1.32; CN 34.17; S 42.13.
Arsenic pentoxide	As_2O_5	230.0	As 65.22; O 34.78.
trioxide	As_2O_3	198.0	As 75.76; O 24.24.
trisulphide	As_2S_3	246.18	As 60.93; S 39.07.
Barium monoxide	BaO	153.4	Ba 89.57; O 10.48.
hydroxide	$\text{Ba}(\text{OH})_2$	171.42	BaO 89.49; H_2O 10.51.
cryst.	$\text{Ba}(\text{OH})_2 + 8\text{H}_2\text{O}$	315.54	BaO 48.62; H_2O 51.38.
carbonate	BaCO_3	197.40	BaO 77.71; CO_2 22.29.
chloride	$\text{BaCl}_2 + 2\text{H}_2\text{O}$	244.33	BaCl ₂ 85.25; H_2O 14.75.
sulphate	BaSO_4	233.46	BaO 65.71; SO_3 34.29.
Calcium oxide (lime)	CaO	56.1	Ca 71.48; O 28.52.
hydroxide	$\text{Ca}(\text{OH})_2$	74.12	CaO 75.69; H_2O 24.31.
carbonate	CaCO_3	100.1	CaO 56.04; CO_2 43.96.
chlorate	$\text{Ca}(\text{ClO}_3)_2$	207.0	CaO 27.10; Cl_2O_7 72.90.
chloride	CaCl_2	111.0	Ca 36.18; Cl 63.87.
cryst.	$\text{CaCl}_2 + 6\text{H}_2\text{O}$	219.10	CaCl ₂ 50.66; H_2O 49.34.
hypochlorite	$\text{Ca}(\text{OCl})_2$	148.0	CaO 39.28; Cl 49.58; O 11.19.
phosphate, primary	$\text{CaH}_2(\text{PO}_4)_2$	234.13	CaO 23.96; P_2O_5 60.66; H_2O 15.38.
secondary	$\text{CaH}(\text{PO}_4)$	186.11	CaO 41.22; P_2O_5 52.16; H_2O 6.62.

TABLE 2.—SYMBOLS, MOLECULAR WEIGHTS, AND PERCENTAGE COMPOSITION

Of Compounds which are of importance in the Inorganic Chemical Industries and in Technical Analysis.

Note.—The salts are arranged alphabetically according to their cations. The H₂O given in the percentage composition includes the water formed by the decomposition of hydrates and of the ammonium-ion.

Compounds.	Formula.	Molec. weight. O = 16.	Percentage Composition.
Alum., <i>cf.</i> Ammonium & Potassium			
Aluminium chloride	AlCl ₃	133.45	Al 20.31; Cl 76.69.
hydroxide	Al(OH) ₃	78.13	Al ₂ O ₃ 65.40; H ₂ O 34.60.
oxide (alumina)	Al ₂ O ₃	102.20	Al 58.03; O 46.97.
sulphate	Al ₂ (SO ₄) ₃	342.38	Al ₂ O ₃ 29.85; SO ₃ 70.15.
cryst.	Al ₂ (SO ₄) ₃ + 18H ₂ O	666.67	Al ₂ O ₃ 15.38; SO ₃ 36.08; H ₂ O 48.64.
Ammonia	NH ₃	17.03	N 82.26; H 17.74.
alum	Al(NH ₄)(SO ₄) ₂ + 12H ₂ O	453.45	Al ₂ O ₃ 11.27; NH ₃ 3.76; SO ₃ 35.31; H ₂ O 49.66.
Ammonium carbonate	(NH ₄)HCO ₃ + (NH ₄)CO ₃ (NH ₄) ₂	157.12	NH ₃ 32.52; CO ₂ 56.01; H ₂ O 11.47.
chloride	NH ₄ Cl	53.49	NH ₃ 31.85; HCl 68.15.
magnesium arsenate	(NH ₄)MgAsO ₄ + $\frac{1}{2}$ H ₂ O	190.41	MgO 21.20; As ₂ O ₅ 60.40; NH ₃ 8.95; H ₂ O 9.45.
magnesium phosphate, cryst.	(NH ₄)MgPO ₄ + 6H ₂ O	245.50	MgO 16.44; NH ₃ 6.94; P ₂ O ₅ 28.92; H ₂ O 47.70.
nitrate	(NH ₄)NO ₃	80.05	NH ₃ 21.27; N ₂ O ₅ 67.48; H ₂ O 11.25.

TABLE 2—Continued.

Compounds.	Formulas.	Molec. weight, O=16.	Percentage Composition.
Ammonium phosphate	$(\text{NH}_4)_2\text{HPO}_4$	182.09	NH_3 25.79; P_2O_5 58.75; H_2O 20.46.
sodium phosphate	$(\text{NH}_4)\text{NaPO}_4 + 4\text{H}_2\text{O}$	209.16	NH_3 8.14; Na_2O 14.85; P_2O_5 38.95; H_2O 43.06.
platinum chloride	$(\text{NH}_4)_2\text{PtCl}_6$	443.58	NH_3 7.68; Pt 43.92; Cl 47.95; H_2O 0.45.
sulphate	$(\text{NH}_4)_2\text{SO}_4$	132.14	NH_3 25.78; SO_3 60.59; H_2O 13.68.
thiocyanate	$(\text{NH}_4)\text{CNS}$	76.11	NH_3 22.38; H 1.32; CN 34.17; S 42.13.
Arsenic pentoxide	As_2O_5	230.0	As 65.22; O 34.78.
trioxide	As_2O_3	198.0	As 75.76; O 24.24.
trisulphide	As_2S_3	246.18	As 60.93; S 39.07.
Barium monoxide	BaO	153.4	Ba 89.57; O 10.43.
hydroxide	$\text{Ba}(\text{OH})_2$	171.42	BaO 89.49; H_2O 10.51.
carbonate	$\text{Ba}(\text{OH})_2 + 8\text{H}_2\text{O}$	315.54	BaO 48.62; H_2O 51.38.
chloride	BaCO_3	197.40	BaO 77.71; CO_2 22.29.
sulphate	$\text{BaCl}_2 + 2\text{H}_2\text{O}$	244.33	BaCl_2 85.25; H_2O 14.75.
oxide (lime)	BaSO_4	233.46	BaO 65.71; SO_3 34.29.
hydroxide	CaO	56.1	Ca 71.48; O 28.52.
carbonate	$\text{Ca}(\text{OH})_2$	74.12	CaO 75.69; H_2O 24.31.
chlorate	CaCO_3	100.1	CaO 56.04; CO_2 43.96.
chloride	$\text{Ca}(\text{ClO}_3)_2$	207.0	CaO 27.10; Cl_2O_5 72.90.
chloride	CaCl_2	111.0	Ca 36.13; Cl 63.87.
hypochlorite	$\text{CaCl}_2 + 6\text{H}_2\text{O}$	219.10	CaCl_2 50.66; H_2O 49.34.
phosphate, primary	$\text{Ca}(\text{OCl})_2$	148.0	CaO 39.23; Cl 49.58; O 11.19.
phosphate, secondary	$\text{Ca}_2(\text{PO}_4)_2$	234.18	CaO 23.96; P_2O_5 60.66; H_2O 15.38.
	$\text{CaH}(\text{PO}_4)$	136.11	CaO 41.22; P_2O_5 52.16; H_2O 6.62.

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oxide (alumina)	Al ₂ O ₃	102.20	Al 53.08; O 46.97.
sulphate	Al ₂ (SO ₄) ₃	342.38	Al ₂ O ₃ 29.85; SO ₃ 70.15.
cryst.	Al ₂ (SO ₄) ₃ + 18H ₂ O	666.67	Al ₂ O ₃ 15.38; SO ₃ 86.03; H ₂ O 48.64.
Ammonia	NH ₃	17.03	N 82.26; H 17.74.
alum	Al(NH ₄)(SO ₄) ₂ + 12H ₂ O	463.45	Al ₂ O ₃ 11.27; NH ₃ 3.76; SO ₃ 85.31; H ₂ O 49.66.
Ammonium carbonate	(NH ₄)HCO ₃ + (NH ₄)CO ₃ (NH ₂)	157.12	NH ₃ 32.52; CO ₂ 56.01; H ₂ O 11.47.
chloride	NH ₄ Cl	53.49	NH ₃ 31.85; HCl 68.15.
magnesium arsenate	(NH ₄)MgAsO ₄ + 1/2H ₂ O	190.41	MgO 21.20; As ₂ O ₅ 60.40; NH ₃ 8.95; H ₂ O 9.45.
magnesium phosphate, phosphat.	(NH ₄)MgPO ₄ + 6H ₂ O	245.50	MgO 16.44; NH ₃ 6.94; P ₂ O ₅ 28.92; H ₂ O 47.70.
nitrate	(NH ₄)NO ₃	80.05	NH ₃ 21.27; N ₂ O ₅ 67.48; H ₂ O 11.26.

TABLE 2—Continued.

Compounds.	Formula.	Molec. weight. O = 16.	Percentage Composition.
Ammonium phosphate	$(\text{NH}_4)_2\text{HPO}_4$	182.09	NH_3 25.79; P_2O_5 58.75; H_2O 20.46.
sodium phosphate	$(\text{NH}_4)\text{NaPO}_4 + 4\text{H}_2\text{O}$	209.16	NH_3 8.14; Na_2O 14.85; P_2O_5 38.95; H_2O 43.06.
platinum chloride	$(\text{NH}_4)_2\text{PtCl}_6$	443.58	NH_3 7.08; Pt 43.92; Cl 47.95; H_2O 0.46.
sulphate	$(\text{NH}_4)_2\text{SO}_4$	132.14	NH_3 25.78; SO_3 60.59; H_2O 13.63.
thiocyanate	$(\text{NH}_4)\text{CNS}$	76.11	NH_3 22.38; H 1.32; CN 34.17; S 42.13.
Arsenic pentoxide	As_2O_5	230.0	As 65.22; O 34.78.
trioxide	As_2O_3	198.0	As 75.76; O 24.24.
trisulphide	As_2S_3	246.18	As 60.93; S 39.07.
Barium monoxide	BaO	153.4	Ba 89.57; O 10.43.
hydroxide	$\text{Ba}(\text{OH})_2$	171.42	BaO 89.49; H_2O 10.51.
cryst.	$\text{Ba}(\text{OH})_2 + 8\text{H}_2\text{O}$	315.54	BaO 48.62; H_2O 51.38.
carbonate	BaCO_3	197.40	BaO 77.71; CO_2 22.29.
chloride	$\text{BaCl}_2 + 2\text{H}_2\text{O}$	244.38	BaCl_2 85.25; H_2O 14.75.
sulphate	BaSO_4	233.46	BaO 65.71; SO_3 34.29.
Calcium oxide (lime)	CaO	56.1	Ca 71.48; O 28.52.
hydroxide	$\text{Ca}(\text{OH})_2$	74.12	CaO 75.69; H_2O 24.31.
carbonate	CaCO_3	100.1	CaO 56.04; CO_2 43.96.
chlorate	$\text{Ca}(\text{ClO}_3)_2$	207.0	CaO 27.10; Cl_2O_5 72.90.
chloride	CaCl_2	111.0	Ca 36.18; Cl 63.87.
cryst.	$\text{CaCl}_2 + 6\text{H}_2\text{O}$	219.10	CaCl_2 50.66; H_2O 49.34.
hypochlorite	$\text{Ca}(\text{OCl})_2$	143.0	CaO 39.23; Cl 49.58; O 11.19.
phosphate, primary	$\text{CaH}_2(\text{PO}_4)_2$	234.13	CaO 23.96; P_2O_5 60.66; H_2O 15.38.
secondary	$\text{CaH}(\text{PO}_4)$	136.11	CaO 41.22; P_2O_5 52.16; H_2O 6.62.

TABLE 2—Continued.

Compounds.	Formula.	Molec. weight. O = 16.	Percentage Composition.
Calcium phosphate, tertiary sulphate (anhydrite)	$\text{Ca}_3(\text{PO}_4)_2$	310.8	CaO 54.24; P_2O_5 45.76.
hydrated (gypsum)	$\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$	136.16	CaO 41.20; SO_3 58.80.
hydrous	$\text{CaSO}_4 + 2\text{H}_2\text{O}$	172.19	CaO 32.58; SO_3 46.50; H_2O 20.92.
sulphide.	CaS	72.16	Ca 55.57; S 44.43.
pentasulphide	CaS_5	200.40	Ca 20.01; S 79.99.
sulphite.	CaSO_3	120.16	CaO 46.69; SO_2 53.31.
thiosulphate.	CaS_2O_3	152.22	CaO 36.85; SO_2 42.09; S 21.06.
Carbon dioxide.	CO_2	44.00	C 27.27; O 72.73.
Carbon monoxide.	CO	28.00	C 42.86; O 57.14.
Chloric acid.	HClO_3	84.46	Cl 41.97; O 47.36; H_2O 10.67.
Copper oxide.	CuO	79.6	Cu 79.90; O 20.10.
chloride.	CuCl_2	134.5	Cu 47.29; Cl 52.71.
sulphide (cuprous).	Cu_2S	159.26	Cu 79.87; S 20.13.
(cupric).	CuS	95.66	Cu 66.49; S 33.51.
sulphate.	$\text{CuSO}_4 + 5\text{H}_2\text{O}$	249.74	CuO 31.87; SO_3 32.06; H_2O 85.07.
Ethylene.	C_2H_4	28.03	C 85.62; H 14.38.
Hydrochloric acid.	HCl	36.46	Cl 97.23; H 2.77.
Hypochlorous acid.	HOCl	52.46	Cl 67.58; O 30.50; H 1.92.
anhydride.	Cl_2O	86.90	Cl 81.59; O 18.41.
Iron oxide (ferric).	Fe_2O_3	159.8	Fe 69.96; O 30.04.
hydrated (ferric hydroxide).	$\text{Fe}(\text{OH})_3$	106.98	Fe_2O_3 74.73; H_2O 25.27.
Iron chloride (ferrous).	FeCl_2	126.80	Fe 44.09; Cl 55.91.
cryst.	$\text{FeCl}_2 + 4\text{H}_2\text{O}$	198.86	FeCl_2 63.76; H_2O 36.24.

TABLE 2—Continued.

Compounds.	Formula.	Molec. weight. O=16.	Percentage Composition.
Iron chloride (ferric) bisulphide (pyrites) sulphate (ferrous)	FeCl_3 FeS_2 $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$	162.25 120.02 278.07	Fe 34.45; Cl 65.55. Fe 46.58; S 53.42. Fe 20.10; O 5.75; SO_3 28.79; H_2O 45.86.
Lead monoxide (litharge) oxide (red lead) carbonate chloride sulphate sulphide	PbO Pb_2O_3 PbCO_3 PbCl_2 PbSO_4 PbS	222.90 684.7 266.90 277.80 302.96 238.96	Pb 92.82; O 7.18. Pb 90.65; O 9.35. Pb 88.51; CO_2 16.49. Pb 74.48; Cl 25.42. Pb 73.57; SO_3 26.48. Pb 86.58; S 13.42.
Magnesium oxide hydroxide chloride cryst. carbonate pyrophosphate sulphate, cryst.	MgO Mg(OH)_2 MgCl_2 $\text{MgCl}_2 \cdot 6\text{H}_2\text{O}$ MgCO_3 $\text{Mg}_2\text{P}_2\text{O}_7$ $\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$	40.86 58.38 95.26 208.36 84.36 222.72 246.53	Mg 60.36; O 39.64. Mg 69.13; H_2O 30.87. Mg 25.57; Cl 74.43. Mg Cl_2 46.84; H_2O 53.16. Mg 47.84; CO_3 52.16. Mg 36.24; P_2O_5 63.76. Mg 16.87; SO_3 32.48; H_2O 51.15.
Manganese protoxide. sesquioxide dioxide	MnO Mn_2O_3 MnO_2	71 158 87	Mn 77.46; O 22.54. Mn 69.62; O 30.38. Mn 68.22; O 36.78.
Manganous manganese oxide chloride sulphate	Mn_2O_4 MnCl_2 MnSO_4	229 125.90 151.06	Mn 72.05; O 27.95. Mn 43.69; Cl 56.31. Mn 47.00; SO_3 53.00.
Mercurous chloride	HgCl	234.45	Hg 84.94; Cl 15.06.

TABLE 72—Continued.

Compounds.	Formula.	Molec. weight, O = 16.	Percentage Composition.
Mercuric chloride	HgCl ₂	270·90	Hg 73·83; Cl 26·17.
Methane	CH ₄	16·03	C 74·86; H 25·14.
Nitrosulphonic acid (nitrososulphuric acid, chamber crystals)	SO ₂ (OH)(ONO)	127·08	SO ₂ 63·00; N ₂ O ₃ 29·91; H ₂ O 7·09.
Nitrous oxide	N ₂ O	44·02	N 63·65; O 36·35.
Nitric oxide	NO	30·01	N 46·68; O 53·32.
Nitrous anhydride	N ₂ O ₃	76·02	N 36·86; O 63·14.
Nitrous acid	NO ₂ H	47·02	N ₂ O ₃ 80·84; H ₂ O 19·16.
Nitric peroxide (tetroxide)	NO ₂ or N ₂ O ₄	{ 46·01 92·02	} N 30·45; O 69·55.
acid	NO ₃ H	63·02	
Pentathionic acid, <i>cf.</i> Sulphur	P ₂ O ₅	142·00	P 43·66; O 56·34.
Phosphoric pentoxide.	H ₃ PO ₄	98·02	P ₂ O ₅ 72·43; H ₂ O 27·57.
acid, ortho-	H ₄ P ₂ O ₇	178·03	P ₂ O ₅ 79·76; H ₂ O 20·24.
pyro-	HPO ₃	80·01	P ₂ O ₅ 88·74; H ₂ O 11·26.
meta-	H ₂ PtCl ₆	409·52	Pt 47·57; Cl 51·94; H 0·49.
Platinum-hydrogen chloride	K ₂ O	94·30	K 83·03; O 16·97.
Potassium	KOH	56·16	K ₂ O 83·96; H ₂ O 16·04.
hydroxide	K ₂ CO ₃	138·30	K ₂ O 68·19; CO ₂ 31·81.
carbonate	KHCO ₃	100·16	K ₂ O 47·07; CO ₂ 43·93; H ₂ O 9·00.
bicarbonate	K ₂ Cr ₂ O ₇	294·50	K ₂ O 32·02; Cr ₂ O ₃ 67·98.
bichromate	KClO ₃	122·60	K ₂ O 38·46; Cl 28·92; O 32·62.
chlorate	KCl	74·60	K ₂ O 48·51; Cl 47·52.
chloride	K ₂ CrO ₄	194·4	K ₂ O 48·51; Cr ₂ O ₃ 51·49.
chromate			

TABLE 2—Continued.

Compounds.	Formula.	Molec. weight. O = 16.	Percentage Composition.
Potassium cyanide	KCN	65.16	K 60.08; CN 39.92.
ferricyanide	$K_3Fe(CN)_6$	329.41	K 35.65; Fe 16.97; CN 47.38.
ferrocyanide	$K_4Fe(CN)_6 + 3H_2O$	422.61	K 37.06; Fe 13.22; CN 36.93; H_2O 12.79.
iodide	KJ	166.12	K 23.57; J 76.43.
nitrate	KNO_3	101.16	K_2O 46.61; N_2O_5 53.39.
nitrite	KNO_2	85.16	K_2O 55.37; N_2O_3 44.63.
permanganate	$KMnO_4$	158.15	K_2O 29.81; Mn_2O_7 70.19.
phosphate	K_2HPO_4	174.31	K_2O 54.10; P_2O_5 40.73; H_2O 5.17.
platinum chloride	K_2PtCl_6	485.80	Pt 40.10; Cl 43.78; K 16.12 (KCl 30.72).
silicate	K_2SiO_3	154.70	K_2O 60.96; SiO_2 39.04.
sulphate	K_2SO_4	174.36	K_2O 54.08; SO_3 45.92.
bisulphate	$KHSO_4$	136.22	K_2O 34.61; SO_3 55.77; H_2O 6.62.
sulphide	K_2S	110.36	K 70.95; S 29.05.
sulphite, cryst.	$K_2SO_3 + 2H_2O$	194.39	K_2O 48.51; SO_2 32.95; H_2O 18.54.
bisulphite	$KHSO_3$	120.22	K_2O 39.22; SO_2 53.29; H_2O 7.49.
thiocyanate	KCN S	97.22	K 40.27; CNS 59.73.
Polash alum	$KAl(SO_4)_2 + 12H_2O$	474.56	K_2O 9.94; Al_2O_3 10.77; SO_3 33.74; H_2O 45.55.
Selenious anhydride	SeO_2	111.2	Se 71.22; O 28.78.
Silicic anhydride (silica)	SiO_2	60.4	Si 47.02; O 52.98.
Silver bromide	AgBr	187.89	Ag 57.44; Br 42.56.
chloride	AgCl	143.38	Ag 75.28; Cl 24.72.
iodide	AgJ	234.90	Ag 45.95; J 54.05.
nitrate	$AgNO_3$	169.94	Ag 63.51; NO_3 36.49.

TABLE 2—Continued.

Compounds.	Formula.	Molec. weight. O = 16.	Percentage Composition.
Silver sulphide	Ag ₂ S	247·92	Ag 87·07; S 12·93.
thiocyanate	AgCNS	166·00	Ag 65·02; CNS 34·98.
Sodium oxide	Na ₂ O	62·00	Na 74·23; O 25·77.
hydroxide	NaOH	40·05	Na ₂ O 77·53; H ₂ O 22·47.
aluminate	Na ₃ AlO ₃	144·25	Na ₂ O 64·58; Al ₂ O ₃ 35·42.
borate	Na ₂ Al ₂ O ₄	164·3	Na ₂ O 37·80; Al ₂ O ₃ 62·20.
	Na ₂ B ₄ O ₇ + 10H ₂ O	382·26	Na ₂ O 16·25; B ₂ O ₃ 36·62; H ₂ O 47·13.
carbonate anhydrous	Na ₂ CO ₃	106·1	Na ₂ O 58·53; CO ₂ 41·47.
decahydrated	Na ₂ CO ₃ + 10H ₂ O	286·26	Na ₂ O 21·69; CO ₂ 15·87; H ₂ O 62·94.
bicarbonate	NaHCO ₃	84·06	Na ₂ O 36·94; CO ₂ 52·34; H ₂ O 10·72.
chlorate	NaClO ₃	106·50	Na ₂ O 29·15; Cl ₂ O ₆ 70·86.
chloride	NaCl	58·50	Na 39·40; Cl 60·60.
chromate	Na ₂ CrO ₄	162·2	Na ₂ O 38·29; CrO ₃ 61·71.
bichromate	NaHCrO ₄	140·16	Na ₂ O 22·15; CrO ₃ 71·42; H ₂ O 6·43.
hypochlorite	NaOCl	74·50	Na ₂ O 41·68; Cl ₂ O 58·32.
nitrate	NaNO ₃	85·06	Na ₂ O 36·50; N ₂ O ₅ 63·50.
nitrite	NaNO ₂	69·06	Na ₂ O 44·96; N ₂ O ₃ 55·04.
phosphate	Na ₃ HPO ₄ + 12H ₂ O	368·30	Na ₂ O 17·38; P ₂ O ₅ 19·82; H ₂ O 62·85.
silficate	Na ₂ SiO ₃	122·50	Na ₂ O 50·69; SiO ₂ 49·31.
sulphate	Na ₂ SO ₄	142·16	Na ₂ O 43·68; SO ₃ 56·32.
bisulphate	Na ₂ SO ₄ + 10H ₂ O	322·32	Na ₂ O 19·27; SO ₃ 27·84; H ₂ O 55·89.
	cryst.	120·12	Na ₂ O 25·85; SO ₃ 66·66; H ₂ O 7·50.
hydrogen sulphide	NaHS	78·16	Na ₂ S 98·98; S 41·02.
sulphite, cryst.	Na ₂ S	56·12	Na ₂ S 69·64; H ₂ S 30·36.
	Na ₂ SO ₃ + 6H ₂ O	234·26	Na ₂ O 26·51; SO ₂ 27·35; H ₂ O 46·14.

TABLE 2—Continued.

Compounds.	Formula.	Molec. weight. O = 16.	Percentage Composition.
Sodium bisulphite	NaHSO_3	104.12	Na_2O 29.82; SO_3 61.53; H_2O 8.65.
thiosulphate	$\text{Na}_2\text{S}_2\text{O}_3 + 5\text{H}_2\text{O}$	248.80	Na_2O 25.01; S 12.91; SO_2 25.80; H_2O 36.28.
Sulphur dioxide	SO_2	64.06	S 50.05; O 49.95.
trioxide	SO_3	80.06	S 40.05; O 59.95.
Sulphuric acid	H_2SO_4	98.08	SO_3 81.63; H_2O 18.37.
pyro-	$\text{H}_2\text{S}_2\text{O}_7$	178.14	H_2SO_4 55.06; SO_3 44.94.
Trithionic acid	$\text{H}_2\text{S}_3\text{O}_6$	194.2	SO_3 41.23; SO_2 32.99; S 16.51; H_2O 9.27.
Tetrathionic acid	$\text{H}_2\text{S}_4\text{O}_6$	222.26	SO_3 35.39; SO_2 28.31; S 28.34; H_2O 7.96.
Pentathionic acid	$\text{H}_2\text{S}_5\text{O}_6$	258.32	SO_3 30.99; SO_2 24.80; S 37.23; H_2O 6.98.
Sulphuretted hydrogen	H_2S	34.08	S 94.07; O 5.93.
Tin chloride (stannous)	$\text{SnCl}_2 + 2\text{H}_2\text{O}$	225.44	Sn 52.56; Cl 31.45; H_2O 15.99.
Water	H_2O	18.02	H 11.21; O 88.79.
Zinc oxide	ZnO	81.4	Zn 80.34; O 19.66.
chloride	ZnCl_2	136.3	Zn 47.98; Cl 52.02.
sulphate	ZnSO_4	161.46	ZnO 50.41; SO_3 49.59.
cryst.	$\text{ZnSO}_4 + 7\text{H}_2\text{O}$	287.57	ZnO 28.31; SO_3 27.84; H_2O 18.85.
sulphide	ZnS	97.46	Zn 67.10; S 32.90.

TABLE 3.—FACTORS FOR CALCULATING

Substance Weighed.	Substance to be determined.	1.
Ammonium.		
Ammonium chloride, NH_4Cl	Ammonia NH_3	0·3184
Ammonium platinum chloride, $(\text{NH}_4)_2\text{PtCl}_6$	Ammonium oxide $(\text{NH}_4)_2\text{O}$	0·1174
	Ammonia, NH_3	0·0768
	Nitrogen N	0·0632
Arsenic.		
Arsenic trisulphide, As_2S_3	Arsenic, As	0·6093
	Arsenic trioxide, As_2O_3	0·8043
	Arsenic anhydride, As_2O_5	0·9343
Ammonium magnesium arsenate, $\text{Mg}(\text{NH}_4)\text{AsO}_4 + \frac{1}{2} \text{aq.}$	Arsenic, As	0·3939
	Arsenic trioxide, As_2O_3	0·5198
	Arsenic anhydride, As_2O_5	0·6039
Barium.		
Barium sulphate, BaSO_4	Barium oxide, $\left\{ \begin{array}{l} \text{BaO} \\ \text{BaO} \\ \text{BaO} \end{array} \right.$	0·6571
		0·7771
		0·5483
Barium carbonate, BaCO_3		
Barium silicofluoride, BaSiF_6		
Calcium.		
Calcium sulphate, CaSO_4	Calcium oxide, $\left\{ \begin{array}{l} \text{CaO} \\ \text{CaO} \end{array} \right.$	0·4120
		0·5604
Calcium carbonate, CaCO_3		
Carbon.		
Barium carbonate, BaCO_3	Carbon dioxide, CO_2	0·2229
Calcium carbonate, CaCO_3	Carbon dioxide, CO_2	0·4396
Carbon dioxide, CO_2	Carbon, C	0·2727
Chlorine.		
Silver chloride, AgCl	Chlorine, Cl	0·2472
	Chloric anhydride, Cl_2O_5	0·5262
	Potassium chloride, KCl	0·5203
	Sodium chloride, NaCl	0·4080
	Hydrogen chloride, HCl	0·2543
Copper.		
Cupric oxide, CuO	Copper, Cu	0·7990
Cuprous sulphide, Cu_2S	Copper, Cu	0·7987
	Cupric oxide, CuO	0·9996
Hydrogen.		
Water, H_2O	Hydrogen, H	0·1119
Iron.		
Ferric oxide, Fe_2O_3	Iron, Fe	0·6996
	Ferrous oxide, FeO	0·8999

GRAVIMETRIC ANALYSES.

log	2.	3.	4.	5.	6.	7.	8.	9.
0·50297 - 1	0·6367	0·9551	1·2785	1·5919	1·9102	2·2286	2·5470	2·8653
0·06967 - 1	0·2348	0·3523	0·4697	0·5871	0·7045	0·8219	0·9394	1·0568
0·88536 - 2	0·1536	0·2304	0·3072	0·3840	0·4608	0·5376	0·6144	0·6912
0·80072 - 2	0·1263	0·1895	0·2527	0·3158	0·3790	0·4422	0·5053	0·5685
0·78483 - 1	1·2186	1·8279	2·4372	3·0466	3·6559	4·2652	4·8745	5·4838
0·90542 - 1	1·6086	2·4129	3·2172	4·0215	4·8257	5·6300	6·4343	7·2386
0·97049 - 1	1·8686	2·8028	3·7371	4·6714	5·6057	6·5400	7·4742	8·4085
0·59539 - 1	0·7878	1·1817	1·5756	1·9695	2·3634	2·7573	3·1512	3·5451
0·71584 - 1	1·0396	1·5595	2·0793	2·5991	3·1189	3·6387	4·1586	4·6784
0·78097 - 1	1·2077	1·8116	2·4155	3·0194	3·6232	4·2271	4·8309	5·4348
0·81763 - 1	1·3141	1·9712	2·6283	3·2854	3·9424	4·5995	5·2566	5·9136
0·89048 - 1	1·5542	2·3313	3·1084	3·8855	4·6626	5·4397	6·2168	6·9939
0·73902 - 1	1·0965	1·6448	2·1930	2·7413	3·2895	3·8378	4·3860	4·9343
0·61490 - 1	0·8240	1·2360	1·6480	2·0601	2·4721	2·8841	3·2961	3·7081
0·74850 - 1	1·1209	1·6813	2·2418	2·8022	3·3626	3·9231	4·4835	5·0440
0·34811 - 1	0·4458	0·6687	0·8916	1·1145	1·3374	1·5603	1·7832	2·0061
0·64306 - 1	0·8791	1·3187	1·7582	2·1978	2·6374	3·0769	3·5165	3·9560
0·43569 - 1	0·5455	0·8182	1·0909	1·3637	1·6364	1·9091	2·1818	2·5446
0·39305 - 1	0·4944	0·7415	0·9887	1·2359	1·4831	1·7303	1·9774	2·2246
0·72115 - 1	1·0524	1·5787	2·1049	2·6311	3·1573	3·6835	4·2098	4·7360
0·71625 - 1	1·0406	1·5609	2·0812	2·6015	3·1218	3·6421	4·1624	4·6827
0·61066 - 1	0·8160	1·2240	1·6320	2·0401	2·4481	2·8561	3·2641	3·6721
0·40535 - 1	0·5086	0·7628	1·0171	1·2714	1·5257	1·7800	2·0342	2·2885
0·90255 - 1	1·5980	2·3970	3·1960	3·9950	4·7939	5·5929	6·3919	7·1909
0·90238 - 1	1·5974	2·3961	3·1948	3·9935	4·7921	5·5908	6·3895	7·1882
0·99983 - 1	1·9992	2·9989	3·9985	4·9981	5·9977	6·9973	7·9970	8·9966
0·04883 - 1	0·2238	0·3357	0·4476	0·5595	0·6714	0·7833	0·8952	1·0071
0·84485 - 1	1·3993	2·0939	2·7985	3·4982	4·1978	4·8974	5·5970	6·2967
0·95419 - 1	1·7997	2·6996	3·5995	4·4994	5·3992	6·2991	7·1990	8·0988

TABLE 3—

Substance Weighed.	Substance to be determined.	1.
Lead.		
Lead monoxide, PbO	Lead, Pb	0·9282
Lead sulphate, PbSO ₄	Lead, Pb	0·6829
	Lead oxide, PbO	0·7357
Lead sulphide, PbS	Lead, Pb	0·8658
	Lead oxide, PbO	0·9328
Lead, Pb	Lead oxide, PbO	1·0773
Magnesium.		
Magnesium pyrophosphate, Mg ₂ P ₂ O ₇	Magnesium oxide, MgO.	0·8624
Magnesium sulphate, MgSO ₄	Magnesium oxide, MgO.	0·3352
Manganese.		
Mangano-manganic oxide, Mn ₃ O ₄	Manganese, Mn	0·7205
Manganese sulphide, MnS	Manganese, Mn	0·6318
	Manganous oxide, MnO.	0·8155
Nitrogen.		
Ammonium platinum chloride, (NH ₄) ₂ PtCl ₆	Nitrogen, N	0·0632
Platinum, Pt	Nitrogen, N	0·1438
Phosphorus.		
Magnesium pyrophosphate, Mg ₂ P ₂ O ₇	Phosphorus, P	0·2784
	Phosphorus pentoxide, P ₂ O ₅	0·6376
Potassium.		
Potassium chloride, KCl	Potassium oxide, K ₂ O	0·6320
Potassium - platinum chloride, K ₂ PtCl ₆ (reduction factors adopted at Stassfurt)	Potassium oxide	1·1931
	Potassium chloride	0·3056
Potassium sulphate	Potassium sulphate	0·3571
	Potassium oxide	0·5408
Sodium.		
Sodium sulphate, Na ₂ SO ₄	Sodium oxide, Na ₂ O	0·4368
Sodium carbonate, Na ₂ CO ₃	Sodium oxide, Na ₂ O	0·5853
Sodium chloride, NaCl	Sodium oxide, Na ₂ O	0·5308
Sulphur.		
Barium sulphate, BaSO ₄	Sulphur, S	0·1373
	Sulphur dioxide, SO ₂	0·2744
	Sulphur trioxide, SO ₃	0·3429
	Sulphuric acid, H ₂ SO ₄	0·4201
	Sodium sulphate, Na ₂ SO ₄	0·6089
Zinc.		
Zinc oxide, ZnO	Zinc, Zn	0·8034
Zinc sulphide, ZnS	Zinc, Zn	0·6710
	Zinc oxide, ZnO	0·8352

FACTORS FOR GRAVIMETRIC ANALYSES 15

Continued.

log	2.	3.	4.	5.	6.	7.	8.	9.
0·96764 - 1	1·8564	2·7847	3·7129	4·6411	5·5693	6·4975	7·4258	8·3540
0·88436 - 1	1·3659	2·0488	2·7317	3·4147	4·0976	4·7806	5·4634	6·1464
0·86670 - 1	1·4715	2·2072	2·9430	3·6787	4·4144	5·1502	5·8859	6·6217
0·93742 - 1	1·7317	2·5975	3·4633	4·3292	5·1950	6·0608	6·9266	7·7925
0·96979 - 1	1·8656	2·7984	3·7312	4·6640	5·5967	6·5295	7·4623	8·3951
0·03234	2·1547	3·2320	4·3093	5·3867	6·4640	7·5413	8·6186	9·6960
0·55919 - 1	0·7249	1·0873	1·4497	1·8122	2·1746	2·5370	2·8994	3·2619
0·52530 - 1	0·6708	1·0055	1·3406	1·6758	2·0110	2·3461	2·6813	3·0164
0·85763 - 1	1·4410	2·1616	2·8821	3·6026	4·3231	5·0436	5·7642	6·4847
0·80058 - 1	1·2635	1·8953	2·5270	3·1588	3·7905	4·4223	5·0540	5·6858
0·91142 - 1	1·6311	2·4466	3·2621	4·0777	4·8932	5·7087	6·5242	7·3398
0·80072 - 2	0·1263	0·1895	0·2527	0·3159	0·3790	0·4422	0·5054	0·5685
0·15776 - 1	0·2877	0·4315	0·5754	0·7192	0·8630	1·0069	1·1507	1·2946
0·44467 - 1	0·5568	0·8351	1·1135	1·3919	1·6703	1·9487	2·2270	2·5054
0·80455 - 1	1·2751	1·9127	2·5503	3·1879	3·8254	4·4630	5·1006	5·7381
0·80072 - 1	1·2641	1·8961	2·5282	3·1602	3·7922	4·4243	5·0563	5·6884
0·28578 - 1	0·3862	0·5793	0·7724	0·9655	1·1586	1·3517	1·5448	1·7379
0·48515 - 1	0·6112	0·9168	1·2224	1·5280	1·8336	2·1392	2·4448	2·7504
0·55279 - 1	0·7142	1·0713	1·4284	1·7855	2·1426	2·4997	2·8568	3·2139
0·73304 - 1	1·0817	1·6225	2·1634	2·7042	3·2450	3·7859	4·3267	4·8676
0·64028 - 1	0·8737	1·3105	1·7473	2·1842	2·6210	3·0578	3·4946	3·9315
0·76738 - 1	1·1706	1·7559	2·3412	2·9265	3·5118	4·0971	4·6824	5·2677
0·73493 - 1	1·0615	1·5923	2·1231	2·6539	3·1846	3·7154	4·2462	4·7769
0·80455 - 1	0·2747	0·4120	0·5493	0·6867	0·8240	0·9613	1·0986	1·2360
0·13767 - 1	0·5488	0·8232	1·0976	1·3720	1·6463	1·9207	2·1951	2·4695
0·43338 - 1	0·6859	1·0288	1·3717	1·7147	2·0576	2·4005	2·7434	3·0864
0·53517 - 1	0·8402	1·2603	1·6804	2·1005	2·5206	2·9407	3·3608	3·7809
0·78455 - 1	1·2179	1·8268	2·4357	3·0447	3·6536	4·2625	4·8714	5·4804
0·90493 - 1	1·6069	2·4103	3·2138	4·0172	4·8206	5·6241	6·4275	7·2310
0·82672 - 1	1·3421	2·0131	2·6842	3·3552	4·0262	4·6973	5·3683	6·0394
0·92179 - 1	1·6704	2·5056	3·3408	4·1761	5·0113	5·8465	6·6817	7·5169

TABLE 4. — DENSITY OF GASES AND VAPOURS
And Litre Weights at 0° C., and at a pressure of 760 mm.

grm. mol. of each gas = 22·412 litres. 1 litre of each gas = 0·04463 × its molecular weight. The spec. gravity of gases referred to atmospheric air as unity is = its molecular weight divided by 28·97, or = $\frac{84·52 \times \text{molec. weight}}{1000}$.

Gas.	Formula.	Molecular Weight.	Weight of 1 litre in grams.		Density, air = 1.		Observer.
			Calculated.	Observed.	Calculated.	Observed.	
Acetylene . . .	C ₂ H ₂	26·02	1·1610	1·189	0·8981	0·92	Berthelot.
Ammonia . . .	NH ₃	17·03	0·7599	0·7719	0·5878	0·5971	Leduc.
Atmospheric air	1·2928	...	1·0000
Bromine . . .	Br ₂	159·92	7·1354	7·1418	5·5193	5·5243	(at 228°) Jahn.
Chlorine . . .	Cl ₂	70·90	3·1635	3·2191	2·4470	2·490	Treadwell.
Carbon monoxide . . .	CO	28·00	1·2493	1·2503	0·9664	0·96709	Rayleigh, Leduc.
Carbon dioxide . . .	CO ₂	44·00	1·9632	1·9766	1·5186	1·52892	Rayleigh, Leduc.
Ethylene . . .	C ₂ H ₄	28·03	1·2507	1·2737	0·9674	0·9852	Saussure.
Hydrogen . . .	H ₂	2·02	0·0901	0·08998	0·06969	0·06960	Rayleigh.
Hydrogen chloride . . .	HCl	36·46	1·6268	1·6408	1·2583	1·2692	Leduc.
Methane . . .	CH ₄	16·03	0·7152	0·7209	0·5532	0·5576	Thomson.
Nitrogen . . .	N ₂	28·02	1·2502	1·2505	0·9670	0·96727	Rayleigh, Leduc.
Nitrous oxide . . .	N ₂ O	44·02	1·9641	1·9781	1·5192	1·5301	Leduc.
Nitric oxide . . .	NO	30·01	1·3390	1·3402	1·0357	1·0357	Gray, Guye and Davila.
peroxide . . .	NO ₂	46·01	2·0529	...	1·5879
Oxygen . . .	N ₂ O ₄	92·02	4·1058	...	3·1758
Sulphur . . .	O ₂	32·00	1·4278	1·4289	1·1044	1·10529	Rayleigh, Leduc.
Sulphuretted hydrogen . . .	S ₂	64·12	2·8610	...	2·2130
Sulphur dioxide . . .	H ₂ S	34·08	1·5206	1·5878	1·1762	1·1895	Leduc.
Sulphur trioxide . . .	SO ₂	64·06	2·8583	2·9268	2·2109	2·2639	Leduc.
Water . . .	SO ₃	80·06	3·5722	...	2·7681
	H ₂ O	18·02	0·8040	...	0·6219

TABLE 5.—CALCULATION OF THE C.C. READ OFF IN GAS-VOLUMETRIC ANALYSIS, TO MILLIGRAMS OF THE SUBSTANCE REQUIRED.

N.B.—The data for this calculation are not the theoretically calculated, but the observed densities of the gases, according to Table 4.

c.c. at 0° and 760 mm.	1.	log	2.	3.	4.	5.	6.	7.	8.	9.
CO ₂ = mg CO ₂ .	1·9766	0·29592	3·9532	5·9298	7·9064	9·8830	11·8596	13·8362	15·8128	17·7894
CO ₂ = mg CaCO ₃	4·4968	0·65290	8·9936	13·4904	17·9872	22·4840	26·9808	31·4776	35·9744	40·4712
O = mg O	1·4289	0·15500	2·8578	4·2867	5·7156	7·1445	8·5734	10·0023	11·4312	12·8601
(O = mg O)*	0·7145	0·85400 - 1	1·4289	2·1434	2·8578	3·5723	4·2867	5·0012	5·7156	6·4301
O = mg MnO ₂ .	3·8850	0·58939	7·7700	11·6550	15·5400	19·4250	23·3100	27·1950	31·0800	34·9650
O = mg Cl	3·1661	0·50052	6·3322	9·4983	12·6644	15·8305	18·9966	22·1627	25·3288	28·4949
N = mg N	1·2505	0·09709	2·5010	3·7515	5·0020	6·2525	7·5030	8·7535	10·0040	11·2545
N = mg NH ₃ .	1·5200	0·18184	3·0400	4·5600	6·0800	7·6000	9·1200	10·6400	12·1600	13·6800
(N = mg N)†	1·2818	0·10782	2·5636	3·8454	5·1272	6·4090	7·6908	8·9726	10·2544	11·5362
(N = mg NH ₃)†	1·5582	0·19263	3·1164	4·6746	6·2328	7·7910	9·3492	10·9074	12·4656	14·0238
NO = mg N	0·6257	0·79637 - 1	1·2514	1·8771	2·5028	3·1285	3·7542	4·3799	5·0056	5·6313
NO = mg NO	1·3402	0·12717	2·6804	4·0206	5·3608	6·7010	8·0412	9·3814	10·7216	12·0618
NO = mg N ₂ O ₃	1·6975	0·22881	3·3950	5·0925	6·7900	8·4875	10·1850	11·8825	13·5800	15·2775
NO = mg HNO ₃	2·8144	0·44938	5·6288	8·4432	11·2576	14·0720	16·8864	19·7008	22·5152	25·3296
NO = mg NaNO ₃	3·7986	0·57962	7·5972	11·3958	15·1944	18·9930	22·7916	26·5902	30·3888	34·1874
Cl = mg Cl	3·2191	0·50773	6·4382	9·6578	12·8764	16·0955	19·3146	22·5337	25·7528	28·9719
H ₂ S = mg H ₂ S .	1·5378	0·18690	3·0756	4·6134	6·1512	7·6890	9·2268	10·7646	12·3024	13·8402

* In the case of the hydrogen peroxide methods, where only half of the oxygen liberated comes from the substance analysed.

† In the case of the azotometric methods, where the potassium-bromate method yields 2·5 per cent. too little nitrogen.

TABLE 6.—SOLUBILITY OF SALTS.

Note.—The solubility is given in parts of the anhydrous salt dissolved by 100 parts of water.

100 parts of Water dissolve	At 15°.	At 100° C.	100 parts of Water dissolve	At 15°.	At 100° C.
Alum, ammonium	5.5	109.7 (95°)	Potassium hydrate	200	791
potassium	5	154	chromate (neutral)	62	102
Aluminium sulphate	33	89	bichromate	10.5	16
Ammonium oxalate	4.5	40.8	oxalate (acid)	2.5	32 (75°)
nitrate	163	871	permanganate	5.4	deliquescent
Barium chloride	34.5	60	thiosulphate	0.46	6.9
hydroxide	2.8	140	bitartrate	150	300
nitrate	8.1	34.2	tartrate (neutral)	122	...
Boric acid	2	21	cyanide	22	75
Bromine	3.6	0.002	ferrocyanide	40	77.5
Calcium carbonate	0.0013	...	ferrocyanide	140	209
hydroxide	0.129	0.05	iodide	35	150
nitrate	110	830	Sodium acetate	4	55
Copper acetate	7	19.8	borate	87	126.5
nitrate	100	250	bromide	174	302
sulphate	19.3	70.5	iodide	61	...
Ferric chloride	87	535.7	hydrate	50	more than 200
Ferrous sulphate	24	43 (90°)	thiosulphate	5	100
Lead acetate	46	71	phosphate (ordinary)	24	33
chloride	0.9	3.8	sulphite	0.57	22.85
nitrate	48	127	Strontium hydrate	62	101.5
sulphate	.004	...	nitrate	56.5	101.9
Magnesium oxide	.0008	.004	chloride	182	848
carbonate	.01	...	Tartaric acid	270	...
Manganous chloride	70	116	Tin (stannous) chloride		
Oxalic acid	7	100			

TABLE 7.—SOLUBILITY OF OTHER SALTS IN WATER AT VARIOUS TEMPERATURES.

Interpolated from the values given in Landolt-Börnstein-Meyerhoffer's Tables, No. 176.

100 parts of Water dissolve	At 0°.	At 15°.	At 30°.	At 50°.	At 100°.	Observer.
Ammonium sulphate	31·8	34·6	40·4	52·1	89·1	Poggiale.
bicarbonate	11·9	17·3	27	Dibbits.
chloride	29·7	35·1	41·4	50·4	77·3	Mulder.
sulphate	70·6	74·2	78·0	84·1	103·3	Mulder.
Calcium chloride	59·5	68	102·7	134	154	Roozeboom.
sulphate	0·176	0·199	0·210	0·207	0·17	Hulett and Allen.
Magnesium chloride	52·8	54	56	60	73	Van't Hoff, Meyerhoffer.
sulphate	26·0	33·2	40·9	50·4	68·5	Loewel, Mulder, Meyerhoffer.
Potassium chlorate	3·3	5·9	10·1	19·7	56	Gay-Lussac.
chloride	28·5	32·6	37·3	42·9	56·6	Andreas, Mulder.
hydroxide	97	107	126	140	178	Pickering.
nitrate	13·3	25·7	45·9	85·5	246	Andreas, Berkeley.
sulphate	7·4	10·2	13·6	16·5	24·1	Andreas, Berkeley, Trevor.
Sodium bicarbonate	6·9	8·9	11·1	14·5	...	Dibbits.
carbonate	7·1	16	40·9	47·5	45·1	Mulder, Loewel, Epple.
chlorate	82	94	111	135	204	Kremers, Graebe.
chloride	35·63	35·75	36·03	36·67	39·12	Andreas, Berkeley.
hydroxide	42	63·5	119	145	340	Pickering.
nitrate	73	84·2	96·2	114	175·5	Berkeley.
sulphate	5·0	13·2	40	46·8	42·7	Loewel, Gay-Lussac.
tetraborate (borax)	1·1	1·9	3·9	10·5	52·3	Horn and van Wegener.
thiosulphate	52·5	65·5	84·7	169·7	266	Taylor.
Zinc chloride	208	350	435	470	615	Mylus and Dietz.
sulphate	41·9	50·9	62	76·8	78·5	Cohen, Callendar & Barnes, Etard.

TABLE 8.—SOLUBILITY OF GASES IN WATER.

Column *a* gives the volume of gas (reduced to 0° and 760 mm.) dissolved by one volume of the liquid at the temperature indicated, if the partial pressure of the gas is = 760 mm. Hg.

Column *q* gives the weight of the substance in grams, dissolved by 100 gr. of the pure solvent, if the partial pressure of the gas + the vapour pressure of the liquid at the temperature indicated = 760 mm. Hg.

The letters following the name of the gas indicate the observer, viz., W. = Winkler; B. & B. = Bohr & Bock; F. = Fauser; R. = Raoult; S. = Schönfeld; R.-D. = Roscoe-Dittmar; R. = Roozeboom; B. = Bunsen.

T.	Oxygen, W.		Hydrogen, W.		Nitrogen, B. & B.		Chlorine, W.	
	<i>a.</i>	<i>q.</i>	<i>a.</i>	<i>q.</i>	<i>a.</i>	<i>q.</i>	<i>a.</i>	<i>q.</i>
0	·04890	·006948	·02148	·0001922	·02388	·002977
1	·04759	·006758	·02126	·0001902	·02337	·002912
2	·04633	·006576	·02105	·0001882	·02288	·002843
3	·04512	·006401	·02084	·0001862	·02241	·002790
4	·04397	·006234	·02064	·0001843	·02196	·002732
5	·04286	·006074	·02044	·0001824	·02153	·002677
6	·04181	·005920	·02025	·0001806	·02111	·002624
7	·04080	·005775	·02007	·0001789	·02070	·002570
8	·03983	·005633	·01989	·0001772	·02031	·002520
9	·03891	·005499	·01972	·0001756	·01993	·002472
10	·03802	·005370	·01955	·0001739	·01956	·002424	3·095	·9969
11	·03718	·005248	·01940	·0001725	·01920	·002378	2·996	·9652
12	·03637	·005129	·01925	·0001710	·01885	·002333	2·900	·9344
13	·03560	·005011	·01911	·0001696	·01851	·002289	2·808	·9048
14	·03486	·004908	·01897	·0001682	·01818	·002246	2·720	·8766
15	·03415	·004804	·01883	·0001669	·01786	·002205	2·635	·8493
16	·03347	·004703	·01869	·0001654	·01755	·002164	2·553	·8230
17	·03283	·004609	·01856	·0001641	·01725	·002125	2·474	·7977
18	·03220	·004515	·01844	·0001630	·01698	·002089	2·399	·7736
19	·03161	·004428	·01831	·0001616	·01667	·002049	2·328	·7508
20	·03102	·004339	·01819	·0001604	·01639	·002012	2·260	·7291
21	·03044	·004253	·01806	·0001590	·01611	·001975	2·200	·7098
22	·02988	·004169	·01792	·0001575	·01584	·001940	2·143	·6916
23	·02934	·004088	·01779	·0001561	·01557	·001903	2·087	·6737
24	·02881	·004009	·01766	·0001548	·01530	·001868	2·035	·6570
25	·02831	·003932	·01754	·0001534	·01504	·001832	1·985	·6411
26	·02783	·003859	·01742	·0001522	·01478	·001798	1·937	·6257
27	·02736	·003787	·01731	·0001509	·01453	·001764	1·891	·6110
28	·02691	·003717	·01720	·0001497	·01428	·001731	1·848	·5973
29	·02649	·003653	·01709	·0001485	·01404	·001699	1·808	·5845
30	·02608	·003588	·01699	·0001470	·01380	·001666	1·769	·5722
35	·02440	·003315	·01666	·0001426	·01271	·001516	1·575	·5103
40	·02306	·003081	·01644	·0001385	·01182	·001386	1·414	·4589
45	·02187	·002860	·01624	·0001338	·01111	·001275	1·300	·4227
50	·02090	·002657	·01608	·0001288	·01061	·001184	1·204	·3927
60	·01946	·002274	·01600	·0001178	·01000	·001026	1·006	·3294
70	·01833	·001857	·01600	·0001021	0·848	·2792
80	·01761	·001381	·01600	·0000790	0·672	·2226
90	·01723	·000787	·01600	·0000461	0·380	·1268
100	·01700	·000000	·01600	·0000000	·01000	·000000	0·000	·0000

TABLE 8—Continued.

T.	Carbon monoxide, W.		Carbon dioxide, B. & B.		Hydrogen sulphide, F.		Ammonia, R.	
	a.	q.	a.	q.	a.	q.	a.	q.
0	0·03537	0·004397	1·713	0·3347	4·686	0·710	1298·9	98·7
1	0·03455	0·004293	1·646	0·3214	4·555	0·689	1220·2	92·7
2	0·03375	0·004192	1·584	0·3091	4·428	0·670	1154·7	87·7
3	0·03297	0·004092	1·527	0·2979	4·303	0·651	1100·9	83·6
4	0·03222	0·003997	1·473	0·2872	4·182	0·632	1053·0	79·9
5	0·03149	0·003904	1·424	0·2774	4·063	0·615	1019·5	77·3
6	0·03078	0·003814	1·377	0·2681	3·948	0·596	997·2	75·6
7	0·03009	0·003726	1·331	0·2590	3·836	0·579	974·9	73·9
8	0·02942	0·003641	1·282	0·2494	3·728	0·562	954·5	72·3
9	0·02878	0·003560	1·237	0·2404	3·622	0·546	933·0	70·6
10	0·02816	0·003481	1·194	0·2319	3·520	0·530	910·4	68·9
11	0·02757	0·003416	1·154	0·2240	3·421	0·515	888·0	67·2
12	0·02701	0·003333	1·117	0·2166	3·325	0·500	865·6	65·5
13	0·02646	0·003260	1·083	0·2099	3·232	0·485	843·2	63·7
14	0·02593	0·003188	1·050	0·2033	3·142	0·471	822·1	62·1
15	0·02543	0·003130	1·019	0·1971	3·056	0·458	802·4	60·6
16	0·02494	0·003065	0·985	0·1904	2·973	0·445	783·2	59·1
17	0·02448	0·003007	0·956	0·1845	2·893	0·433	764·1	57·6
18	0·02402	0·002943	0·928	0·1789	2·816	0·421	744·3	56·1
19	0·02360	0·002893	0·902	0·1736	2·742	0·409	725·8	54·7
20	0·02319	0·002839	0·878	0·1689	2·672	0·398	710·6	53·5
21	0·02281	0·002789	0·854	0·1641	690·2	51·9
22	0·02244	0·002739	0·829	0·1591	674·3	50·6
23	0·02208	0·002691	0·804	0·1541	661·0	49·6
24	0·02174	0·002647	0·781	0·1494	647·8	48·6
25	0·02142	0·002603	0·759	0·1450	634·6	47·6
26	0·02110	0·002560	0·738	0·1407	621·3	46·5
27	0·02080	0·002519	0·718	0·1367	608·1	45·5
28	0·02051	0·002479	0·699	0·1328	594·8	44·4
29	0·02024	0·002442	0·682	0·1293
30	0·01998	0·002405	0·665	0·1259
35	0·01877	0·002231	0·592	0·1106
40	0·01775	0·002076	0·530	0·0974
45	0·01690	0·001934	0·479	0·0862
50	0·01615	0·001797	0·436	0·0762
60	0·01488	0·001521	0·359	0·0577
70	0·01440	0·001276
80	0·01430	0·000981
90	0·01420	0·000568
100	0·01410	0·000000

TABLE 8—Continued.

T.	Sulphur dioxide, S.		Hydrogen chloride, H.-D.		Methane, W.	
	a.	q.	a.	q.	a.	q.
0	79·789	22·83	506·7	82·5	0·05563	0·008959
1	77·210	22·09	0·05401	0·008342
2	74·691	21·37	499·8	81·4	0·05244	0·008729
3	72·230	20·67	0·05098	0·008620
4	69·828	19·98	493·7	80·4	0·04946	0·008514
5	67·485	19·31	0·04805	0·008411
6	65·200	18·66	486·9	79·3	0·04669	0·008312
7	62·973	18·02	0·04539	0·008218
8	60·805	17·40	480·8	78·3	0·04413	0·008127
9	58·697	16·80	0·04292	0·008039
10	56·647	16·21	473·9	77·2	0·04177	0·007956
11	54·655	15·64	0·04072	0·007880
12	52·723	15·09	467·7	76·2	0·03970	0·007805
13	50·849	14·56	0·03872	0·007733
14	49·033	14·04	461·5	75·2	0·03779	0·007666
15	47·276	13·54	0·03690	0·007600
16	45·578	13·05	455·2	74·2	0·03606	0·007538
17	43·939	12·59	0·03525	0·007479
18	43·360	12·14	448·3	73·1	0·03446	0·007422
19	40·838	11·70	0·03376	0·007369
20	39·374	11·29	442·0	72·1	0·03308	0·007319
21	37·970	10·89	0·03243	0·007270
22	36·617	10·50	435·0	71·0	0·03180	0·007223
23	35·302	10·13	0·03119	0·007178
24	34·026	9·76	428·7	70·0	0·03061	0·007134
25	32·786	9·41	0·03006	0·007092
26	31·584	9·07	423·0	69·1	0·02952	0·007051
27	30·422	8·43	0·02901	0·007012
28	29·314	8·42	417·2	68·2	0·02852	0·006974
29	28·210	8·10	0·02806	0·006939
30	27·161	7·81	411·5	67·3	0·02762	0·006905
35	22·489	6·47	0·02546	0·006732
40	18·766	5·41	387·7	63·3	0·02369	0·006586
50	361·6	59·6	0·02134	0·006359
60	338·7	56·1	0·01954	0·006145
70	0·01825	0·005926
80	0·01770	0·005695
90	0·01735	0·005398
100	0·01700	0·005000

TABLE 8—Continued.

T.	Ethylene, W.		Acetylene, W.		Air, W.		Nitrous oxide, in Alcohol, B.
	a.	g.	a.	g.	a.		a.
0	0.226	0.0281	1.73	0.20	0.02881	...	4.1780
1	0.219	0.0272	1.68	0.19	0.02808	...	4.1088
2	0.211	0.0262	1.63	0.19	0.02738	...	4.0409
3	0.204	0.0254	1.58	0.18	0.02670	...	3.9741
4	0.197	0.0245	1.53	0.18	0.02606	...	3.9085
5	0.191	0.0237	1.49	0.17	0.02543	...	3.8442
6	0.184	0.0228	1.45	0.17	0.02482	...	3.7811
7	0.178	0.0221	1.41	0.16	0.02424	...	3.7192
8	0.173	0.0214	1.37	0.16	0.02369	...	3.6585
9	0.167	0.0207	1.34	0.15	0.02316	...	3.5990
10	0.162	0.0200	1.31	0.15	0.02264	...	3.5408
11	0.157	0.0194	1.27	0.15	0.02217	...	3.4838
12	0.152	0.0188	1.24	0.14	0.02171	...	3.4279
13	0.148	0.0183	1.21	0.14	0.02127	...	3.3734
14	0.143	0.0176	1.18	0.14	0.02085	...	3.3200
15	0.139	0.0171	1.15	0.13	0.02045	...	3.2678
16	0.136	0.0167	1.13	0.13	0.02005	...	3.2169
17	0.132	0.0162	1.10	0.13	0.01970	...	3.1672
18	0.129	0.0158	1.08	0.12	0.01935	...	3.1187
19	0.125	0.0153	1.05	0.12	0.01901	...	3.0714
20	0.122	0.0150	1.03	0.12	0.01869	...	3.0253
21	0.119	0.0146	1.01	0.12	0.01838	...	2.9805
22	0.116	0.0142	0.99	0.11	0.01808	...	2.9368
23	0.114	0.0139	0.97	0.11	0.01779	...	2.8944
24	0.111	0.0135	0.95	0.11	0.01751	...	2.8532
25	0.108	0.0131	0.93	0.11	0.01724
26	0.106	0.0129	0.91	0.10	0.01698
27	0.104	0.0126	0.89	0.10	0.01674
28	0.102	0.0123	0.87	0.10	0.01650
29	0.100	0.0121	0.85	0.10	0.01627
30	0.098	0.0118	0.84	0.09	0.01606
...	0.01503
...	0.01418
...	0.01297
...	0.01216
...	0.01156
...	0.01126
...	0.01113
...	0.01105



TABLE 9.—SPECIFIC GRAVITIES OF SOLIDS.

Alumina, anhydrous	4·15	Calcespar	2·72
Alum, ammonium	1·626	Cannel coal	1·16-1·27
potassium	1·724	Cement	2·7-3·05
Aluminium sulphate,		China clay, kaolin	2·21
cryst.	1·596	Charcoal, organic	1·57
Aluminium	2·76	wood	0·3-0·5
Alum stone	2·8	Coke, porous	0·4
Ammonium nitrate	1·707	Coal, porous	1·16-1·63
sulphate	1·77	Copper, metallic, cast	8·726
chloride	1·528	hammered	8·94
Anhydrite (CaSO ₄)	2·96	pyrites	4·1-4·3
Anthracite	1·4-1·7	oxide	6·43
Antimony	6·7	sulphate	2·27
Arsenious acid	3·884	Cuprous sulphide	5·97
Arsenic acid	4·250	Clay	1·8-2·6
Asphalt	1·1-1·2	Cryolite	2·96
Ash wood	0·7-0·8	Elm wood	0·67
Barium chloride, cryst.	2·664	Fat, animal	0·92
carbonate	4·56	Felspar	2·5-2·6
sulphate (spar)	4·73	Fibres, vegetable	1·51
hydroxide, cryst.	1·66	Fir wood, dry	0·6
Bauxite		Firebricks	1·85
Basalt	2·8-3·2	Flint	2·7
Beech wood, dry	0·7-0·8	Glass, green	2·642
Birch wood, dry	0·7-0·8	plate	2·450
Bismuth	9·85	crystal, Bohem.	2·9-3·0
Borate of magnesium		flint, English	3·4-3·44
(boracite)	2·9	Glauber's salt, cryst.	1·52
Borax, crystallised	1·692	anhydrous	2·63
Boric acid, crystallised	1·479	Granite	2·5-2·9
fused	1·830	Gypsum, plaster-of-Paris	2·322
Brown coal, lignite	1·2-1·4	cast, dry	·97
Brickwork	1·5-1·7	Heavy spar	4·3-4·48
Bricks, ordinary	1·4-2·2	Iodine	4·948
Brass	8·4-8·7	Iron, wrought	7·4-7·9
Calamine	4·1-4·5	grey, cast	6·6-7·3
Chalk	1·8-2·7	white, cast	7·1-7·9
Calcium chloride, cryst.	1·612	peroxide	5·22
chloride, anhydrous	2·240	hydrated oxide	3·94
silicate	2·9	magnetic oxide	5·4
carbonate	2·7	carbonate	3·87
phosphate	3·18	sulphate, cryst.	1·904
sulphate, anhydrous	2·927	pyrites, white	4·65-4·88

TABLE 9—Continued.

Iron, pyrites	5·18	Potassium, nitrate	2·058
Larch wood	0·44-0·5	sulphate	2·66
Lignite	1·2-1·4	bisulphate	2·277
Lime, burnt, quick-	3·08	hydroxide	2·044
Lime wood	0·5	Quartz	2·7
Litharge	9·36	Resin	1·07
Lead, cast	11·3	Rock salt	2·1-2·2
red	8·62	Sal-ammoniac	1·528
chromate	6·00	Sand, dry	1·4-1·6
acetate, cryst.	2·395	damp	1·9-2·0
carbonate	6·47	Sandstone	1·9-2·5
nitrate	4·40	Silver	10·6
sulphide	7·505	Silver chloride	5·501
sulphate	6·169	Slate	2·7
chloride	5·802	Sodium carbonate, anh.	2·509
Magnesia, calcined	3·2	carbonate, cryst.	1·454
carbonate	2·94	chloride	2·078
Magnesite	2·9-3·1	nitrate	2·226
Magnesium sulph., cryst.	1·751	sulphate	2·63
chloride, cryst.	1·558	sulphide	2·471
Manganese peroxide	2·94	thiosulphate	1·736
native ore	4·7-5·0	hydroxide	2·130
Maple wood	0·5-0·6	Steel	7·80
Marble	2·5-2·8	Steel, cast	7·92
Nickel	8·9	hardened	7·66
Oak, dry	0·85-0·95	Sulphur, native	2·069
Phosphorus, yellow	1·826	sticks, fresh	1·98
red	2·106	sticks, old	2·05
Pine wood, white	0·55	soft, amorphous	1·96
red	0·5	Sulphuric anhydride	1·97
Platinum	21·1	Tin, cast	7·21-7·4
Pock wood	1·268	hammered	7·475
Poplar	0·38	Willow wood	0·5-0·58
Porcelain	2·1-2·5	Witherite	4·30
Porphyry	2·8	Zinc, cast	6·8
Potash, natural	2·3	rolled	7·2
Potassium carbonate	2·264	blende	3·9-4·2
chlorate	2·35	oxide	5·73
chloride	1·945	sulphate	2·036
chromate	2·603		

TABLE 10.—WEIGHT OF SUBSTANCES AS STORED.

Substance.	1 Cubic Metre Weighs	1 Cubic Foot Weighs	Tons per Cub. Foot.
	Kilo.	lb. avdp.	
Bricks	2100	131	•0584
Cement	1200	75	•0335
Clay, damp	1650	103	•0459
dry	1570	98	•0437
Limestone and other building stones .	2000	125	•0558
Mortar (lime and sand)	1800	112	•0500
Quicklime	1000	62•5	•0279
Sand, dry	1330	83	•0370
damp	1770	110	•0491
Wood, beech logs	400	24•5	•0107
fir logs	330	20•5	•0091
oak logs	420	26	•0116
<i>Raw Materials, etc., for Alkali Works.</i>			
Pyrites, broken pieces	2500	156	•0696
smalls	2340	146•5	•0654
burnt	1520	95•0	•0424
Nitre	1310	81•5	•0364
Nitre cake (acid sulphate of soda) .	1335	83	•0375
Salt	689	43	•0192
Saltcake	1180	73•5	•0328
Limestone (small pieces)	1400	87•5	•0391
Black ash (lumps)	962	60	•0268
Alkali waste (wet)	1268	79	•0352
Soda salts ($\text{Na}_2\text{CO}_3 + \text{H}_2\text{O}$) (drained) .	810	50•5	•0225
Soda ash (unground)	1195	74•5	•0332
Soda crystals	1010	63	•0281
Bicarbonate (ground)	986	61•5	•0274
Quicklime (small lumps)	1058	66	•0295
Sieved lime (for bleaching powder) .	497-593	31-37	•0151
Bleaching powder	721-834	45-52	•0216
Manganese dioxide, native	2210	138	•0616
Limestone dust	1550	96•5	•0431
Coke (for filling towers)	417-534	26-33	•0131
Flints	1600	100	•0446
Cinders (ashes)	738	46	•0205

TABLE 11.—SPECIFIC GRAVITY OF LIQUIDS.

	Specific Gravity.	Temp.
Acetic anhydride	1·004	17°
Acetone	0·81	...
Alcohol	0·7939	12°·5
Acetic acid	1·064	17°
Bisulphide of carbon	1·272	...
Benzene	0·884	15°·5
Coal tar	1·15	15°
Ether	0·723	12°·5
Glycerine	1·260	15°
Linseed oil	0·9347	15°
Mercury	13·596	0°
Nitrogen peroxide (liquid)	1·45	...
Olive oil	0·917	15°
Petroleum	0·78-0·81	15°
Rapeseed oil	0·9136	15°
Sulphur dioxide (liquid)	1·45	20°
Sea water	1·02-1·04	15°
Spirits of turpentine	0·865	15°

TABLE 12.—SPECIFIC GRAVITY AND PERCENTAGE OF SATURATED SOLUTIONS.

The percentage refers to Anhydrous Salt.

	Temperature.	Percentage of Salt.	Specific Gravity.	Degrees Twaddell.
Ammonium chloride	15	26·30	1·0776	15·5
sulphate	19	50·00	1·2890	57·8
Barium chloride	15	25·97	1·2827	56·5
Calcium chloride	15	40·66	1·4110	82·2
Magnesium sulphate	15	25·25	1·2880	57·6
Potassium chloride	15	24·90	1·1723	34·4
carbonate	15	52·02	1·5708	114
nitrate	15	21·07	1·1441	28·8
sulphate	15	9·92	1·0831	16·6
Sodium chloride	15	26·395	1·2043	40·8
carbonate	15	14·35	1·1535	30·7
nitrate	19·5	46·25	1·3804	76
sulphate	15·0	11·95	1·1117	22·3

TABLE 13. — LINEAR EXPANSION OF SUBSTANCES.

By variation of temperature from 0° to 100° C. (32°-212° F.).

Brass	0·001868	1 : 535
Charcoal from oak	0·001200	1 : 833
fir	0·00100	1 : 1000
Copper	0·001718	1 : 582
Glass, flint	0·000817	1 : 1219
white	0·000861	1 : 1161
green	0·000766	1 : 1305
Gold	0·001466	1 : 682
Iron, wrought	0·001235	1 : 812
cast	0·001110	1 : 901
Lead	0·002848	1 : 351
Marble of Carrara	0·000849	1 : 1178
St Beat	0·000418	1 : 2392
Platinum	0·000884	1 : 1132
Silver	0·001908	1 : 524
Solder, hard	0·002058	1 : 486
Steel, hardened	0·001240	1 : 807
not hardened	0·001079	1 : 927
Tin	0·001938	1 : 516
Water	0·015538	1 : 71·4
Zinc	0·002942	1 : 340

TABLE 14.—COMPARISON OF THERMOMETRIC SCALES.

$$t^{\circ}\text{C} = \frac{5}{9}t^{\circ}\text{R} = \frac{5}{9}t + 32^{\circ}\text{F}; \quad t^{\circ}\text{R} = \frac{5}{4}t^{\circ}\text{C} = \frac{5}{4}t + 32^{\circ}\text{F}; \quad t^{\circ}\text{F} = \frac{9}{5}(t - 32^{\circ})\text{C} = \frac{9}{5}(t - 32^{\circ})\text{R}.$$

Celsius' (Centigrade) degrees as units.

Cels.	Réau.	Fahr.	Cels.	Réau.	Fahr.	Cels.	Réau.	Fahr.	Cels.	Réau.	Fahr.	Cels.	Réau.	Fahr.
-40	-32	-40	-16	-12.8	+3.2	+8	+6.4	+46.4	+32	+25.6	+89.6	+55	+44	+131
39	31.2	38.2	15	12	5	9	7.2	48.2	33	26.4	91.4	56	44.8	132.8
38	30.4	36.4	14	11.2	6.8	10	8	50	34	27.2	93.2	57	45.6	134.6
37	29.6	34.6	13	10.4	8.6	11	8.8	51.8	35	28	95	58	46.4	136.4
36	28.8	32.8	12	9.6	10.4	12	9.6	53.6	36	28.8	96.8	59	47.2	138.2
35	28	31	11	8.8	12.2	13	10.4	55.4	37	29.6	98.6	60	48	140
34	27.2	29.2	10	8	14	14	11.2	57.2	38	30.4	100.4	61	48.8	141.8
33	26.4	27.4	9	7.2	15.8	15	12	59	39	31.2	102.2	62	49.6	143.6
32	25.6	25.6	8	6.4	17.6	16	12.8	60.8	40	32	104	63	50.4	145.4
31	24.8	23.8	7	5.6	19.4	17	13.6	62.6	41	32.8	105.8	64	51.2	147.2
30	24	22	6	4.8	21.2	18	14.4	64.4	42	33.6	107.6	65	52	149
29	23.2	20.2	5	4	23	19	15.2	66.2	43	34.4	109.4	66	52.8	150.8
28	22.4	18.4	4	3.2	24.8	20	16	68	44	35.2	111.2	67	53.6	152.6
27	21.6	16.6	3	2.4	26.6	21	16.8	69.8	45	36	113	68	54.4	154.4
26	20.8	14.8	2	1.6	28.4	22	17.6	71.6	46	36.8	114.8	69	55.2	156.2
25	20	13	1	0.8	30.2	23	18.4	73.4	47	37.6	116.6	70	56	158
24	19.2	11.2	0	0	32	24	19.2	75.2	48	38.4	118.4	71	56.8	159.8
23	18.4	9.4	+1	+0.8	33.8	25	20	77	49	39.2	120.2	72	57.6	161.6
22	17.6	7.6	2	1.6	35.6	26	20.8	78.8	50	40	122	73	58.4	163.4
21	16.8	5.8	3	2.4	37.4	27	21.6	80.6	51	40.8	123.8	74	59.2	165.2
20	16	4	4	3.2	39.2	28	22.4	82.4	52	41.6	125.6	75	60	167
19	15.2	2.2	5	4	41	29	23.2	84.2	53	42.4	127.4	76	60.8	168.8
18	14.4	0.4	6	4.8	42.8	30	24	86	54	43.2	129.2	77	61.6	170.6
17	13.6	+1.4	7	5.6	44.6	31	24.8	87.8

TABLE 14b.—FAHRENHEIT DEGREES AS UNITS.

Fah.	Cel.	Réau.	Fah.	Cel.	Réau.	Fah.	Cel.	Réau.	Fah.	Cel.	Réau.	Fah.	Cel.	Réau.	Fah.	Cel.	Réau.			
-40	-40.0	-32.0	-	8	-19.4	+28	+0.6	+0.4	+69	+20.6	+16.4	+105	+40.6	+82.4	+141	+60.6	+48.4	+177	+80.6	+64.4
89	89.4	81.6	-	2	18.9	34	1.1	0.9	70	21.1	16.9	106	41.1	32.9	142	61.1	48.9	178	81.1	64.9
88	88.9	81.1	1	18.8	14.7	85	1.7	1.8	71	21.7	17.8	107	41.7	33.8	148	61.7	49.8	179	81.7	65.8
87	88.8	80.7	0	17.8	14.2	86	2.2	1.8	72	22.2	17.8	108	42.2	33.8	144	62.2	49.8	180	82.2	66.8
86	87.8	80.2	1	17.2	18.8	87	2.8	2.2	73	22.8	18.2	109	42.8	34.2	145	62.8	50.2	181	82.8	66.2
85	87.2	80.8	2	16.7	18.8	88	3.8	2.7	74	23.8	18.7	110	43.8	34.7	146	63.8	50.7	182	83.8	66.7
84	86.7	80.3	3	16.1	12.9	89	8.9	8.1	75	28.9	19.1	111	48.9	35.1	147	68.9	51.1	188	88.9	67.1
83	86.1	80.8	4	15.6	12.4	40	4.4	3.6	76	24.0	19.6	112	44.4	35.6	148	64.4	51.6	184	84.4	67.6
82	85.6	80.4	5	15.0	12.0	41	5.0	4.0	77	25.0	20.0	118	45.0	36.0	149	65.0	52.0	185	85.0	68.0
81	85.0	80.0	6	14.4	11.6	42	5.6	4.4	78	25.6	20.4	114	45.6	36.4	150	65.6	52.4	186	85.6	68.4
80	84.4	80.6	7	18.9	11.1	43	6.1	4.9	79	26.1	20.9	115	46.1	36.9	151	66.1	52.9	187	86.1	68.9
79	83.9	80.1	8	18.3	10.7	44	6.7	5.8	80	26.7	21.8	116	46.7	37.3	152	66.7	53.8	188	86.7	69.8
78	83.8	80.6	9	12.8	10.2	45	7.2	5.8	81	27.2	21.8	117	47.2	37.8	153	67.2	53.8	189	87.2	69.8
27	82.8	80.6	10	12.2	9.8	46	7.8	6.2	82	27.8	22.2	118	47.8	38.2	154	67.8	54.2	190	87.8	70.2
26	82.2	80.8	11	11.7	9.8	47	8.8	6.7	88	28.8	22.7	119	48.8	38.7	155	68.8	54.7	191	88.8	70.7
25	81.7	80.8	12	11.1	8.9	48	8.9	7.1	84	28.9	23.1	120	48.9	39.1	156	68.9	55.1	192	88.9	71.1
24	81.1	80.6	13	10.6	8.4	49	9.4	7.6	86	29.4	23.6	121	49.4	39.6	157	69.4	55.6	198	89.4	71.6
23	80.6	80.6	14	10.0	8.0	50	10.0	8.0	86	30.0	24.0	122	50.0	40.0	158	70.0	56.0	194	90.0	72.0
22	80.0	80.4	15	9.4	7.6	51	10.6	8.4	87	30.6	24.4	128	50.6	40.4	159	70.6	56.4	195	90.6	72.4
21	79.4	80.6	16	8.9	7.1	52	11.1	8.9	88	31.1	24.9	124	51.1	40.9	160	71.1	56.9	196	91.1	72.9
19	78.9	80.1	17	8.3	6.7	58	11.7	9.8	89	31.7	25.8	125	51.7	41.8	161	71.7	57.8	197	91.7	73.8
18	78.8	80.6	18	7.8	6.2	54	12.2	9.8	90	32.2	26.8	126	52.2	41.8	162	72.2	57.8	198	92.2	73.8
17	77.8	80.6	19	7.2	5.8	55	12.8	10.2	91	32.8	26.2	127	52.8	42.3	163	72.8	58.2	199	92.8	74.2
16	77.2	80.8	20	6.7	5.8	56	18.8	10.7	92	33.8	26.7	128	53.8	42.7	164	73.8	58.7	200	93.8	74.7
16	26.7	21.8	21	6.1	4.9	57	18.9	11.1	98	38.9	27.1	129	58.9	45.1	165	78.9	59.1	201	98.9	75.1
15	26.1	20.9	22	5.6	4.4	58	14.4	11.6	94	34.4	27.6	180	54.4	48.6	166	74.4	59.6	202	94.4	75.6
14	25.6	20.4	23	5.0	4.0	59	15.0	12.0	95	35.0	28.0	181	55.0	44.0	167	75.0	60.0	208	95.0	76.0
12	24.4	19.6	24	4.4	3.6	60	15.6	12.4	96	35.6	28.4	182	55.6	44.4	168	75.6	60.4	204	95.6	76.4
12	24.4	19.6	25	8.9	8.1	61	16.1	12.9	97	36.1	28.9	183	56.1	44.9	169	76.1	60.9	205	96.1	76.9
11	23.9	19.1	26	8.3	7.7	62	16.7	13.8	98	36.7	29.8	184	56.7	45.3	170	76.7	61.8	206	96.7	77.8
10	23.8	18.7	27	2.8	2.2	68	17.2	13.8	99	37.2	29.8	185	57.2	45.3	171	77.2	61.8	207	97.2	77.8
9	23.8	18.2	28	2.2	1.8	64	17.8	14.2	100	37.8	30.2	186	57.8	45.8	172	77.8	62.2	208	97.8	78.2
8	23.2	17.8	29	1.7	1.8	65	18.8	14.7	101	38.8	30.7	187	58.8	46.7	178	78.8	62.7	209	98.8	78.7
7	21.7	17.8	30	1.1	0.9	66	18.9	15.1	102	38.9	31.1	188	58.9	47.1	174	78.9	63.1	210	98.9	79.1
6	21.1	16.9	31	0.6	0.4	67	19.4	15.6	108	39.4	31.6	189	59.4	47.6	175	79.4	63.6	211	99.4	79.6
5	20.6	16.4	32	+0.0	+0.0	68	20.0	16.0	104	40.0	32.0	140	60.0	48.0	176	80.0	64.0	212	100.0	80.0

TABLE 15.—CONVERSION OF CENTIGRADE INTO FAHRENHEIT DEGREES ABOVE 100, AND VICE VERSA.

Divide the degrees above 100 into hundreds and a remainder. The figure corresponding to the hundreds is taken from the following tables and added to that corresponding to the remainder as taken from Table 17. If, on converting Fahrenheit into Centigrade, the "remainder" amounts to 32°, or less, the degrees Centigrade corresponding to it are negative (below freezing point), and hence must be *deducted* from the figures of the following table. Also note, for example, that 300° F. is not = 166·7° C., but = 166·7 - 17·8, or = 111·1 + 377·7 = 148·9° C.

A.

C.	Fahr.	C.	Fahr.	C.	Fahr.	C.	Fahr.
100	180	600	1080	1100	1980	1600	2880
200	360	700	1260	1200	2160	1700	3060
300	540	800	1440	1300	2340	1800	3240
400	720	900	1620	1400	2520	1900	3420
500	900	1000	1800	1500	2700	2000	3600

B.

Fahr.	C.	Fahr.	C.	Fahr.	C.	Fahr.	C.
100	55·6	1000	556·6	1900	1055·6	2800	1555·6
200	111·1	1100	611·1	2000	1111·1	2900	1611·1
300	166·7	1200	666·7	2100	1166·7	3000	1666·7
400	222·2	1300	722·2	2200	1222·2	3100	1722·2
500	277·8	1400	777·8	2300	1277·8	3200	1777·8
600	333·3	1500	833·3	2400	1333·3	3300	1833·3
700	388·9	1600	888·9	2500	1388·9	3400	1888·9
800	444·4	1700	944·4	2600	1444·4	3500	1944·4
900	500	1800	1000	2700	1500

TABLE 16.—MELTING POINTS (FREEZING POINTS).

	Degrees Cent.
Alcohol (ethylic)	- 130
Aluminium	657
Ammonia	- 75
Antimony	630
Asphalt	100
Benzene (pure)	6
Bismuth	268
Boric acid	186
Brass	900
Bromine	- 22
Bronze	900
Cadmium	321
Carbon dioxide	- 70
Cobalt	1500
Colophonium	185
Copper	1084
Cupric chloride	498
Cuprous chloride	434
Fat, ox	40
sheep	42
pig	27
Fluorspar *	902-1380
Glass	1200
containing lead	1000
Gold	1063
Iron, cast, white	1075-1135
grey	1200-1250
wrought	1500
Iodine	113
Lead	326
oxide	954
chloride	490
Magnesium	633
Mercury	- 39.5
Mercuric chloride *	287-293
Naphthalene	79
Nickel	1484
Nitric acid	- 54
oxide	- 148.8 to - 167
Nitric tetroxide	- 11
Nitrous oxide	- 102

* The statements found in literature vary between these limits.

TABLE 16—*Continued.*

	Degrees Cent.
Palm oil	29
Paraffin, hard	45-60
Pitch (coal tar, hard)	150-200
Phosphorus	44
Platinum	1710
Potassium chlorate *	248-302
iodide *	614-723
carbonate *	884-898
nitrate *	827-853
chloride *	740-804
sulphate	1015-1078
Rose's metal	94
Selenium	217
Stearic acid	70
Steel	1875
Silver, metallic	961.5
chloride *	450-460
nitrate	217
Strontium chloride	825
Sodium chloride *	772-840
sulphate *	861-884
nitrate *	308-330
chlorate *	248-302
carbonate *	814-918
Spermaceti	45-50
Sulphur (monoclinic)	120.1
dioxide	-72.7
trioxide	14.8
Sulphuretted hydrogen	-85
Sulphuric acid, <i>cf.</i> special part.	
Thallium	301
Tin	282
tetrachloride	-88
Wax, bees'	62-70
Wood's metal	70
Zinc	419

* The statements found in literature vary between these limits.

TABLE 17.—FREEZING MIXTURES.

Substances.	Parts by Weight.	Temp. falls		Substances.	Parts by Weight.	Temp. falls	
		From	To			From	To
1. Sodium sulphate	6	10°	-25°	7. Dilute nitric acid	1	10°	-35°
Ammonium nitrate	5			Snow	1		
Dilute nitric acid	4						
2. Ammonium chloride	5	10°	-12°	8. Sodium sulphate	8	10°	-18°
Potassium nitrate	5			Hydrochloric acid	5		
Water	16						
3. Sodium sulphate	8	10°	-10°	9. Ammonium nitrate	1	10°	-16°
Dilute nitric acid	2			Water	1		
4. Sodium sulphate	6	10°	-23°	10. Potassium hydroxide	4	0°	-37°
Ammonium chloride	4			Snow	3		
Potassium nitrate	2						
Dilute nitric acid	4						
5. Sodium chloride	1	0°	-18°	11. Dilute nitric acid	1	0°	-40°
Snow	3			Dilute sulphuric acid	1		
6. Ammonium chloride	1	8°	-24°	Snow	2	5°	-41°
Potassium nitrate	1			Dilute sulphuric acid	1		
Water	1			Snow	1		
				13. Calcium chloride	3	0°	-33°
				Snow	2		
				14. Calcium chloride	2	0°	-42°
				Snow	1		

TABLE 18.—BOILING POINTS.

	Degrees Centigrade.
Acetone	56
Alcohol, absolute	78
Aldehyde	21
Ammonia, anhydrous	-33·7
nitrate, satur. solution	164
Barium chloride, satur. solution	104·4
Benzene	80·4
Bromine	68·0
Calcium chloride, satur. solution	178
66 per cent. solution	156
33 per cent. solution	128
nitrate, satur. solution	152
Carbon dioxide	-78
bisulphide	47
Chlorine	-33·6
Ether	35
Hydrochloric acid, 20·2 per cent. HCl	110
Iodine	184·4
Methylic alcohol	60
Mercury	356
Naphthalene	218
Nitric acid, very concentrated	86
specific gravity 1·42	121
Nitrous anhydride	3·5

TABLE 18—*Continued.*

	Degrees Centigrade.
Nitrous oxide	- 88
Nitric peroxide	20
Potassium chloride, satur. solution	108·5
chlorate, satur. solution	104·4
acetate, satur. solution	161
carbonate, satur. solution	133·5
nitrate, satur. solution	115
sulphate, satur. solution	102·1
Sodium chloride, satur. solution	108·8
acetate, satur. solution	125
carbonate, satur. solution	105
phosphate, satur. solution	106·6
nitrate, satur. solution	120
Sulphur	445
Sulphuric acid, H ₂ SO ₄	328
anhydride α	15
β	50
Sulphur dioxide	- 10
Toluene	111
Xylenes	136-141
Turpentine, spirits of	160
Zinc	930

TABLE 19.—HIGH TEMPERATURES, AS MEASURED WITH LE CHATELIER'S PYROMETER.

(Where no other observer is quoted, according to Le Chatelier's publications 1892, 1895, and 1900.)

Spirit lamp (Heraeus), about	800	Blast-furnace (grey Bessemer pig) at tuyeres	1980
Petroleum flame, about	1500	iron, on tapping	1400-1520
Bunsen burner (Lewes)—		Glass furnaces—pot furnace	1375
With blue cone.		temp. of pot during refining	1310
Top of inner cone	1090	temp. of pot during hot firing	1045
Middle of outer cone	1533	cistern furnace.	1400
Top	1175	cistern furnace, temp. of glass	1310
Margin	1333	Porcelain furnace, for hard porcelain (final temperature)	1400
(At the level of the top of the inner cone.)		Coal-gas, Siemens furnaces, top	1190
Fusing point of white Swedish pig iron	1135	bottom	1045
grey foundry pig iron	1220	retorts (final temperature)	975
ingot iron, with 3.1 per cent. C.	1475	fire gases at chimney	680
ingot, half hard, 0.3 per cent. C.	1455	Annular brick kiln	1100
ingot steel, 0.9 per cent. C.	1410	Electric incandescent lamps	1800-2100
silver	962	light arc (absolute temp.)	4100
gold	1065	Fusing point of fireclay	1670-1700
copper	1076	Seger cone, No. 36 (Heraeus)	1705
nickel	1496	No. 36	1685
platinum	1710	No. 34	1670
Bessemer converter	1580-1640	No. 33	1650
Siemens-Martin furnace	1420-1550	No. 32	1635
Siemens crucible steel furnace	1600	No. 31	1618
Revolving puddling furnace (final temperature)	1380	No. 30	1605

TABLE 20.—REDUCTION OF THE VOLUME OF

General formula for Dry Gases, $V_0 = \frac{V \times 273b}{(273+t)760}$

b = Barometric pressure, reduced to 0°; t = temperature; f = tension

I. Table for reducing the volumes of

0°.	1°.	2°.	3°.	4°.	5°.	6°.	7°.	8°.	9°.	10°.	0°.
1	0.996	0.998	0.999	0.996	0.982	0.978	0.975	0.972	0.968	0.965	1
2	1.998	1.985	1.978	1.971	1.964	1.967	1.960	1.948	1.986	1.929	2
3	2.989	2.978	2.967	2.967	2.946	2.986	2.925	2.915	2.904	2.894	3
4	3.985	3.971	3.956	3.942	3.928	3.914	3.900	3.886	3.872	3.859	4
5	4.982	4.964	4.946	4.928	4.910	4.898	4.876	4.858	4.841	4.824	5
6	5.978	5.956	5.985	5.918	5.892	5.871	5.850	5.880	5.809	5.788	6
7	6.974	6.949	6.924	6.899	6.874	6.850	6.825	6.801	6.777	6.758	7
8	7.970	7.942	7.918	7.885	7.856	7.828	7.800	7.778	7.745	7.718	8
9	8.967	8.934	8.902	8.870	8.838	8.807	8.775	8.744	8.718	8.682	9
10	9.968	9.927	9.891	9.856	9.820	9.785	9.750	9.716	9.681	9.647	10
11	10.96	10.92	10.88	10.84	10.80	10.76	10.78	10.69	10.65	10.61	11
12	11.96	11.91	11.87	11.83	11.78	11.74	11.70	11.66	11.62	11.57	12
13	12.95	12.91	12.86	12.81	12.76	12.72	12.68	12.63	12.59	12.54	13
14	13.95	13.90	13.85	13.80	13.75	13.70	13.65	13.60	13.55	13.50	14
15	14.95	14.89	14.84	14.78	14.73	14.68	14.63	14.57	14.52	14.47	15
16	15.94	15.88	15.83	15.77	15.71	15.66	15.60	15.55	15.49	15.48	16
17	16.94	16.87	16.82	16.75	16.69	16.64	16.58	16.52	16.46	16.40	17
18	17.93	17.87	17.81	17.74	17.67	17.61	17.55	17.49	17.48	17.86	18
19	18.93	18.86	18.79	18.72	18.65	18.59	18.53	18.46	18.39	18.33	19
20	19.93	19.85	19.78	19.71	19.64	19.57	19.50	19.43	19.36	19.29	20
21	20.93	20.84	20.77	20.69	20.62	20.55	20.48	20.40	20.33	20.26	21
22	21.92	21.84	21.76	21.68	21.60	21.53	21.45	21.37	21.30	21.22	22
23	22.92	22.83	22.75	22.66	22.58	22.51	22.43	22.35	22.26	22.18	23
24	23.92	23.82	23.74	23.65	23.56	23.48	23.40	23.32	23.23	23.15	24
25	24.91	24.81	24.73	24.64	24.55	24.46	24.38	24.29	24.20	24.11	25
26	25.91	25.81	25.72	25.62	25.53	25.44	25.35	25.26	25.17	25.08	26
27	26.90	26.80	26.71	26.61	26.52	26.42	26.33	26.23	26.13	26.04	27
28	27.90	27.79	27.69	27.59	27.50	27.40	27.30	27.20	27.10	27.01	28
29	28.90	28.78	28.68	28.58	28.48	28.38	28.28	28.17	28.07	27.97	29
30	29.89	29.78	29.67	29.57	29.46	29.36	29.25	29.15	29.04	28.94	30
31	30.89	30.77	30.66	30.55	30.44	30.34	30.23	30.12	30.01	29.91	31
32	31.88	31.76	31.65	31.54	31.42	31.32	31.20	31.09	30.98	30.87	32
33	32.88	32.76	32.64	32.52	32.40	32.30	32.18	32.06	31.94	31.84	33
34	33.88	33.75	33.63	33.51	33.38	33.27	33.15	33.03	32.91	32.80	34
35	34.87	34.74	34.62	34.50	34.37	34.25	34.13	34.01	33.88	33.77	35
36	35.87	35.74	35.61	35.48	35.35	35.23	35.10	34.98	34.85	34.73	36
37	36.87	36.73	36.60	36.47	36.33	36.21	36.08	35.95	35.82	35.70	37
38	37.86	37.72	37.59	37.45	37.32	37.19	37.05	36.92	36.79	36.66	38
39	38.86	38.71	38.58	38.44	38.30	38.16	38.03	37.89	37.75	37.62	39
40	39.85	39.71	39.56	39.42	39.28	39.14	39.00	38.86	38.72	38.59	40
41	40.85	40.70	40.55	40.41	40.26	40.12	39.98	39.83	39.69	39.55	41
42	41.85	41.69	41.54	41.39	41.24	41.10	40.95	40.80	40.66	40.52	42
43	42.84	42.68	42.53	42.38	42.22	42.08	41.93	41.78	41.62	41.48	43
44	43.84	43.68	43.52	43.37	43.20	43.05	42.90	42.75	42.59	42.45	44
45	44.84	44.67	44.51	44.35	44.19	44.03	43.88	43.72	43.56	43.41	45
46	45.83	45.66	45.50	45.34	45.17	45.01	44.85	44.69	44.53	44.38	46
47	46.83	46.65	46.48	46.32	46.15	45.99	45.83	45.66	45.50	45.34	47
48	47.83	47.65	47.48	47.31	47.14	46.97	46.80	46.63	46.47	46.31	48
49	48.82	48.64	48.47	48.29	48.12	47.95	47.78	47.60	47.44	47.27	49
50	49.82	49.64	49.46	49.28	49.10	48.93	48.75	48.58	48.41	48.24	50

GASES TO NORMAL TEMPERATURE & PRESSURE.

General formula for Moist Gases, $V_0 = \frac{V \times 273(t-f)}{(273+t)760}$

of aqueous vapour at f . Compare Table 28.

gases to a temperature of 0° C.

0°.	1°.	2°.	3°.	4°.	5°.	6°.	7°.	8°.	9°.	10°.	0°.
51	50·82	50·68	50·45	50·26	50·08	49·91	49·78	49·55	49·88	49·21	51
52	51·81	51·62	51·44	51·25	51·06	50·89	50·70	50·52	50·85	50·17	52
53	52·81	52·62	52·48	52·24	52·05	51·87	51·68	51·49	51·81	51·18	53
54	53·81	53·61	53·42	53·22	53·03	52·84	52·65	52·46	52·28	52·10	54
55	54·80	54·60	54·41	54·21	54·01	53·82	53·63	53·44	53·25	53·06	55
56	55·80	55·60	55·40	55·19	54·99	54·80	54·60	54·41	54·22	54·03	56
57	56·80	56·59	56·39	56·18	55·97	55·78	55·58	55·38	55·19	54·99	57
58	57·79	57·58	57·37	57·16	56·95	56·76	56·55	56·35	56·15	55·96	58
59	58·79	58·57	58·37	58·15	57·93	57·74	57·53	57·32	57·12	56·92	59
60	59·78	59·56	59·35	59·13	58·92	58·71	58·50	58·30	58·09	57·88	60
61	60·78	60·56	60·34	60·12	59·90	59·69	59·48	59·27	59·06	58·85	61
62	61·78	61·55	61·33	61·10	60·88	60·67	60·45	60·24	60·03	59·81	62
63	62·77	62·54	62·32	62·09	61·86	61·65	61·43	61·21	60·99	60·77	63
64	63·77	63·53	63·31	63·07	62·84	62·63	62·40	62·18	61·96	61·74	64
65	64·76	64·53	64·30	64·06	63·83	63·61	63·38	63·15	62·93	62·70	65
66	65·76	65·52	65·29	65·04	64·81	64·58	64·35	64·13	63·90	63·67	66
67	66·75	66·51	66·27	66·03	65·79	65·56	65·33	65·10	64·86	64·63	67
68	67·75	67·50	67·26	67·02	66·77	66·54	66·30	66·07	65·83	65·60	68
69	68·75	68·50	68·25	68·01	67·75	67·52	67·28	67·04	66·80	66·56	69
70	69·74	69·49	69·24	68·99	68·74	68·50	68·25	68·01	67·77	67·53	70
71	70·74	70·48	70·23	69·98	69·72	69·48	69·23	68·98	68·74	68·49	71
72	71·74	71·48	71·22	70·96	70·70	70·46	70·20	69·95	69·71	69·46	72
73	72·73	72·47	72·21	71·95	71·69	71·44	71·18	70·93	70·67	70·42	73
74	73·73	73·46	73·20	72·94	72·68	72·42	72·16	71·90	71·64	71·39	74
75	74·72	74·45	74·19	73·92	73·65	73·39	73·13	72·87	72·61	72·35	75
76	75·72	75·45	75·18	74·90	74·63	74·37	74·10	73·84	73·58	73·32	76
77	76·72	76·44	76·17	75·89	75·61	75·35	75·08	74·81	74·55	74·28	77
78	77·71	77·43	77·15	76·87	76·59	76·33	76·05	75·78	75·51	75·25	78
79	78·71	78·42	78·14	77·86	77·58	77·31	77·03	76·75	76·48	76·21	79
80	79·70	79·42	79·13	78·85	78·56	78·28	78·00	77·73	77·45	77·18	80
81	80·70	80·41	80·12	79·83	79·54	79·26	78·98	78·70	78·42	78·14	81
82	81·69	81·40	81·11	80·82	80·52	80·24	79·95	79·67	79·39	79·11	82
83	82·69	82·39	82·10	81·81	81·51	81·22	80·93	80·64	80·36	80·07	83
84	83·68	83·38	83·09	82·79	82·49	82·20	81·90	81·61	81·32	81·04	84
85	84·68	84·38	84·08	83·78	83·47	83·17	82·88	82·58	82·29	82·00	85
86	85·68	85·37	85·07	84·76	84·45	84·15	83·85	83·55	83·26	82·97	86
87	86·68	86·37	86·06	85·75	85·44	85·13	84·83	84·53	84·23	83·93	87
88	87·67	87·36	87·05	86·74	86·42	86·11	85·80	85·50	85·20	84·90	88
89	88·67	88·35	88·04	87·72	87·40	87·09	86·78	86·47	86·16	85·86	89
90	89·67	89·34	89·02	88·70	88·38	88·07	87·75	87·44	87·13	86·82	90
91	90·66	90·34	90·01	89·69	89·36	89·05	88·73	88·41	88·10	87·79	91
92	91·66	91·33	91·00	90·67	90·34	90·02	89·70	89·38	89·07	88·75	92
93	92·66	92·32	91·99	91·66	91·33	91·01	90·68	90·36	90·04	89·72	93
94	93·65	93·31	92·98	92·64	92·31	91·98	91·65	91·33	91·00	90·68	94
95	94·65	94·31	93·97	93·63	93·29	92·96	92·63	92·30	91·97	91·65	95
96	95·65	95·30	94·96	94·61	94·27	93·94	93·60	93·27	92·94	92·61	96
97	96·64	96·29	95·95	95·60	95·25	94·92	94·58	94·24	93·91	93·57	97
98	97·64	97·28	96·93	96·58	96·24	95·90	95·55	95·21	94·87	94·54	98
99	98·64	98·27	97·92	97·57	97·22	96·87	96·53	96·18	95·84	95·50	99
100	99·63	99·27	98·91	98·56	98·20	97·85	97·50	97·16	96·81	96·47	100

TABLE 20—

I. Table for reducing the volumes of

0°.	11°.	12°.	13°.	14°.	15°.	16°.	17°.	18°.	19°.	20°.	0°.
1	0·961	0·958	0·955	0·951	0·948	0·945	0·941	0·938	0·935	0·932	1
2	1·923	1·916	1·909	1·908	1·896	1·889	1·888	1·876	1·869	1·864	2
3	2·884	2·874	2·864	2·854	2·844	2·834	2·824	2·815	2·805	2·795	3
4	3·845	3·832	3·818	3·805	3·792	3·779	3·766	3·758	3·740	3·727	4
5	4·807	4·790	4·778	4·757	4·740	4·724	4·707	4·691	4·675	4·659	5
6	5·768	5·747	5·728	5·708	5·688	5·668	5·648	5·629	5·609	5·591	6
7	6·729	6·706	6·682	6·659	6·636	6·613	6·590	6·567	6·544	6·523	7
8	7·690	7·668	7·637	7·610	7·584	7·558	7·531	7·506	7·479	7·454	8
9	8·652	8·621	8·591	8·562	8·532	8·502	8·472	8·444	8·414	8·386	9
10	9·613	9·579	9·546	9·513	9·480	9·447	9·414	9·382	9·349	9·318	10
11	10·57	10·53	10·50	10·46	10·43	10·39	10·35	10·32	10·28	10·25	11
12	11·53	11·49	11·45	11·42	11·38	11·33	11·30	11·26	11·21	11·18	12
13	12·49	12·45	12·41	12·36	12·32	12·28	12·24	12·20	12·15	12·11	13
14	13·45	13·41	13·36	13·31	13·27	13·22	13·17	13·13	13·08	13·04	14
15	14·42	14·37	14·32	14·27	14·22	14·17	14·13	14·07	14·02	13·97	15
16	15·38	15·32	15·27	15·22	15·17	15·11	15·06	15·01	14·96	14·91	16
17	16·34	16·28	16·23	16·17	16·12	16·06	16·00	15·95	15·89	15·84	17
18	17·30	17·24	17·18	17·12	17·06	17·00	16·94	16·89	16·82	16·76	18
19	18·26	18·20	18·14	18·07	18·01	17·95	17·89	17·83	17·76	17·70	19
20	19·23	19·16	19·09	19·03	18·96	18·89	18·83	18·76	18·69	18·64	20
21	20·19	20·12	20·04	19·98	19·91	19·84	19·77	19·70	19·62	19·57	21
22	21·15	21·08	21·00	20·93	20·86	20·78	20·71	20·64	20·56	20·50	22
23	22·11	22·03	21·95	21·88	21·80	21·73	21·65	21·58	21·50	21·43	23
24	23·07	22·99	22·91	22·83	22·75	22·67	22·59	22·51	22·43	22·37	24
25	24·03	23·95	23·86	23·78	23·70	23·61	23·54	23·45	23·37	23·30	25
26	25·00	24·91	24·81	24·73	24·65	24·56	24·48	24·39	24·30	24·23	26
27	25·96	25·87	25·77	25·69	25·60	25·50	25·42	25·33	25·25	25·16	27
28	26·92	26·82	26·72	26·64	26·54	26·45	26·36	26·27	26·17	26·09	28
29	27·88	27·78	27·68	27·59	27·49	27·39	27·30	27·20	27·10	27·02	29
30	28·84	28·74	28·64	28·54	28·44	28·34	28·24	28·15	28·05	27·95	30
31	29·80	29·70	29·59	29·49	29·39	29·28	29·18	29·09	28·99	28·87	31
32	30·76	30·66	30·55	30·44	30·34	30·23	30·12	30·02	29·92	29·81	32
33	31·72	31·61	31·50	31·39	31·28	31·17	31·06	30·97	30·86	30·74	33
34	32·68	32·57	32·46	32·34	32·23	32·12	32·01	31·90	31·79	31·68	34
35	33·65	33·53	33·41	33·30	33·18	33·06	32·95	32·84	32·73	32·61	35
36	34·61	34·49	34·37	34·25	34·13	34·01	33·89	33·78	33·66	33·54	36
37	35·57	35·45	35·32	35·20	35·08	34·95	34·83	34·72	34·59	34·47	37
38	36·53	36·40	36·28	36·15	36·02	35·90	35·77	35·66	35·53	35·40	38
39	37·49	37·36	37·23	37·10	36·97	36·84	36·71	36·59	36·46	36·34	39
40	38·45	38·32	38·18	38·05	37·92	37·79	37·66	37·53	37·40	37·27	40
41	39·41	39·28	39·14	39·00	38·87	38·73	38·60	38·47	38·34	38·20	41
42	40·37	40·24	40·09	39·95	39·82	39·68	39·54	39·41	39·27	39·13	42
43	41·33	41·19	41·05	40·90	40·76	40·62	40·48	40·35	40·21	40·07	43
44	42·30	42·15	42·00	41·86	41·71	41·57	41·43	41·28	41·14	41·00	44
45	43·26	43·11	42·95	42·81	42·66	42·51	42·37	42·22	42·08	41·93	45
46	44·23	44·07	43·91	43·76	43·61	43·46	43·31	43·16	43·01	42·86	46
47	45·18	45·02	44·86	44·71	44·56	44·40	44·25	44·10	43·94	43·79	47
48	46·14	45·98	45·82	45·66	45·50	45·35	45·19	45·04	44·88	44·72	48
49	47·10	46·94	46·77	46·61	46·45	46·29	46·13	45·97	45·81	45·65	49
50	48·07	47·90	47·73	47·57	47·40	47·24	47·07	46·91	46·75	46·59	50

REDUCTION OF THE VOLUME OF GASES 41

Continued.

gases to a temperature of 0° C.—*Continued.*

0°.	11°.	12°.	13°.	14°.	15°.	16°.	17°.	18°.	19°.	20°.	0°.
51	49.06	48.86	48.69	48.52	48.35	48.18	48.01	47.85	47.68	47.52	51
52	49.99	49.82	49.64	49.47	49.30	49.13	48.95	48.79	48.62	48.45	52
53	50.95	50.77	50.59	50.42	50.24	50.07	49.89	49.72	49.55	49.38	53
54	51.91	51.73	51.55	51.37	51.19	51.02	50.84	50.66	50.49	50.32	54
55	52.87	52.69	52.50	52.33	52.14	51.96	51.78	51.60	51.43	51.25	55
56	53.84	53.65	53.46	53.28	53.09	52.91	52.72	52.54	52.36	52.18	56
57	54.80	54.61	54.41	54.23	54.04	53.86	53.66	53.48	53.29	53.11	57
58	55.76	55.56	55.37	55.18	54.98	54.80	54.60	54.42	54.23	54.04	58
59	56.72	56.52	56.32	56.13	55.93	55.74	55.54	55.35	55.16	54.97	59
60	57.68	57.47	57.28	57.08	56.88	56.68	56.48	56.29	56.09	55.91	60
61	58.64	58.43	58.23	58.03	57.83	57.63	57.43	57.23	57.02	56.84	61
62	59.60	59.39	59.19	58.98	58.78	58.57	58.36	58.17	57.96	57.77	62
63	60.56	60.35	60.14	59.93	59.72	59.52	59.30	59.11	58.90	58.71	63
64	61.52	61.31	61.10	60.88	60.67	60.46	60.25	60.04	59.83	59.64	64
65	62.49	62.28	62.06	61.84	61.62	61.40	61.19	60.98	60.77	60.57	65
66	63.45	63.23	63.01	62.79	62.57	62.35	62.13	61.92	61.70	61.50	66
67	64.41	64.18	63.96	63.74	63.52	63.29	63.07	62.85	62.63	62.42	67
68	65.37	65.13	64.92	64.69	64.46	64.23	64.01	63.80	63.57	63.36	68
69	66.33	66.09	65.87	65.64	65.41	65.18	64.95	64.73	64.50	64.30	69
70	67.29	67.05	66.82	66.59	66.36	66.13	65.90	65.67	65.44	65.23	70
71	68.25	68.01	67.77	67.54	67.31	67.07	66.84	66.61	66.38	66.16	71
72	69.21	68.97	68.73	68.49	68.26	68.02	67.78	67.55	67.31	67.09	72
73	70.17	69.92	69.68	69.44	69.20	68.96	68.72	68.49	68.26	68.03	73
74	71.14	70.88	70.64	70.40	70.15	69.91	69.66	69.42	69.18	68.96	74
75	72.10	71.84	71.59	71.35	71.10	70.85	70.61	70.37	70.12	69.89	75
76	73.06	72.80	72.55	72.30	72.05	71.80	71.55	71.30	71.05	70.82	76
77	74.02	73.76	73.51	73.25	73.00	72.74	72.49	72.24	71.98	71.75	77
78	74.98	74.71	74.46	74.20	73.94	73.69	73.43	73.18	72.92	72.68	78
79	75.94	75.67	75.41	75.15	74.89	74.63	74.37	74.11	73.85	73.61	79
80	76.90	76.63	76.37	76.10	75.84	75.58	75.31	75.06	74.79	74.54	80
81	77.86	77.59	77.32	77.05	76.79	76.52	76.25	76.00	75.73	75.47	81
82	78.82	78.55	78.28	78.00	77.74	77.47	77.19	76.94	76.66	76.40	82
83	79.78	79.50	79.23	78.95	78.68	78.41	78.13	77.87	77.60	77.34	83
84	80.75	80.46	80.19	79.91	79.63	79.35	79.08	78.81	78.53	78.27	84
85	81.71	81.42	81.14	80.86	80.58	80.30	80.02	79.75	79.47	79.20	85
86	82.67	82.38	82.10	81.81	81.53	81.24	80.96	80.69	80.40	80.13	86
87	83.63	83.33	83.05	82.76	82.48	82.19	81.90	81.63	81.35	81.06	87
88	84.59	84.29	84.01	83.71	83.42	83.13	82.84	82.57	82.27	81.99	88
89	85.56	85.25	84.96	84.66	84.37	84.08	83.78	83.50	83.22	82.93	89
90	86.52	86.21	85.92	85.62	85.32	85.02	84.72	84.44	84.14	83.86	90
91	87.48	87.17	86.87	86.57	86.27	85.96	85.66	85.38	85.07	84.79	91
92	88.44	88.13	87.83	87.52	87.22	86.91	86.60	86.32	86.01	85.72	92
93	89.40	89.09	88.78	88.47	88.16	87.85	87.54	87.25	86.95	86.66	93
94	90.36	90.04	89.73	89.42	89.11	88.80	88.49	88.19	87.88	87.59	94
95	91.32	91.00	90.68	90.37	90.06	89.74	89.43	89.13	88.82	88.52	95
96	92.29	91.96	91.64	91.32	91.01	90.69	90.37	90.07	89.75	89.45	96
97	93.25	92.92	92.59	92.27	91.96	91.63	91.31	91.00	90.68	90.38	97
98	94.21	93.87	93.55	93.23	92.90	92.58	92.25	91.94	91.62	91.31	98
99	95.17	94.83	94.50	94.18	93.85	93.52	93.19	92.88	92.55	92.24	99
100	96.13	95.79	95.46	95.13	94.80	94.47	94.14	93.82	93.49	93.18	100

TABLE 20—

I. Table for reducing the volumes of

0°.	31°.	22°.	23°.	24°.	25°.	26°.	27°.	28°.	29°.	0°.
1	0·929	0·936	0·932	0·919	0·916	0·913	0·910	0·907	0·904	1
2	1·857	1·851	1·845	1·839	1·832	1·826	1·820	1·814	1·808	2
3	2·786	2·777	2·767	2·758	2·749	2·739	2·730	2·721	2·712	3
4	3·714	3·702	3·690	3·677	3·665	3·652	3·640	3·628	3·616	4
5	4·643	4·628	4·612	4·597	4·581	4·566	4·551	4·535	4·520	5
6	5·572	5·558	5·544	5·516	5·497	5·479	5·461	5·442	5·424	6
7	6·500	6·479	6·457	6·435	6·413	6·392	6·371	6·349	6·328	7
8	7·429	7·404	7·379	7·354	7·330	7·305	7·281	7·256	7·232	8
9	8·357	8·330	8·302	8·274	8·246	8·218	8·191	8·163	8·136	9
10	9·286	9·255	9·224	9·193	9·162	9·131	9·101	9·070	9·040	10
11	10·21	10·18	10·15	10·11	10·07	10·04	10·01	9·98	9·94	11
12	11·14	11·11	11·07	11·03	10·99	10·96	10·92	10·88	10·85	12
13	12·07	12·03	11·99	11·96	11·91	11·87	11·83	11·79	11·75	13
14	13·00	12·96	12·91	12·87	12·83	12·78	12·74	12·70	12·66	14
15	13·93	13·88	13·84	13·79	13·74	13·70	13·66	13·61	13·56	15
16	14·86	14·81	14·76	14·71	14·66	14·61	14·56	14·51	14·46	16
17	15·79	15·73	15·68	15·63	15·58	15·52	15·47	15·42	15·37	17
18	16·71	16·66	16·60	16·55	16·49	16·44	16·38	16·33	16·27	18
19	17·64	17·58	17·53	17·47	17·41	17·35	17·29	17·23	17·18	19
20	18·57	18·51	18·45	18·39	18·33	18·26	18·20	18·14	18·08	20
21	19·50	19·44	19·37	19·31	19·24	19·17	19·11	19·05	18·98	21
22	20·43	20·36	20·29	20·23	20·15	20·09	20·02	19·95	19·89	22
23	21·36	21·29	21·21	21·15	21·07	21·00	20·93	20·86	20·79	23
24	22·28	22·21	22·14	22·07	21·99	21·91	21·84	21·77	21·70	24
25	23·21	23·14	23·06	22·99	22·90	22·83	22·75	22·68	22·60	25
26	24·14	24·06	23·98	23·91	23·83	23·74	23·66	23·58	23·50	26
27	25·07	24·99	24·90	24·83	24·75	24·65	24·57	24·49	24·41	27
28	26·00	25·91	25·82	25·74	25·65	25·57	25·48	25·40	25·31	28
29	26·93	26·84	26·75	26·67	26·57	26·48	26·39	26·30	26·22	29
30	27·86	27·77	27·67	27·58	27·49	27·39	27·30	27·21	27·12	30
31	28·79	28·70	28·59	28·50	28·41	28·30	28·21	28·12	28·02	31
32	29·72	29·62	29·51	29·42	29·32	29·22	29·12	29·02	28·93	32
33	30·65	30·55	30·44	30·34	30·24	30·13	30·03	29·93	29·83	33
34	31·57	31·47	31·36	31·26	31·16	31·04	30·94	30·84	30·74	34
35	32·50	32·40	32·28	32·18	32·07	31·96	31·85	31·75	31·64	35
36	33·43	33·32	33·20	33·10	32·99	32·87	32·76	32·65	32·54	36
37	34·36	34·25	34·12	34·02	33·90	33·78	33·67	33·56	33·45	37
38	35·29	35·17	35·05	34·93	34·82	34·70	34·58	34·47	34·35	38
39	36·22	36·10	35·97	35·85	35·74	35·61	35·49	35·37	35·25	39
40	37·14	37·02	36·90	36·77	36·65	36·52	36·40	36·28	36·16	40
41	38·07	37·95	37·82	37·69	37·57	37·43	37·31	37·19	37·06	41
42	39·00	38·87	38·74	38·61	38·48	38·35	38·22	38·09	37·97	42
43	39·93	39·80	39·66	39·53	39·40	39·26	39·13	39·00	38·87	43
44	40·85	40·72	40·59	40·45	40·32	40·17	40·04	39·91	39·78	44
45	41·78	41·65	41·51	41·37	41·23	41·09	40·95	40·82	40·68	45
46	42·71	42·57	42·43	42·29	42·15	42·00	41·86	41·72	41·58	46
47	43·64	43·50	43·35	43·21	43·06	42·91	42·77	42·63	42·49	47
48	44·57	44·42	44·27	44·12	43·98	43·83	43·68	43·54	43·39	48
49	45·50	45·35	45·19	45·04	44·89	44·74	44·59	44·44	44·30	49
50	46·43	46·28	46·12	45·97	45·81	45·66	45·51	45·35	45·20	50

REDUCTION OF THE VOLUME OF GASES 43

Continued.

gases to a temperature of 0° C.—*Continued.*

0°.	21°.	22°.	23°.	24°.	25°.	26°.	27°.	28°.	29°.	0°.
51	47·86	47·90	47·04	46·89	46·78	46·57	46·42	46·26	46·10	51
52	48·29	48·18	47·96	47·81	47·64	47·49	47·38	47·16	47·01	52
53	49·22	49·06	48·89	48·78	48·56	48·40	48·24	48·07	47·91	53
54	50·14	49·98	49·81	49·65	49·48	49·31	49·15	48·98	48·82	54
55	51·07	50·91	50·78	50·57	50·39	50·28	50·06	49·89	49·72	55
56	52·00	51·88	51·65	51·49	51·31	51·14	50·97	50·79	50·62	56
57	52·98	52·76	52·58	52·41	52·22	52·05	51·88	51·70	51·58	57
58	53·86	53·68	53·50	53·32	53·14	52·97	52·79	52·61	52·48	58
59	54·79	54·61	54·42	54·24	54·06	53·88	53·70	53·51	53·48	59
60	55·72	55·58	55·44	55·16	54·97	54·79	54·61	54·42	54·24	60
61	56·65	56·46	56·26	56·08	55·89	55·70	55·52	55·33	55·14	61
62	57·58	57·38	57·19	57·00	56·80	56·62	56·43	56·23	56·05	62
63	58·51	58·31	58·11	57·92	57·72	57·58	57·44	57·14	56·96	63
64	59·42	59·28	59·08	58·84	58·64	58·44	58·25	58·06	57·86	64
65	60·36	60·16	59·96	59·76	59·55	59·36	59·16	58·96	58·76	65
66	61·29	61·08	60·87	60·68	60·47	60·27	60·07	59·86	59·66	66
67	62·22	62·01	61·79	61·60	61·38	61·18	60·98	60·77	60·57	67
68	63·15	62·98	62·72	62·51	62·30	62·10	61·89	61·68	61·47	68
69	64·08	63·86	63·64	63·48	63·22	63·01	62·80	62·58	62·38	69
70	65·00	64·79	64·57	64·35	64·18	63·92	63·71	63·49	63·28	70
71	65·98	65·71	65·49	65·27	65·05	64·88	64·62	64·40	64·18	71
72	66·86	66·64	66·42	66·19	65·96	65·75	65·58	65·30	65·09	72
73	67·79	67·57	67·34	67·11	66·88	66·66	66·44	66·21	65·99	73
74	68·61	68·49	68·26	68·08	67·80	67·67	67·36	67·12	66·90	74
75	69·64	69·42	69·18	68·95	68·71	68·49	68·26	68·08	67·80	75
76	70·57	70·34	70·10	69·87	69·63	69·40	69·17	68·98	68·70	76
77	71·50	71·27	71·08	70·79	70·54	70·31	70·08	69·84	69·61	77
78	72·48	72·19	71·95	71·70	71·46	71·22	70·99	70·75	70·51	78
79	73·46	73·12	72·87	72·62	72·38	72·14	71·90	71·65	71·42	79
80	74·29	74·04	73·79	73·54	73·30	73·05	72·81	72·56	72·32	80
81	75·22	74·97	74·71	74·46	74·22	73·96	73·72	73·47	73·22	81
82	76·15	75·89	75·68	75·38	75·18	74·88	74·68	74·37	74·18	82
83	77·08	76·82	76·56	76·30	76·05	75·79	75·54	75·28	75·08	83
84	78·00	77·74	77·48	77·22	76·96	76·70	76·45	76·19	75·94	84
85	78·98	78·67	78·40	78·14	77·88	77·62	77·36	77·10	76·84	85
86	79·86	79·59	79·32	79·06	78·80	78·58	78·27	78·00	77·74	86
87	80·79	80·52	80·25	79·98	79·71	79·44	79·18	78·91	78·65	87
88	81·72	81·44	81·17	80·90	80·63	80·36	80·09	79·82	79·55	88
89	82·65	82·37	82·09	81·82	81·55	81·27	81·00	80·72	80·46	89
90	83·67	83·38	83·02	82·74	82·46	82·18	81·91	81·68	81·36	90
91	84·50	84·22	83·94	83·66	83·38	83·09	82·82	82·54	82·26	91
92	85·48	85·16	84·86	84·58	84·29	84·01	83·78	83·44	83·17	92
93	86·36	86·06	85·79	85·50	85·21	84·92	84·64	84·35	84·07	93
94	87·28	87·00	86·71	86·42	86·13	85·88	85·55	85·26	84·98	94
95	88·21	87·98	87·68	87·38	87·04	86·75	86·46	86·17	85·88	95
96	89·14	88·85	88·55	88·26	87·96	87·66	87·37	87·07	86·78	96
97	90·07	89·78	89·48	89·18	88·87	88·57	88·28	87·98	87·69	97
98	91·00	90·70	90·40	90·09	89·79	89·48	89·19	88·89	88·59	98
99	91·98	91·68	91·38	91·01	90·71	90·40	90·10	89·79	89·50	99
100	92·86	92·55	92·24	91·98	91·62	91·31	91·01	90·70	90·40	100

TABLE 20—Continued. II. Table for reducing the

Deduct from the barometric pressure 1 mm. for temperature between 0° and 12° for the expansion

760	710	712	714	716	718	720	722	724	726	728	760
1	0.984	0.987	0.940	0.942	0.945	0.947	0.950	0.953	0.955	0.958	1
2	1.868	1.874	1.879	1.884	1.890	1.895	1.900	1.905	1.911	1.916	2
3	2.808	2.810	2.818	2.826	2.834	2.842	2.850	2.858	2.866	2.874	3
4	3.783	3.747	3.758	3.768	3.779	3.789	3.800	3.810	3.821	3.832	4
5	4.672	4.685	4.697	4.711	4.724	4.736	4.750	4.763	4.777	4.790	5
6	5.607	5.621	5.637	5.653	5.669	5.684	5.700	5.716	5.732	5.747	6
7	6.540	6.558	6.577	6.595	6.614	6.631	6.650	6.668	6.687	6.705	7
8	7.474	7.494	7.516	7.537	7.558	7.578	7.600	7.621	7.642	7.663	8
9	8.409	8.431	8.456	8.479	8.503	8.526	8.550	8.573	8.598	8.621	9
10	9.34	9.37	9.40	9.42	9.45	9.47	9.50	9.53	9.55	9.58	10
11	10.28	10.31	10.34	10.36	10.39	10.42	10.45	10.48	10.51	10.54	11
12	11.21	11.24	11.27	11.30	11.34	11.37	11.40	11.43	11.46	11.50	12
13	12.14	12.18	12.21	12.24	12.28	12.31	12.35	12.38	12.41	12.45	13
14	13.08	13.12	13.16	13.19	13.23	13.26	13.30	13.34	13.37	13.41	14
15	14.02	14.06	14.10	14.13	14.17	14.21	14.25	14.29	14.33	14.37	15
16	14.95	14.99	15.03	15.07	15.11	15.15	15.20	15.24	15.28	15.33	16
17	15.88	15.93	15.98	16.02	16.06	16.10	16.15	16.19	16.23	16.28	17
18	16.82	16.87	16.92	16.96	17.01	17.05	17.10	17.15	17.19	17.24	18
19	17.76	17.81	17.86	17.90	17.95	18.00	18.05	18.10	18.15	18.21	19
20	18.68	18.74	18.79	18.84	18.90	18.95	19.00	19.05	19.11	19.16	20
21	19.62	19.68	19.73	19.78	19.84	19.90	19.95	20.00	20.06	20.12	21
22	20.55	20.61	20.67	20.72	20.78	20.84	20.90	20.96	21.01	21.07	22
23	21.49	21.55	21.61	21.66	21.73	21.79	21.85	21.91	21.97	22.03	23
24	22.43	22.49	22.55	22.61	22.68	22.74	22.80	22.86	22.92	22.99	24
25	23.35	23.42	23.49	23.55	23.62	23.69	23.75	23.81	23.88	23.95	25
26	24.29	24.36	24.43	24.50	24.57	24.64	24.70	24.77	24.83	24.90	26
27	25.23	25.30	25.37	25.44	25.51	25.58	25.65	25.72	25.79	25.86	27
28	26.16	26.23	26.30	26.37	26.45	26.52	26.60	26.67	26.74	26.82	28
29	27.10	27.17	27.24	27.31	27.40	27.48	27.55	27.62	27.70	27.78	29
30	28.03	28.10	28.18	28.26	28.34	28.42	28.50	28.58	28.66	28.74	30
31	28.97	29.04	29.12	29.20	29.29	29.37	29.45	29.53	29.62	29.70	31
32	29.90	29.98	30.06	30.14	30.23	30.32	30.40	30.48	30.57	30.66	32
33	30.83	30.91	31.00	31.08	31.17	31.26	31.35	31.43	31.52	31.61	33
34	31.77	31.85	31.94	32.03	32.12	32.21	32.30	32.39	32.48	32.57	34
35	32.71	32.79	32.88	32.97	33.07	33.16	33.25	33.34	33.44	33.53	35
36	33.64	33.73	33.82	33.91	34.01	34.10	34.20	34.29	34.39	34.49	36
37	34.57	34.66	34.76	34.86	34.96	35.05	35.15	35.25	35.35	35.45	37
38	35.50	35.60	35.70	35.80	35.90	36.00	36.10	36.20	36.30	36.40	38
39	36.44	36.54	36.64	36.74	36.85	36.95	37.05	37.15	37.26	37.37	39
40	37.38	37.48	37.58	37.68	37.79	37.89	38.00	38.10	38.21	38.32	40
41	38.31	38.41	38.52	38.62	38.74	38.84	38.95	39.05	39.17	39.28	41
42	39.25	39.35	39.46	39.57	39.69	39.79	39.90	40.01	40.12	40.23	42
43	40.18	40.29	40.40	40.51	40.62	40.73	40.85	40.96	41.08	41.19	43
44	41.11	41.22	41.34	41.44	41.56	41.68	41.80	41.91	42.03	42.14	44
45	42.05	42.16	42.28	42.39	42.52	42.63	42.75	42.87	42.99	43.11	45
46	42.98	43.10	43.22	43.34	43.46	43.58	43.70	43.82	43.94	44.06	46
47	43.91	44.03	44.15	44.27	44.40	44.52	44.65	44.77	44.90	45.03	47
48	44.84	44.96	45.09	45.22	45.35	45.47	45.60	45.73	45.85	45.98	48
49	45.78	45.91	46.04	46.17	46.30	46.42	46.55	46.67	46.80	46.94	49
50	46.72	46.85	46.97	47.11	47.24	47.36	47.50	47.63	47.77	47.90	50

volumes of gases to a pressure of 760 mm.

C., and 2 mm. between 18° and 19° C., 3 mm. between 20° and 25° C., to compensate of mercury.

760	710	712	714	716	718	720	722	724	726	728	760
51	47-65	47-79	47-92	48-06	48-18	48-31	48-45	48-59	48-73	48-86	51
52	48-58	48-72	48-85	48-99	49-18	49-26	49-40	49-54	49-68	49-82	52
53	49-52	49-66	49-79	49-92	50-07	50-21	50-35	50-48	50-64	50-78	53
54	50-45	50-59	50-73	50-87	51-01	51-15	51-30	51-44	51-59	51-73	54
55	51-38	51-52	51-67	51-82	51-96	52-10	52-25	52-39	52-54	52-69	55
56	52-32	52-47	52-61	52-76	52-91	53-06	53-20	53-35	53-50	53-65	56
57	53-25	53-41	53-55	53-70	53-85	54-00	54-15	54-30	54-45	54-60	57
58	54-19	54-34	54-49	54-64	54-79	54-94	55-10	55-25	55-41	55-56	58
59	55-13	55-28	55-43	55-59	55-74	55-89	56-05	56-21	56-37	56-52	59
60	56-07	56-22	56-37	56-52	56-67	56-82	57-00	57-16	57-32	57-47	60
61	57-00	57-15	57-31	57-47	57-63	57-79	57-95	58-11	58-27	58-43	61
62	57-98	58-09	58-25	58-41	58-58	58-74	58-90	59-06	59-23	59-39	62
63	58-87	59-06	59-19	59-35	59-52	59-68	59-85	60-01	60-18	60-35	63
64	59-80	59-96	60-13	60-30	60-47	60-63	60-80	60-97	61-14	61-30	64
65	60-74	60-90	61-07	61-24	61-41	61-58	61-75	61-92	62-09	62-26	65
66	61-67	61-84	62-01	62-18	62-35	62-52	62-70	62-87	63-05	63-22	66
67	62-60	62-77	62-95	63-12	63-30	63-47	63-65	63-82	64-00	64-18	67
68	63-54	63-71	63-89	64-06	64-24	64-42	64-60	64-78	64-96	65-13	68
69	64-47	64-65	64-83	65-01	65-19	65-37	65-55	65-73	65-91	66-09	69
70	65-40	65-58	65-77	65-95	66-14	66-32	66-50	66-68	66-87	67-05	70
71	66-34	66-52	66-71	66-89	67-08	67-26	67-45	67-63	67-82	68-01	71
72	67-27	67-46	67-65	67-83	68-02	68-21	68-40	68-59	68-78	68-97	72
73	68-20	68-39	68-58	68-77	68-97	69-16	69-35	69-54	69-73	69-92	73
74	69-14	69-33	69-52	69-72	69-92	70-11	70-30	70-49	70-69	70-88	74
75	70-07	70-27	70-47	70-66	70-86	71-05	71-25	71-44	71-64	71-84	75
76	71-01	71-21	71-41	71-60	71-80	72-00	72-20	72-40	72-60	72-80	76
77	71-94	72-14	72-34	72-54	72-75	72-95	73-15	73-35	73-55	73-75	77
78	72-87	73-07	73-28	73-48	73-69	73-89	74-10	74-30	74-51	74-71	78
79	73-80	74-01	74-22	74-42	74-63	74-84	75-05	75-25	75-46	75-67	79
80	74-74	74-94	75-16	75-37	75-58	75-78	76-00	76-21	76-42	76-63	80
81	75-67	75-88	76-10	76-31	76-52	76-74	76-95	77-16	77-37	77-58	81
82	76-60	76-82	77-04	77-25	77-47	77-68	77-90	78-11	78-32	78-54	82
83	77-54	77-76	77-98	78-19	78-41	78-63	78-85	79-07	79-28	79-50	83
84	78-47	78-69	78-91	79-13	79-35	79-57	79-80	80-02	80-24	80-46	84
85	79-41	79-63	79-86	80-08	80-31	80-53	80-75	80-97	81-19	81-41	85
86	80-34	80-57	80-80	81-02	81-25	81-47	81-70	81-92	82-15	82-37	86
87	81-28	81-50	81-74	81-96	82-19	82-42	82-65	82-87	83-10	83-33	87
88	82-21	82-44	82-68	82-90	83-13	83-36	83-60	83-83	84-06	84-29	88
89	83-15	83-38	83-62	83-85	84-08	84-31	84-55	84-78	85-02	85-25	89
90	84-09	84-31	84-56	84-79	85-02	85-25	85-50	85-73	85-98	86-21	90
91	85-02	85-25	85-50	85-73	85-98	86-21	86-45	86-69	86-93	87-17	91
92	86-05	86-19	86-44	86-68	86-92	87-16	87-40	87-64	87-89	88-13	92
93	86-89	87-12	87-38	87-62	87-87	88-11	88-35	88-59	88-84	89-08	93
94	87-82	88-06	88-32	88-56	88-81	89-05	89-30	89-54	89-80	90-04	94
95	88-76	89-01	89-26	89-50	89-75	90-00	90-25	90-50	90-75	91-00	95
96	89-69	89-94	90-20	90-45	90-70	90-95	91-20	91-45	91-70	91-95	96
97	90-62	90-87	91-12	91-38	91-64	91-89	92-15	92-40	92-66	92-91	97
98	91-56	91-82	92-07	92-33	92-59	92-84	93-10	93-35	93-62	93-87	98
99	92-49	92-75	93-01	93-26	93-52	93-79	94-05	94-31	94-57	94-83	99
100	93-42	93-68	93-95	94-21	94-47	94-74	95-00	95-26	95-52	95-79	100

TABLE 20—Continued. II. Table for reducing the

760	780	782	784	786	788	740	742	744	746	748	760
1	0.961	0.968	0.966	0.968	0.971	0.974	0.976	0.979	0.982	0.984	1
2	1.921	1.926	1.982	1.987	1.942	1.947	1.958	1.958	1.968	1.968	2
3	2.882	2.889	2.898	2.905	2.918	2.921	2.929	2.987	2.945	2.958	3
4	3.842	3.852	3.864	3.874	3.884	3.895	3.905	3.916	3.926	3.987	4
5	4.808	4.816	4.880	4.842	4.855	4.868	4.882	4.895	4.908	4.921	5
6	5.768	5.779	5.796	5.810	5.826	5.849	5.858	5.874	5.890	5.906	6
7	6.724	6.742	6.762	6.779	6.797	6.816	6.834	6.858	6.871	6.889	7
8	7.684	7.705	7.728	7.747	7.768	7.790	7.810	7.832	7.858	7.874	8
9	8.645	8.668	8.693	8.716	8.739	8.763	8.787	8.811	8.834	8.858	9
10	9.61	9.68	9.66	9.68	9.71	9.74	9.76	9.79	9.82	9.84	10
11	10.57	10.59	10.62	10.65	10.68	10.71	10.74	10.77	10.80	10.82	11
12	11.58	11.66	11.59	11.62	11.65	11.68	11.71	11.75	11.78	11.81	12
18	12.49	12.52	12.55	12.59	12.62	12.66	12.69	12.78	12.76	12.79	18
14	18.45	18.48	18.52	18.56	18.59	18.68	18.66	18.70	18.74	18.78	14
15	14.41	14.44	14.48	14.52	14.56	14.60	14.64	14.69	14.78	14.77	15
16	15.87	15.41	15.45	15.49	15.58	15.58	15.62	15.67	15.71	15.75	16
17	16.88	16.87	16.41	16.46	16.50	16.55	16.60	16.65	16.69	16.78	17
18	17.29	17.88	17.88	17.43	17.47	17.52	17.57	17.62	17.67	17.72	18
19	18.25	18.29	18.35	18.40	18.45	18.50	18.55	18.60	18.65	18.70	19
20	19.21	19.26	19.32	19.37	19.42	19.47	19.58	19.58	19.63	19.68	20
21	20.17	20.22	20.28	20.34	20.39	20.44	20.50	20.56	20.61	20.66	21
22	21.18	21.19	21.25	21.31	21.36	21.42	21.48	21.54	21.59	21.65	22
23	22.09	22.15	22.21	22.27	22.33	22.39	22.45	22.51	22.57	22.64	23
24	23.05	23.11	23.18	23.24	23.30	23.36	23.43	23.50	23.56	23.63	24
25	24.01	24.07	24.14	24.21	24.27	24.34	24.41	24.48	24.54	24.61	25
26	24.97	25.04	25.11	25.18	25.24	25.31	25.38	25.45	25.52	25.59	26
27	25.98	26.00	26.07	26.14	26.21	26.28	26.36	26.43	26.50	26.58	27
28	26.89	26.96	27.04	27.12	27.18	27.26	27.33	27.41	27.48	27.56	28
29	27.85	27.92	28.00	28.08	28.15	28.23	28.31	28.39	28.47	28.55	29
30	28.82	28.89	28.97	29.05	29.13	29.21	29.29	29.37	29.45	29.53	30
31	29.78	29.86	29.94	30.02	30.10	30.18	30.26	30.35	30.43	30.51	31
32	30.74	30.82	30.91	30.99	31.07	31.15	31.24	31.33	31.41	31.50	32
33	31.70	31.78	31.87	31.96	32.04	32.13	32.21	32.30	32.39	32.48	33
34	32.66	32.75	32.84	32.93	33.01	33.10	33.19	33.28	33.37	33.46	34
35	33.62	33.71	33.80	33.89	33.98	34.07	34.17	34.27	34.36	34.45	35
36	34.58	34.67	34.77	34.86	34.95	35.05	35.15	35.25	35.34	35.43	36
37	35.54	35.63	35.73	35.83	35.92	36.02	36.12	36.22	36.32	36.42	37
38	36.50	36.60	36.70	36.80	36.90	37.00	37.10	37.20	37.30	37.40	38
39	37.47	37.57	37.67	37.77	37.87	37.97	38.07	38.18	38.28	38.39	39
40	38.42	38.52	38.64	38.74	38.84	38.95	39.05	39.16	39.26	39.37	40
41	39.38	39.48	39.60	39.71	39.81	39.92	40.02	40.14	40.24	40.36	41
42	40.34	40.44	40.56	40.68	40.78	40.89	41.00	41.12	41.22	41.34	42
43	41.30	41.41	41.53	41.64	41.75	41.86	41.97	42.10	42.20	42.32	43
44	42.27	42.38	42.50	42.62	42.73	42.84	42.95	43.07	43.18	43.30	44
45	43.22	43.34	43.46	43.58	43.69	43.81	43.93	44.06	44.17	44.29	45
46	44.18	44.30	44.42	44.54	44.66	44.78	44.90	45.03	45.15	45.27	46
47	45.15	45.26	45.39	45.52	45.64	45.76	45.88	46.01	46.13	46.26	47
48	46.10	46.23	46.36	46.49	46.61	46.73	46.85	46.99	47.12	47.24	48
49	47.06	47.19	47.32	47.44	47.57	47.70	47.83	47.97	48.10	48.23	49
50	48.08	48.16	48.30	48.42	48.55	48.68	48.82	48.95	49.08	49.21	50

REDUCTION OF VOLUMES OF GASES

47

volumes of gases to a pressure of 760 mm.—*Continued.*

760	780	782	784	786	788	740	742	744	746	748	760
51	48.99	49.12	49.26	49.39	49.52	49.65	49.79	49.93	50.06	50.19	51
52	49.96	50.08	50.22	50.36	50.49	50.63	50.77	50.91	51.04	51.18	52
53	50.91	51.06	51.19	51.33	51.46	51.60	51.75	51.89	52.02	52.16	53
54	51.87	52.01	52.16	52.30	52.44	52.58	52.72	52.87	53.01	53.15	54
55	52.83	52.98	53.13	53.27	53.41	53.55	53.70	53.85	53.99	54.14	55
56	53.79	53.94	54.09	54.23	54.37	54.52	54.68	54.83	54.97	55.11	56
57	54.75	54.90	55.05	55.20	55.35	55.50	55.65	55.80	55.95	56.10	57
58	55.71	55.86	56.02	56.17	56.32	56.47	56.63	56.78	56.93	57.08	58
59	56.67	56.83	56.99	57.14	57.29	57.44	57.60	57.76	57.92	58.07	59
60	57.63	57.79	57.95	58.10	58.26	58.42	58.58	58.74	58.90	59.06	60
61	58.59	58.75	58.91	59.07	59.23	59.39	59.56	59.72	59.88	60.04	61
62	59.55	59.72	59.88	60.04	60.20	60.36	60.53	60.70	60.86	61.02	62
63	60.51	60.68	60.85	61.01	61.17	61.34	61.51	61.68	61.84	62.00	63
64	61.47	61.64	61.81	61.98	62.15	62.32	62.49	62.66	62.82	62.99	64
65	62.43	62.60	62.77	62.94	63.11	63.28	63.46	63.64	63.81	63.98	65
66	63.39	63.57	63.74	63.91	64.08	64.26	64.44	64.62	64.79	64.96	66
67	64.35	64.53	64.71	64.88	65.05	65.23	65.41	65.59	65.77	65.94	67
68	65.31	65.50	65.68	65.85	66.02	66.20	66.38	66.56	66.74	66.92	68
69	66.27	66.45	66.64	66.82	67.00	67.18	67.37	67.55	67.73	67.91	69
70	67.24	67.42	67.61	67.79	67.97	68.16	68.34	68.53	68.71	68.89	70
71	68.20	68.39	68.58	68.76	68.94	69.13	69.32	69.51	69.69	69.88	71
72	69.16	69.35	69.54	69.73	69.92	70.11	70.30	70.49	70.68	70.86	72
73	70.12	70.31	70.51	70.69	70.88	71.08	71.27	71.47	71.66	71.85	73
74	71.08	71.28	71.48	71.66	71.85	72.05	72.25	72.45	72.64	72.83	74
75	72.04	72.24	72.44	72.63	72.82	73.02	73.22	73.42	73.62	73.82	75
76	73.00	73.20	73.40	73.60	73.80	74.00	74.20	74.40	74.60	74.80	76
77	73.96	74.17	74.37	74.57	74.77	74.97	75.18	75.39	75.59	75.79	77
78	74.93	75.13	75.33	75.53	75.74	75.95	76.16	76.37	76.57	76.77	78
79	75.89	76.09	76.30	76.50	76.71	76.92	77.13	77.34	77.55	77.75	79
80	76.84	77.05	77.27	77.47	77.68	77.90	78.10	78.32	78.53	78.74	80
81	77.80	78.02	78.23	78.44	78.65	78.87	79.08	79.30	79.51	79.72	81
82	78.76	78.98	79.20	79.41	79.62	79.84	80.06	80.28	80.50	80.71	82
83	79.72	79.94	80.16	80.38	80.60	80.82	81.04	81.26	81.48	81.69	83
84	80.68	80.90	81.12	81.34	81.56	81.79	82.01	82.24	82.46	82.68	84
85	81.64	81.87	82.10	82.31	82.53	82.76	82.99	83.22	83.44	83.66	85
86	82.60	82.83	83.06	83.28	83.50	83.73	83.97	84.20	84.42	84.64	86
87	83.56	83.79	84.02	84.25	84.48	84.71	84.94	85.17	85.40	85.62	87
88	84.52	84.76	85.00	85.23	85.46	85.69	85.93	86.16	86.38	86.61	88
89	85.48	85.72	85.96	86.19	86.42	86.66	86.89	87.13	87.36	87.59	89
90	86.45	86.68	86.92	87.16	87.39	87.63	87.87	88.11	88.34	88.58	90
91	87.41	87.65	87.89	88.12	88.36	88.61	88.85	89.09	89.33	89.56	91
92	88.37	88.61	88.86	89.09	89.33	89.58	89.82	90.07	90.31	90.55	92
93	89.33	89.57	89.82	90.06	90.30	90.55	90.80	91.05	91.29	91.53	93
94	90.29	90.54	90.79	91.03	91.27	91.52	91.78	92.03	92.27	92.51	94
95	91.25	91.50	91.75	92.00	92.25	92.50	92.75	93.00	93.25	93.50	95
96	92.21	92.46	92.72	92.97	93.22	93.47	93.73	93.98	94.23	94.48	96
97	93.17	93.43	93.68	93.93	94.19	94.45	94.71	94.96	95.22	95.47	97
98	94.13	94.39	94.65	94.91	95.16	95.42	95.68	95.94	96.20	96.45	98
99	95.09	95.35	95.61	95.87	96.13	96.39	96.66	96.92	97.18	97.44	99
100	96.05	96.32	96.58	96.84	97.11	97.37	97.63	97.89	98.16	98.42	100

TABLE 20—Continued. II. Table for reducing the

760	760	752	754	756	758	762	764	766	768	770	760
1	0.987	0.989	0.992	0.995	0.997	1.008	1.005	1.008	1.011	1.018	1
2	1.974	1.979	1.984	1.989	1.995	2.005	2.011	2.016	2.021	2.026	2
3	2.960	2.968	2.976	2.984	2.992	3.007	3.016	3.024	3.032	3.039	3
4	3.947	3.958	3.968	3.979	3.990	4.010	4.021	4.032	4.042	4.052	4
5	4.934	4.947	4.960	4.974	4.987	5.018	5.026	5.040	5.058	5.066	5
6	5.921	5.937	5.952	5.968	5.984	6.016	6.032	6.047	6.068	6.079	6
7	6.908	6.926	6.944	6.962	6.982	7.018	7.037	7.055	7.074	7.092	7
8	7.894	7.916	7.936	7.958	7.979	8.021	8.042	8.063	8.084	8.106	8
9	8.881	8.906	8.929	8.952	8.977	9.023	9.043	9.071	9.095	9.119	9
10	9.87	9.89	9.92	9.95	9.97	10.03	10.05	10.08	10.11	10.18	10
11	10.85	10.88	10.91	10.94	10.97	11.08	11.06	11.09	11.12	11.14	11
12	11.84	11.87	11.90	11.94	11.97	12.04	12.07	12.10	12.18	12.16	12
13	12.83	12.86	12.89	12.93	12.96	13.04	13.07	13.10	13.14	13.17	13
14	13.82	13.85	13.88	13.92	13.96	14.04	14.07	14.11	14.15	14.17	14
15	14.81	14.84	14.87	14.92	14.96	15.04	15.08	15.12	15.16	15.19	15
16	15.79	15.83	15.87	15.91	15.95	16.05	16.09	16.18	16.17	16.21	16
17	16.78	16.82	16.86	16.91	16.95	17.05	17.09	17.14	17.18	17.22	17
18	17.77	17.81	17.85	17.90	17.95	18.05	18.09	18.15	18.19	18.23	18
19	18.76	18.80	18.85	18.90	18.95	19.05	19.10	19.15	19.20	19.25	19
20	19.74	19.79	19.84	19.89	19.95	20.05	20.11	20.16	20.21	20.26	20
21	20.73	20.77	20.82	20.89	20.94	21.05	21.11	21.17	21.22	21.27	21
22	21.71	21.76	21.82	21.88	21.94	22.06	22.12	22.18	22.23	22.28	22
23	22.70	22.75	22.81	22.88	22.94	23.06	23.12	23.18	23.24	23.30	23
24	23.69	23.74	23.80	23.87	23.93	24.06	24.13	24.19	24.25	24.31	24
25	24.67	24.73	24.80	24.87	24.93	25.06	25.13	25.20	25.26	25.32	25
26	25.66	25.72	25.79	25.86	25.93	26.06	26.14	26.21	26.27	26.34	26
27	26.65	26.71	26.78	26.86	26.93	27.07	27.15	27.22	27.28	27.35	27
28	27.63	27.70	27.77	27.85	27.92	28.07	28.15	28.23	28.29	28.36	28
29	28.62	28.69	28.76	28.84	28.92	29.07	29.16	29.24	29.30	29.37	29
30	29.60	29.68	29.76	29.84	29.92	30.07	30.16	30.24	30.32	30.39	30
31	30.59	30.67	30.75	30.84	30.92	31.08	31.17	31.25	31.33	31.41	31
32	31.58	31.66	31.74	31.83	31.92	32.08	32.17	32.26	32.34	32.42	32
33	32.56	32.65	32.73	32.82	32.91	33.08	33.18	33.27	33.35	33.43	33
34	33.55	33.64	33.73	33.82	33.91	34.09	34.18	34.28	34.36	34.45	34
35	34.54	34.63	34.72	34.82	34.91	35.09	35.19	35.28	35.37	35.46	35
36	35.52	35.62	35.71	35.81	35.91	36.09	36.19	36.29	36.38	36.47	36
37	36.51	36.61	36.71	36.81	36.90	37.09	37.20	37.30	37.39	37.49	37
38	37.50	37.60	37.70	37.80	37.90	38.20	38.20	38.30	38.40	38.50	38
39	38.49	38.59	38.69	38.80	38.90	39.10	39.21	39.31	39.41	39.51	39
40	39.47	39.58	39.68	39.79	39.90	40.10	40.21	40.32	40.42	40.52	40
41	40.46	40.56	40.67	40.79	40.89	41.11	41.22	41.33	41.43	41.54	41
42	41.44	41.55	41.66	41.78	41.89	42.11	42.23	42.34	42.44	42.55	42
43	42.43	42.54	42.66	42.78	42.89	43.11	43.23	43.35	43.45	43.56	43
44	43.42	43.53	43.66	43.77	43.89	44.12	44.23	44.35	44.46	44.58	44
45	44.40	44.52	44.64	44.76	44.88	45.12	45.24	45.36	45.47	45.59	45
46	45.39	45.51	45.63	45.76	45.88	46.12	46.24	46.36	46.48	46.60	46
47	46.38	46.50	46.63	46.76	46.88	47.12	47.25	47.38	47.49	47.61	47
48	47.36	47.49	47.62	47.75	47.87	48.18	48.25	48.39	48.51	48.63	48
49	48.35	48.48	48.61	48.74	48.87	49.18	49.26	49.40	49.52	49.64	49
50	49.34	49.47	49.60	49.74	49.87	50.18	50.26	50.40	50.53	50.66	50

REDUCTION OF VOLUMES OF GASES

volumes of gases to a pressure of 760 mm.—Continued.

760	750	752	754	756	758	762	764	766	768	770	760
51	50·88	50·46	50·60	50·74	50·87	51·14	51·27	51·41	51·54	51·67	51
52	51·82	51·45	51·59	51·73	51·87	52·14	52·28	52·42	52·55	52·68	52
53	52·80	52·44	52·58	52·72	52·87	53·14	53·28	53·42	53·56	53·70	53
54	53·29	53·48	53·57	53·72	53·86	54·14	54·28	54·43	54·57	54·72	54
55	54·28	54·42	54·56	54·71	54·86	55·15	55·29	55·44	55·58	55·73	55
56	55·26	55·41	55·56	55·71	55·86	56·15	56·29	56·45	56·59	56·74	56
57	56·25	56·40	56·55	56·70	56·85	57·15	57·30	57·45	57·60	57·76	57
58	57·24	57·39	57·54	57·69	57·85	58·15	58·30	58·46	58·61	58·77	58
59	58·22	58·38	58·53	58·69	58·85	59·16	59·31	59·47	59·62	59·78	59
60	59·21	59·37	59·52	59·68	59·84	60·16	60·32	60·47	60·63	60·79	60
61	60·20	60·36	60·52	60·68	60·84	61·16	61·32	61·48	61·64	61·81	61
62	61·19	61·35	61·51	61·67	61·84	62·16	62·33	62·49	62·65	62·82	62
63	62·17	62·34	62·50	62·67	62·83	63·17	63·33	63·50	63·67	63·84	63
64	63·16	63·33	63·49	63·66	63·83	64·17	64·34	64·51	64·68	64·85	64
65	64·15	64·32	64·49	64·66	64·83	65·17	65·34	65·51	65·69	65·86	65
66	65·13	65·31	65·48	65·65	65·82	66·17	66·35	66·52	66·70	66·88	66
67	66·12	66·30	66·47	66·64	66·82	67·18	67·35	67·52	67·71	67·89	67
68	67·10	67·29	67·46	67·64	67·82	68·18	68·36	68·54	68·72	68·90	68
69	68·09	68·28	68·45	68·63	68·82	69·18	69·36	69·54	69·73	69·91	69
70	69·08	69·26	69·44	69·63	69·82	70·18	70·37	70·55	70·74	70·92	70
71	70·07	70·25	70·43	70·62	70·81	71·19	71·37	71·56	71·75	71·94	71
72	71·05	71·24	71·43	71·62	71·81	72·19	72·38	72·57	72·76	72·95	72
73	72·04	72·23	72·42	72·61	72·81	73·19	73·38	73·57	73·77	73·97	73
74	73·03	73·22	73·41	73·61	73·80	74·19	74·39	74·58	74·78	74·98	74
75	74·01	74·21	74·40	74·60	74·80	75·20	75·39	75·59	75·79	75·99	75
76	75·00	75·20	75·40	75·60	75·80	76·20	76·40	76·60	76·80	77·01	76
77	75·99	76·19	76·39	76·59	76·79	77·20	77·40	77·60	77·81	78·02	77
78	76·97	77·18	77·38	77·58	77·79	78·20	78·41	78·61	78·82	79·03	78
79	77·96	78·17	78·37	78·58	78·79	79·21	79·41	79·62	79·83	80·04	79
80	78·94	79·16	79·36	79·58	79·79	80·21	80·42	80·63	80·84	81·06	80
81	79·93	80·15	80·35	80·57	80·79	81·21	81·42	81·64	81·85	82·07	81
82	80·92	81·14	81·35	81·56	81·78	82·21	82·43	82·65	82·87	83·09	82
83	81·91	82·13	82·34	82·56	82·78	83·22	83·44	83·66	83·88	84·10	83
84	82·90	83·12	83·34	83·56	83·78	84·22	84·44	84·66	84·89	85·11	84
85	83·88	84·11	84·33	84·55	84·78	85·22	85·45	85·67	85·90	86·13	85
86	84·87	85·10	85·32	85·55	85·78	86·22	86·46	86·69	86·91	87·14	86
87	85·85	86·08	86·31	86·54	86·77	87·22	87·46	87·69	87·92	88·15	87
88	86·84	87·07	87·30	87·54	87·77	88·23	88·47	88·69	88·93	89·17	88
89	87·82	88·06	88·29	88·53	88·77	89·24	89·47	89·70	89·94	90·18	89
90	88·81	89·05	89·29	89·52	89·77	90·25	90·48	90·71	90·95	91·19	90
91	89·80	90·04	90·28	90·52	90·76	91·24	91·48	91·72	91·96	92·21	91
92	90·79	91·03	91·27	91·51	91·76	92·24	92·49	92·73	92·97	93·22	92
93	91·77	92·02	92·26	92·51	92·76	93·24	93·49	93·74	93·98	94·23	93
94	92·76	93·01	93·26	93·50	93·75	94·24	94·49	94·74	94·99	95·24	94
95	93·74	94·00	94·25	94·50	94·75	95·25	95·50	95·75	96·00	96·26	95
96	94·73	94·98	95·24	95·49	95·75	96·25	96·51	96·76	97·01	97·27	96
97	95·72	95·97	96·23	96·49	96·75	97·25	97·51	97·77	98·02	98·29	97
98	96·70	96·96	97·22	97·48	97·74	98·25	98·52	98·77	99·03	99·30	98
99	97·69	97·95	98·21	98·48	98·74	99·26	99·52	99·78	100·04	100·31	99
100	98·68	98·95	99·21	99·47	99·74	100·26	100·53	100·79	101·05	101·32	100

TABLE 20—Continued. II. Table for reducing the

760	750	752	754	756	758	762	764	766	768	770	760
1	0·987	0·989	0·992	0·995	0·997	1·008	1·006	1·008	1·011	1·018	1
2	1·974	1·979	1·984	1·989	1·995	2·005	2·011	2·016	2·021	2·036	2
3	2·960	2·968	2·976	2·984	2·992	3·007	3·016	3·024	3·032	3·039	3
4	3·947	3·958	3·968	3·979	3·990	4·010	4·021	4·032	4·042	4·052	4
5	4·934	4·947	4·960	4·974	4·987	5·018	5·036	5·040	5·058	5·066	5
6	5·921	5·937	5·952	5·968	5·984	6·016	6·032	6·047	6·063	6·079	6
7	6·908	6·926	6·944	6·963	6·982	7·018	7·037	7·055	7·074	7·092	7
8	7·894	7·916	7·938	7·958	7·979	8·021	8·042	8·063	8·084	8·106	8
9	8·881	8·906	8·929	8·952	8·977	9·023	9·048	9·071	9·095	9·119	9
10	9·87	9·89	9·92	9·95	9·97	10·08	10·06	10·08	10·11	10·18	10
11	10·85	10·88	10·91	10·94	10·97	11·08	11·06	11·09	11·12	11·14	11
12	11·84	11·87	11·90	11·94	11·97	12·04	12·07	12·10	12·13	12·16	12
13	12·83	12·86	12·89	12·93	12·96	13·04	13·07	13·10	13·14	13·17	13
14	13·82	13·85	13·88	13·92	13·96	14·04	14·07	14·11	14·15	14·17	14
15	14·81	14·84	14·87	14·92	14·96	15·04	15·08	15·12	15·16	15·19	15
16	15·79	15·83	15·87	15·91	15·95	16·06	16·09	16·13	16·17	16·21	16
17	16·78	16·82	16·86	16·91	16·95	17·06	17·09	17·14	17·18	17·22	17
18	17·77	17·81	17·85	17·90	17·95	18·06	18·10	18·15	18·19	18·23	18
19	18·75	18·80	18·85	18·90	18·95	19·06	19·10	19·15	19·20	19·25	19
20	19·74	19·79	19·84	19·89	19·95	20·06	20·11	20·16	20·21	20·26	20
21	20·72	20·77	20·83	20·89	20·94	21·06	21·11	21·17	21·22	21·27	21
22	21·71	21·76	21·82	21·88	21·94	22·06	22·12	22·18	22·23	22·28	22
23	22·70	22·75	22·81	22·88	22·94	23·06	23·12	23·18	23·24	23·30	23
24	23·69	23·74	23·80	23·87	23·93	24·06	24·13	24·19	24·25	24·31	24
25	24·67	24·73	24·80	24·87	24·93	25·06	25·13	25·20	25·26	25·32	25
26	25·66	25·72	25·79	25·86	25·93	26·06	26·14	26·21	26·27	26·34	26
27	26·65	26·71	26·78	26·86	26·93	27·07	27·15	27·22	27·28	27·35	27
28	27·63	27·70	27·77	27·85	27·92	28·07	28·15	28·23	28·29	28·36	28
29	28·62	28·69	28·76	28·84	28·92	29·07	29·16	29·24	29·30	29·37	29
30	29·60	29·68	29·76	29·84	29·92	30·07	30·16	30·24	30·32	30·39	30
31	30·59	30·67	30·75	30·84	30·92	31·08	31·17	31·25	31·33	31·41	31
32	31·58	31·66	31·74	31·83	31·92	32·08	32·17	32·26	32·34	32·42	32
33	32·56	32·65	32·73	32·82	32·91	33·08	33·18	33·27	33·35	33·43	33
34	33·55	33·64	33·73	33·82	33·91	34·09	34·18	34·28	34·36	34·45	34
35	34·54	34·63	34·72	34·82	34·91	35·09	35·19	35·28	35·37	35·46	35
36	35·52	35·62	35·71	35·81	35·91	36·09	36·19	36·29	36·38	36·47	36
37	36·51	36·61	36·71	36·81	36·90	37·09	37·20	37·30	37·39	37·49	37
38	37·50	37·60	37·70	37·80	37·90	38·10	38·20	38·30	38·40	38·50	38
39	38·49	38·59	38·69	38·80	38·90	39·10	39·21	39·31	39·41	39·51	39
40	39·47	39·58	39·68	39·79	39·90	40·10	40·21	40·32	40·42	40·52	40
41	40·46	40·56	40·67	40·79	40·89	41·11	41·22	41·33	41·44	41·54	41
42	41·44	41·55	41·66	41·78	41·89	42·11	42·22	42·34	42·44	42·55	42
43	42·43	42·54	42·66	42·78	42·89	43·11	43·23	43·35	43·45	43·56	43
44	43·42	43·53	43·65	43·77	43·89	44·12	44·23	44·35	44·46	44·58	44
45	44·40	44·52	44·64	44·76	44·88	45·12	45·24	45·36	45·47	45·59	45
46	45·39	45·51	45·63	45·76	45·88	46·12	46·24	46·36	46·48	46·60	46
47	46·38	46·50	46·63	46·76	46·88	47·12	47·25	47·38	47·49	47·61	47
48	47·36	47·49	47·62	47·75	47·87	48·13	48·25	48·39	48·51	48·63	48
49	48·35	48·48	48·61	48·74	48·87	49·13	49·26	49·40	49·52	49·64	49
50	49·34	49·47	49·60	49·74	49·87	50·13	50·26	50·40	50·53	50·66	50

REDUCTION OF VOLUMES OF GASES

volumes of gases to a pressure of 760 mm.—Continued.

760	750	752	754	756	758	762	764	766	768	770	760
51	50·88	50·46	50·60	50·74	50·87	51·14	51·27	51·41	51·54	51·67	51
52	51·82	51·45	51·59	51·78	51·87	52·14	52·28	52·42	52·55	52·68	52
53	52·80	52·44	52·58	52·78	52·87	53·14	53·28	53·42	53·56	53·70	53
54	53·29	53·48	53·57	53·72	53·86	54·14	54·28	54·43	54·57	54·72	54
55	54·28	54·42	54·56	54·71	54·86	55·15	55·29	55·44	55·58	55·78	55
56	55·26	55·41	55·56	55·71	55·86	56·15	56·29	56·45	56·59	56·74	56
57	56·25	56·40	56·55	56·70	56·85	57·15	57·30	57·45	57·60	57·76	57
58	57·24	57·39	57·54	57·69	57·85	58·15	58·30	58·46	58·61	58·77	58
59	58·22	58·38	58·53	58·69	58·85	59·16	59·31	59·47	59·62	59·78	59
60	59·21	59·37	59·52	59·68	59·84	60·16	60·32	60·47	60·63	60·79	60
61	60·20	60·36	60·52	60·68	60·84	61·16	61·32	61·48	61·64	61·81	61
62	61·19	61·35	61·51	61·67	61·84	62·16	62·33	62·49	62·65	62·82	62
63	62·17	62·34	62·50	62·67	62·83	63·17	63·33	63·50	63·67	63·84	63
64	63·16	63·33	63·49	63·66	63·83	64·17	64·34	64·51	64·68	64·85	64
65	64·15	64·32	64·49	64·66	64·83	65·17	65·34	65·51	65·69	65·86	65
66	65·13	65·31	65·48	65·65	65·82	66·17	66·35	66·52	66·70	66·88	66
67	66·12	66·30	66·47	66·64	66·82	67·18	67·35	67·52	67·71	67·89	67
68	67·10	67·29	67·46	67·64	67·82	68·18	68·36	68·54	68·72	68·90	68
69	68·09	68·28	68·45	68·63	68·82	69·18	69·36	69·54	69·73	69·91	69
70	69·08	69·26	69·44	69·63	69·82	70·18	70·37	70·55	70·74	70·92	70
71	70·07	70·25	70·43	70·62	70·81	71·19	71·37	71·56	71·75	71·94	71
72	71·05	71·24	71·43	71·62	71·81	72·19	72·38	72·57	72·76	72·95	72
73	72·04	72·23	72·42	72·61	72·81	73·19	73·38	73·57	73·77	73·97	73
74	73·03	73·22	73·41	73·61	73·80	74·19	74·39	74·58	74·78	74·98	74
75	74·01	74·21	74·40	74·60	74·80	75·20	75·39	75·59	75·79	75·99	75
76	75·00	75·20	75·40	75·60	75·80	76·20	76·40	76·60	76·80	77·01	76
77	75·99	76·19	76·39	76·59	76·79	77·20	77·40	77·60	77·81	78·02	77
78	76·97	77·18	77·38	77·58	77·79	78·20	78·41	78·61	78·82	79·03	78
79	77·96	78·17	78·37	78·58	78·79	79·21	79·41	79·62	79·83	80·04	79
80	78·94	79·16	79·36	79·58	79·79	80·21	80·42	80·63	80·84	81·06	80
81	79·93	80·15	80·35	80·57	80·79	81·21	81·42	81·64	81·85	82·07	81
82	80·92	81·14	81·35	81·56	81·78	82·21	82·43	82·65	82·87	83·09	82
83	81·91	82·13	82·34	82·56	82·78	83·22	83·44	83·66	83·88	84·10	83
84	82·90	83·12	83·34	83·56	83·78	84·22	84·44	84·66	84·89	85·11	84
85	83·88	84·11	84·33	84·55	84·78	85·22	85·45	85·67	85·90	86·13	85
86	84·87	85·10	85·32	85·55	85·78	86·22	86·46	86·67	86·91	87·14	86
87	85·85	86·08	86·31	86·54	86·77	87·23	87·46	87·68	87·92	88·15	87
88	86·84	87·07	87·30	87·54	87·77	88·23	88·47	88·69	88·93	89·17	88
89	87·82	88·06	88·29	88·53	88·77	89·23	89·47	89·70	89·94	90·18	89
90	88·81	89·05	89·29	89·52	89·77	90·23	90·48	90·71	90·95	91·19	90
91	89·80	90·04	90·28	90·52	90·76	91·24	91·48	91·72	91·96	92·21	91
92	90·79	91·03	91·27	91·51	91·76	92·24	92·49	92·73	92·97	93·22	92
93	91·77	92·02	92·26	92·51	92·76	93·24	93·49	93·73	93·98	94·23	93
94	92·76	93·01	93·26	93·50	93·75	94·24	94·49	94·74	94·99	95·24	94
95	93·74	94·00	94·25	94·50	94·75	95·25	95·50	95·75	96·00	96·26	95
96	94·73	94·98	95·24	95·49	95·75	96·25	96·51	96·76	97·01	97·27	96
97	95·72	95·97	96·23	96·49	96·75	97·25	97·51	97·77	98·02	98·29	97
98	96·70	96·96	97·22	97·48	97·74	98·25	98·52	98·77	99·03	99·30	98
99	97·69	97·95	98·21	98·48	98·74	99·26	99·52	99·78	100·04	100·31	99
100	98·68	98·95	99·21	99·47	99·74	100·26	100·53	100·79	101·05	101·32	100

TABLE 21.—FACTORS FOR REDUCING A
TEMPERATURE

0° Centigrade, and 760 millimetres, or 32°

Centigrade.		0-0.	1-1.	2-2.	3-3.	4-4.	5-6.	6-7.	7-8.	8-9.
Fahrenheit.		32°.	34°.	36°.	38°.	40°.	42°.	44°.	46°.	48°.
In.	Milli- metres.									
27-5	698-5	·9191	·9154	·9116	·9079	·9043	·9007	·8972	·8936	·8899
27-6	701-0	·9224	·9188	·9149	·9112	·9076	·9040	·9005	·9001	·8964
27-7	708-6	·9258	·9221	·9183	·9145	·9109	·9073	·9037	·9001	·8964
27-8	706-1	·9291	·9254	·9215	·9179	·9142	·9105	·9070	·9034	·8996
27-9	708-6	·9325	·9288	·9249	·9212	·9174	·9138	·9102	·9067	·9029
28-0	711-2	·9358	·9321	·9282	·9244	·9208	·9170	·9135	·9099	·9061
28-1	718-7	·9391	·9354	·9315	·9278	·9241	·9205	·9167	·9131	·9093
28-2	716-3	·9425	·9387	·9348	·9310	·9273	·9236	·9200	·9164	·9125
28-3	718-8	·9458	·9421	·9382	·9344	·9306	·9269	·9233	·9197	·9158
28-4	721-3	·9491	·9454	·9415	·9377	·9339	·9301	·9265	·9229	·9190
28-5	728-9	·9525	·9487	·9448	·9410	·9372	·9334	·9298	·9262	·9223
28-6	726-4	·9558	·9520	·9481	·9443	·9405	·9367	·9331	·9294	·9255
28-7	728-9	·9592	·9554	·9514	·9476	·9438	·9400	·9364	·9327	·9287
28-8	731-5	·9625	·9587	·9547	·9509	·9471	·9432	·9396	·9359	·9320
28-9	734-0	·9659	·9620	·9580	·9542	·9504	·9465	·9429	·9392	·9352
29-0	736-6	·9692	·9654	·9613	·9575	·9536	·9498	·9462	·9424	·9385
29-1	739-1	·9725	·9687	·9647	·9608	·9569	·9531	·9494	·9457	·9417
29-2	741-6	·9759	·9720	·9680	·9640	·9602	·9563	·9527	·9489	·9449
29-3	744-2	·9792	·9753	·9713	·9674	·9635	·9596	·9559	·9522	·9481
29-4	746-7	·9826	·9787	·9746	·9707	·9668	·9629	·9592	·9554	·9514
29-5	749-3	·9859	·9820	·9779	·9740	·9701	·9662	·9624	·9587	·9546
29-6	751-8	·9893	·9853	·9812	·9773	·9733	·9694	·9657	·9619	·9578
29-7	754-3	·9926	·9887	·9845	·9806	·9766	·9727	·9690	·9652	·9611
29-8	756-9	·9959	·9920	·9879	·9839	·9800	·9760	·9722	·9684	·9643
29-9	759-4	·9993	·9954	·9912	·9872	·9832	·9793	·9755	·9717	·9676
30-0	762-0	1-0026	·9987	·9945	·9905	·9865	·9826	·9788	·9749	·9708
30-1	764-5	1-0060	1-0020	·9978	·9938	·9898	·9858	·9820	·9782	·9740
30-2	767-0	1-0093	1-0053	1-0011	·9971	·9931	·9891	·9853	·9814	·9773
30-3	769-6	1-0126	1-0086	1-0044	1-0004	·9964	·9924	·9885	·9846	·9805
30-4	772-1	1-0160	1-0120	1-0078	1-0037	·9997	·9957	·9918	·9879	·9837
30-5	774-7	1-0194	1-0153	1-0111	1-0070	1-0030	·9989	·9950	·9911	·9870
30-6	777-2	1-0227	1-0186	1-0144	1-0103	1-0063	1-0022	·9983	·9944	·9902
30-7	779-7	1-0260	1-0220	1-0177	1-0136	1-0096	1-0055	1-0016	·9976	·9935
30-8	782-3	1-0294	1-0253	1-0210	1-0169	1-0128	1-0087	1-0048	1-0009	·9967
30-9	784-8	1-0327	1-0286	1-0243	1-0202	1-0161	1-0120	1-0081	1-0041	1-0000
31-0	787-4	1-0360	1-0319	1-0276	1-0235	1-0194	1-0153	1-0114	1-0074	1-0032



NORMAL TEMPERATURE AND PRESSURE 51

GIVEN VOLUME OF GAS TO NORMAL AND PRESSURE.

Fahrenheit, and 29.92 inches barometric pressure.

Centigrade.	10.0.	11.1.	12.2.	13.3.	14.4.	15.6.	16.7.	17.8.
Fahrenheit.	50°.	52°.	54°.	56°.	58°.	60°.	62°.	64°.
In. Millimetres.								
27.5	698.5	.8867	.8882	.8797	.8768	.8728	.8695	.8668
27.6	701.0	.8900	.8864	.8829	.8795	.8760	.8726	.8690
27.7	703.6	.8932	.8897	.8861	.8827	.8792	.8758	.8724
27.8	706.1	.8964	.8928	.8892	.8859	.8823	.8790	.8756
27.9	708.6	.8996	.8960	.8925	.8890	.8855	.8821	.8787
28.0	711.2	.9029	.8992	.8957	.8922	.8887	.8853	.8819
28.1	713.7	.9060	.9025	.8989	.8954	.8919	.8884	.8850
28.2	716.3	.9093	.9057	.9021	.8986	.8951	.8916	.8882
28.3	718.8	.9125	.9089	.9053	.9018	.8983	.8948	.8913
28.4	721.3	.9157	.9121	.9085	.9050	.9014	.8979	.8945
28.5	723.9	.9189	.9153	.9117	.9082	.9046	.9011	.8976
28.6	726.4	.9222	.9185	.9149	.9114	.9077	.9042	.9008
28.7	728.9	.9254	.9218	.9181	.9145	.9109	.9074	.9039
28.8	731.5	.9286	.9250	.9213	.9177	.9141	.9106	.9071
28.9	734.0	.9318	.9282	.9245	.9209	.9173	.9138	.9102
29.0	736.6	.9351	.9314	.9277	.9241	.9205	.9169	.9134
29.1	739.1	.9383	.9346	.9309	.9273	.9236	.9201	.9165
29.2	741.6	.9415	.9378	.9341	.9305	.9268	.9233	.9197
29.3	744.2	.9448	.9410	.9373	.9336	.9300	.9264	.9228
29.4	746.7	.9480	.9443	.9405	.9368	.9332	.9296	.9260
29.5	749.3	.9512	.9475	.9437	.9400	.9363	.9328	.9291
29.6	751.8	.9544	.9506	.9469	.9432	.9395	.9359	.9323
29.7	754.3	.9577	.9539	.9501	.9464	.9427	.9390	.9354
29.8	756.9	.9609	.9571	.9533	.9496	.9459	.9422	.9386
29.9	759.4	.9641	.9603	.9565	.9528	.9490	.9454	.9417
30.0	762.0	.9673	.9635	.9597	.9560	.9522	.9486	.9449
30.1	764.5	.9706	.9667	.9629	.9591	.9554	.9517	.9480
30.2	767.0	.9738	.9700	.9661	.9623	.9586	.9549	.9512
30.3	769.6	.9770	.9731	.9692	.9655	.9617	.9580	.9543
30.4	772.1	.9802	.9764	.9725	.9687	.9649	.9612	.9575
30.5	774.7	.9835	.9796	.9757	.9719	.9681	.9643	.9606
30.6	777.2	.9867	.9828	.9789	.9751	.9712	.9675	.9638
30.7	779.7	.9899	.9860	.9821	.9783	.9744	.9707	.9669
30.8	782.3	.9931	.9892	.9853	.9815	.9777	.9738	.9701
30.9	784.8	.9963	.9924	.9885	.9846	.9807	.9770	.9732
31.0	787.4	.9996	.9956	.9917	.9878	.9840	.9801	.9764

TABLE 21—Continued.

Centigrade.		18·9	20.	21·1.	22·2.	23·3.	24·4.	25·6.	26·7.
Fahrenheit.		66°.	68°.	70°.	72°.	74°.	76°.	78°.	80°.
In.	Milli- metres.								
27·5	698·5	·8595	·8568	·8580	·8498	·8466	·8485	·8408	·8872
27·6	701·0	·8626	·8594	·8561	·8529	·8497	·8465	·8484	·8408
27·7	708·6	·8658	·8625	·8592	·8560	·8528	·8496	·8464	·8488
27·8	706·1	·8689	·8656	·8623	·8591	·8559	·8527	·8495	·8468
27·9	708·6	·8720	·8687	·8654	·8622	·8589	·8557	·8525	·8494
28·0	711·2	·8751	·8718	·8685	·8653	·8620	·8588	·8556	·8524
28·1	718·7	·8783	·8750	·8716	·8684	·8651	·8619	·8587	·8555
28·2	716·8	·8814	·8781	·8747	·8714	·8682	·8649	·8617	·8585
28·3	718·8	·8845	·8812	·8778	·8745	·8713	·8680	·8648	·8616
28·4	721·3	·8876	·8843	·8809	·8776	·8743	·8711	·8678	·8646
28·5	723·9	·8908	·8874	·8840	·8807	·8774	·8741	·8709	·8677
28·6	726·4	·8939	·8906	·8872	·8838	·8805	·8772	·8739	·8707
28·7	728·9	·8970	·8936	·8903	·8869	·8836	·8803	·8770	·8738
28·8	731·5	·9002	·8968	·8934	·8900	·8866	·8833	·8800	·8768
28·9	734·0	·9033	·8999	·8965	·8931	·8897	·8864	·8831	·8798
29·0	736·6	·9064	·9030	·8996	·8962	·8928	·8895	·8862	·8829
29·1	739·1	·9095	·9061	·9027	·8993	·8959	·8925	·8892	·8859
29·2	741·6	·9127	·9092	·9058	·9023	·8990	·8956	·8923	·8890
29·3	744·2	·9158	·9123	·9089	·9054	·9020	·8987	·8953	·8920
29·4	746·7	·9189	·9154	·9120	·9085	·9051	·9017	·8984	·8951
29·5	749·3	·9220	·9186	·9151	·9116	·9082	·9048	·9014	·8981
29·6	751·8	·9252	·9217	·9182	·9147	·9113	·9079	·9045	·9012
29·7	754·3	·9283	·9248	·9213	·9178	·9144	·9109	·9076	·9042
29·8	756·9	·9314	·9279	·9244	·9209	·9174	·9140	·9106	·9072
29·9	759·4	·9345	·9310	·9275	·9240	·9205	·9171	·9137	·9103
30·0	762·0	·9377	·9341	·9306	·9271	·9236	·9201	·9167	·9133
30·1	764·5	·9408	·9372	·9337	·9302	·9267	·9232	·9198	·9164
30·2	767·0	·9439	·9403	·9368	·9333	·9297	·9263	·9228	·9194
30·3	769·6	·9470	·9435	·9399	·9364	·9328	·9293	·9259	·9225
30·4	772·1	·9502	·9466	·9430	·9394	·9359	·9324	·9289	·9255
30·5	774·7	·9533	·9497	·9461	·9425	·9390	·9355	·9320	·9286
30·6	777·2	·9564	·9528	·9492	·9456	·9421	·9385	·9351	·9316
30·7	779·7	·9595	·9559	·9523	·9487	·9451	·9416	·9381	·9346
30·8	782·3	·9627	·9590	·9554	·9518	·9482	·9447	·9412	·9377
30·9	784·8	·9658	·9621	·9585	·9549	·9513	·9477	·9442	·9407
31·0	787·4	·9689	·9653	·9616	·9580	·9544	·9508	·9473	·9438

TABLE 21a.—VOLUMES OF WATER AT DIFFERENT TEMPERATURES. (Rossetti.)

Temp. °C.		Temp. °C.		Temp. °C.	
0	1	14	1·000556	40	1·007531
1	0·999947	15	1·000695	45	1·009541
2	0·999908	16	1·000846	50	1·011766
3	0·999885	17	1·001010	55	1·014100
4	0·999877	18	1·001184	60	1·016590
5	0·999883	19	1·001370	65	1·019302
6	0·999903	20	1·001567	70	1·022246
7	0·999938	21	1·001776	75	1·025440
8	0·999986	22	1·001995	80	1·028581
9	1·000048	23	1·002225	85	1·031894
10	1·000124	24	1·002465	90	1·035397
11	1·000213	25	1·002715	95	1·039094
12	1·000314	30	1·004064	100	1·042986
13	1·000429	35	1·005697		

TABLE 22.—REDUCTION OF WATER PRESSURE TO MERCURIAL PRESSURE.

sq.	Hg.	sq.	Hg.	sq.	Hg.	sq.	Hg.	sq.	Hg.
1	0·07	23	1·70	45	3·32	67	4·94	89	6·57
2	0·15	24	1·77	46	3·39	68	5·02	90	6·64
3	0·22	25	1·84	47	3·47	69	5·09	91	6·72
4	0·30	26	1·92	48	3·54	70	5·17	92	6·79
5	0·37	27	1·98	49	3·62	71	5·24	93	6·86
6	0·44	28	2·07	50	3·69	72	5·31	94	6·94
7	0·52	29	2·14	51	3·76	73	5·39	95	7·01
8	0·59	30	2·21	52	3·84	74	5·46	96	7·08
9	0·66	31	2·29	53	3·91	75	5·54	97	7·16
10	0·74	32	2·36	54	3·99	76	5·61	98	7·23
11	0·81	33	2·44	55	4·06	77	5·68	99	7·31
12	0·89	34	2·51	56	4·13	78	5·76	100	7·38
13	0·96	35	2·58	57	4·21	79	5·83	200	14·76
14	1·03	36	2·66	58	4·28	80	5·90	300	22·14
15	1·12	37	2·73	59	4·35	81	5·98	400	29·52
16	1·18	38	2·80	60	4·43	82	6·05	500	36·90
17	1·26	39	2·88	61	4·50	83	6·13	600	44·28
18	1·33	40	2·95	62	4·58	84	6·20	700	51·66
19	1·40	41	3·03	63	4·65	85	6·27	800	59·04
20	1·38	42	3·10	64	4·72	86	6·35	900	66·42
21	1·55	43	3·17	65	4·80	87	6·42	1000	73·80
22	1·62	44	3·25	66	4·87	88	6·49		

TABLE 23.—TENSION OF AQUEOUS VAPOUR

Between -20° and $+118^{\circ}$ C. in Millimetres Mercury.
(Magnus.)

T.	mm.	T.	mm.	T.	mm.
-20°	0·916	$+15^{\circ}$	12·677	$+50^{\circ}$	92·0
19	0·999	16	13·519	51	96·6
18	1·089	17	14·409	52	101·5
17	1·186	18	15·351	53	106·6
16	1·290	19	16·345	54	111·9
15	1·403	20	17·396	55	117·4
14	1·525	21	18·505	56	123·1
13	1·655	22	19·675	57	129·1
12	1·796	23	20·909	58	135·3
11	1·947	24	22·211	59	141·8
10	2·109	25	23·582	60	148·6
9	2·284	26	25·026	61	155·6
8	2·471	27	26·547	62	162·9
7	2·671	28	28·148	63	170·5
6	2·886	29	29·832	64	178·4
5	3·110	30	31·602	65	186·6
4	3·361	31	33·5	66	195·1
3	3·624	32	35·4	67	204·0
2	3·900	33	37·5	68	213·2
1	4·205	34	39·6	69	222·7
0	4·525	35	41·9	70	232·6
$+1$	4·867	36	44·3	71	242·9
2	5·231	37	46·8	72	253·5
3	5·619	38	49·4	73	264·6
4	6·032	39	52·1	74	276·0
5	6·471	40	55·0	75	287·9
6	6·939	41	58·0	76	300·2
7	7·436	42	61·1	77	312·9
8	7·964	43	64·4	78	326·1
9	8·525	44	67·8	79	339·8
10	9·126	45	71·4	80	353·9
11	9·756	46	75·2	81	368·6
12	10·421	47	79·1	82	383·7
13	11·130	48	83·2	83	399·4
14	11·882	49	87·5	84	415·6

TABLE 23—Continued.

T.	mm.	T.	mm.	T.	mm.
+ 85°	432·3	+ 97°	681·7	+ 109°	1041·3
86	449·6	98	707·0	110	1077·3
87	467·5	99	733·1	111	1114·3
88	486·0	100	760·0	112	1152·3
89	505·0	101	787·7	113	1191·4
90	524·8	102	816·3	114	1231·7
91	545·1	103	845·7	115	1273·0
92	566·1	104	876·0	116	1315·5
93	587·8	105	907·1	117	1359·1
94	610·2	106	939·2	118	1403·9
95	633·3	107	972·3		
96	657·1	108	1006·3		

TABLE 24.—TENSION OF AQUEOUS VAPOUR FOR TEMPERATURES FROM 40° C.

Temperature Centigrade.	Tension in mm.	Pressure in atmospheres.	Pressure per sq. cm. in kilos.
+ 40°	54·906	0·072	0·07465
45	71·391	0·094	0·09706
50	91·982	0·121	0·12505
55	117·478	0·154	0·15972
60	148·791	0·196	0·20323
65	186·945	0·246	0·25417
70	233·093	0·306	0·31692
75	288·517	0·380	0·39227
80	354·643	0·466	0·48217
85	433·041	0·570	0·58877
90	525·450	0·691	0·71440
95	633·778	0·834	0·86168
100	760·00	1·000	1·03330
105	906·41	1·193	1·23236
110	1075·37	1·415	1·46210
115	1269·41	1·673	1·72592
120	1491·28	1·962	2·02755
125	1743·88	2·294	2·37098
130	2030·28	2·671	2·76037
135	2353·73	3·097	3·20013

TABLE 24—Continued.

Temperature Centigrade.	Tension in mm.	Pressure in atmospheres.	Pressure per sq.cm. in kilos.
+140°	2717.63	3.575	3.69490
145	3125.55	4.112	4.24950
150	3531.23	4.712	4.86904
155	4088.56	5.380	5.55881
160	4651.62	6.120	6.32434
165	5274.54	6.940	7.17127
170	5961.66	7.844	8.10547
175	6717.43	8.838	9.13302
180	7546.39	9.929	10.2601
185	8453.23	11.122	11.4930
190	9442.70	12.424	12.8383
195	10519.73	13.841	14.3025
200	11688.96	15.380	15.8923
205	12955.66	17.047	17.6145
210	14324.80	18.848	19.4760
215	15801.33	20.791	21.4835
220	17390.00	22.881	23.6439
225	19097.04	25.127	25.9643
230	20926.40	27.534	28.4515
Temperature Fahrenheit.	Tension in inches of Mercury.	Pressure in atmospheres.	Pressure in lbs. per square inch.
100°	1.918	.064	.941
110	2.577	.086	1.267
120	3.427	.114	1.676
130	4.502	.150	2.205
140	5.858	.196	2.883
150	7.546	.252	3.705
160	9.628	.322	4.734
170	12.18	.407	5.984
180	15.27	.510	7.498
190	19.01	.635	9.336
200	23.46	.784	11.53
212	29.92	1.000	14.706
220	35.01	1.170	17.19
230	42.34	1.415	20.30
240	50.89	1.701	25.01

TABLE 24—*Continued.*

Temperature Fahrenheit.	Tension in inches of Mercury.	Pressure in atmospheres.	Pressure in lbs. per square inch.
250°	60·81	2·082	29·87
260	72·27	2·415	35·50
270	85·41	2·855	41·97
280	100·4	3·356	49·34
290	117·5	3·927	57·78
300	136·8	4·572	67·22
310	158·6	5·301	77·94
320	183·1	6·120	89·98
330	210·5	7·035	103·4
340	241·1	8·058	118·5
350	275·0	9·198	135·2
360	312·6	10·45	153·6
370	354·0	11·83	173·9
380	399·6	13·35	196·3
390	449·6	15·02	220·8
400	504·4	16·86	247·9
410	563·9	18·84	277·0
420	628·8	21·01	309·9
430	699·2	23·37	343·6
440	775·3	25·91	380·9

TABLE 25.—TENSION OF AQUEOUS VAPOUR IN
INCHES OF MERCURY FROM 1° TO 100° F.

Temperature Fahrenheit.	Inches of Mercury.	Temperature Fahrenheit.	Inches of Mercury.
1°	·046	11°	·071
2	·048	12	·074
3	·050	13	·078
4	·052	14	·082
5	·054	15	·086
6	·057	16	·090
7	·060	17	·094
8	·062	18	·098
9	·065	19	·103
10	·068	20	·108

TABLE 25—Continued.

Temperature Fahrenheit.	Inches of Mercury.	Temperature Fahrenheit.	Inches of Mercury.
21°	·118	61°	·587
22	·118	62	·556
23	·123	63	·576
24	·129	64	·596
25	·135	65	·617
26	·141	66	·639
27	·147	67	·661
28	·153	68	·685
29	·160	69	·708
30	·167	70	·733
31	·174	71	·759
32	·181	72	·785
33	·188	73	·812
34	·196	74	·840
35	·204	75	·868
36	·212	76	·897
37	·220	77	·927
38	·229	78	·958
39	·238	79	·990
40	·247	80	1·023
41	·257	81	1·057
42	·267	82	1·092
43	·277	83	1·128
44	·288	84	1·165
45	·299	85	1·203
46	·311	86	1·242
47	·323	87	1·282
48	·335	88	1·323
49	·348	89	1·366
50	·361	90	1·401
51	·374	91	1·455
52	·388	92	1·501
53	·403	93	1·548
54	·418	94	1·596
55	·433	95	1·646
56	·449	96	1·697
57	·465	97	1·751
58	·482	98	1·806
59	·500	99	1·862
60	·518	100	1·918

TABLE 26.—BOILING POINT OF WATER AT DIFFERENT BAROMETRIC PRESSURES.

Barometric Pressure.	Boiling Point.	Barometric Pressure.	Boiling Point.
mm.		mm.	
710	98·11	745	99·44
715	98·30	750	99·63
720	98·49	755	99·82
725	98·69	760	100·00
730	98·88	765	100·18
735	99·07	770	100·37
740	99·26	775	100·55

TABLE 27.—SPECIFIC HEATS.

(a) Of Solids and Liquids.

Aluminium	0·2220	Iron (cast)	0·1050
Alcohol	0·547	(wrought)	0·1081
Antimony	0·0495	Lead	0·0809
Ashes	0·20	Limestone (marble)	0·21
Bismuth	0·0308	Mercury	0·0384
Brass	0·0917	Nickel	0·109
Bricks	0·22	Oil (lubricating)	0·40
Cement	0·19	Platinum	0·0824
Carbon (wood)	0·1653	Sandstone	0·22
(graphite)	0·1604	Slag	0·18
(diamond)	0·1042	Silver	0·0559
Copper	0·0936	Steel	0·1070
Glass (for thermometers)	0·1988	Sulphur	0·1764
Gypsum	0·20	Sulphuric acid	0·332
Granite	0·20	Tin	0·0552
Gold	0·0816	Zinc	0·0985

(b) Of Gases and Vapours for Constant Pressures between the Temperatures of 0° and 200° C. (Langen and Regnault.)

	Cal. per 1 kg.	Cal. per 1 cb.m.		Cal. per 1 kg.	Cal. per 1 cb.m.
Atmospheric air	0·2389	0·3082	Carbon monoxide	0·2466	0·3082
Oxygen	0·2158	0·3082	Methane	0·5930	0·4241
Nitrogen	0·2459	0·3082	Ethylene	0·4040	0·5053
Hydrogen	3·452	0·3082	Sulphur dioxide	0·1544	0·4413
Carbon dioxide	0·2092	0·4109	Aqueous vapour	0·4542	0·3654

TABLE 28.—HEATING EFFECTS.

(a) Definitions.

A metrical gram-calorie (cal.) is the quantity of heat required to raise the temperature of 1 gram of water 1° C. The kilogram-calorie = 1000 cal.

The normal calorie is that which raises 1 gram water of 14·5° to 15·5° C.

The British heat unit is the quantity of heat required to raise the temperature of 1 pound of water from 32° to 33° Fahr., and is = 252 gram-calories. This unit is required only where the absolute values of the heat units are considered. Usually the question is only of relative values—*e.g.*, grams or lbs. of fuel on the one hand, against grams or lbs. of water on the other. For these comparisons the simple proportion of British heat units to gram-calories = 5 : 9 is used, as the unit of fuel weight is the same as that of the water, and only the degrees Centigrade and Fahrenheit differ as above. 1 British heat unit is, therefore, = $\frac{5}{9}$ = 0·5556 gram-calories.

1 Joule (j) = 10 million ergs = 0·2391 gram-calories.

1 Gram-calorie = 4·183 j.

1 J = 1000 j = 239·1 cal. = 10¹⁰ erg.

(b) Calorific Value of Fuels.

(The data given are the *upper* heating values, *i.e.*, they are referred to the combustion of hydrogen to liquid water as found in the calorimeter.)

	met. cal.		met. cal.
Alcohol	7,100	Petroleum residue	10,500
Lignite-tar oil	10,000	Petroleum	11,000
Wood	4,100	Fatty oils	9,300
Methyl alcohol	5,300	Tallow	8,370
Charcoal (C to CO ₂)	8,000	Bees' wax	9,000
„ (C to CO)	2,300	Cellulose	4,200

(c) Calorific Value of Gases.

	Molec. Weight.	Molec. Calories when burnt to		Calories per cub. met. when burnt to	
		Liquid Water.	Steam.	Liquid Water.	Steam.
Hydrogen, H ₂	2	69·0	58·1	3064	2585
Methane, CH ₄	16	213·5	192·1	9565	8606
Ethylene, C ₂ H ₄	28	334·8	313·4	14,999	14,060
Benzene vapour, C ₆ H ₆	78	788·0	755·9	35,302	33,864
Naphthalene vapour, C ₁₀ H ₈	128	1258·4	1230·6	56,376	55,131
Carbon monoxide, CO	28	68·4	68·4	3064	3064

TABLE 29.—AIR COMPRESSION.

The following table is compiled with a view to facilitate calculations of problems connected with the application of compressed gases. The table is strictly correct only for air, but is applicable also to other gases, such as lime-kiln gases. The table relates to 1 cub. foot of atmospheric air measured at 60° F. and 29·92 inches barometric pressure, and shows the volume, temperature, and pressure after adiabatic compression; also the height of a column of water which the compressed gas will just balance, and the power required to compress the air in foot-pounds (33,000 ft.-lbs. per minute = 1 indicated horse-power), and the mean pressure on the air piston.

Final Pressure lbs. per sq. in. above Atmosphere.	Column of Water the Gas will balance.	Volume of compressed Air.	Temperature after Compression.	Mean Pressure on Piston.	Foot-pounds of Work per cub. foot atmosph. air.
Lbs.	Feet.	Cub. feet.	Degrees F.	Lbs. persq.in.	
10	23·12	0·692	144·5	8·23	1186·3
12	27·75	0·655	158·1	9·58	1387
14	32·37	0·622	171·0	10·86	1564
16	37·00	0·593	184·0	12·08	1739
18	41·62	0·567	196·0	13·23	1907
20	46·25	0·544	207·3	14·35	2066
22	50·87	0·523	218·3	15·42	2220
24	55·50	0·504	228·6	16·45	2368
26	60·12	0·486	239·0	17·43	2510
28	64·75	0·469	249·0	18·39	2647
30	69·37	0·454	258·2	19·32	2782
32	74·00	0·440	267·5	20·21	2910
34	78·62	0·428	276·4	21·07	3034
36	83·25	0·416	285·3	21·92	3156
38	87·87	0·404	293·5	22·74	3275
40	92·50	0·394	301·8	23·53	3389

In Metrical Units.

Final Pressure above 1 atm. per sq.cm.	Column of Water the Gas will balance.	Volume of 1 cub.m. air after Com- pression.	Temperature after Compression.	Mean Pressure on Piston.	Work per 1 cub.m. in metre-kg.
Kg.	m.	cub.m.	°C.	Kg. persq.cm.	
0·703	7·05	0·692	62·5	0·579	5,789
0·844	8·44	0·655	70·1	0·674	6,769
0·984	9·87	0·622	77·2	0·764	7,633
1·125	11·28	0·593	84·4	0·849	8,488
1·266	12·69	0·567	91·1	0·930	9,307

TABLE 29—Continued.

Final Pressure above 1 atm. per sq.cm.	Column of Water the Gas will balance.	Volume of 1 cub.m. air after Compression.	Temperature after Compression.	Mean Pressure on Piston.	Work per 1 cub.m. in metre-kg.
Kg.	m.	cub.m.	°C.	Kg. persq.cm.	
1·406	14·10	0·544	97·4	1·009	9,791
1·547	15·50	0·523	103·5	1·084	10,835
1·687	16·91	0·504	109·2	1·157	11,557
1·828	18·32	0·486	115·9	1·226	12,251
1·969	19·74	0·469	120·6	1·293	12,919
2·109	21·14	0·454	125·7	1·358	13,573
2·250	22·55	0·440	130·8	1·421	14,203
2·391	23·96	0·428	135·8	1·481	14,808
2·531	25·37	0·416	140·7	1·541	15,403
2·674	26·78	0·404	145·4	1·599	15,984
2·812	28·19	0·394	149·9	1·654	16,541

TABLE 30.—EXPLOSIVE MIXTURES OF GASES AND AIR. (Hitner.)

	Volumes of Gas.	Volumes of Air.
Acetylene	3·5-52·2	96·5-47·8
Hydrogen	9·5-66·3	90·5-33·7
Carbon monoxide	16·6-77·8	83·4-25·2
Ethylene	4·2-14·5	95·8-85·5
Methane	6·2-12·7	93·8-87·3
Coal-gas	8·0-19	92·0-81
Benzene vapour	2·7- 6·3	97·3-93·7
Petroleum spirit vapour	2·5- 4·8	97·5-95·2
Ether	2·9- 7·5	97·1-92·5

TABLE 81.—PROPERTIES OF THE LIQUEFIED GASES WHICH OCCUR IN COMMERCE.
By Dr A. LANGE.

	Specific gravity at			Vapour tension (atm.) at			1 kg. at 0° and 760 mm. = a gas volume of	Critical temperature.	Critical pressure.	Boiling point at 760 mm. pressure.	Melting point.	Conditions of transit on German Railways.		
	0°.	15°.	80°.	0°.	15°.	80°.						Litres.	Atm.	Yrs.
Nitrous oxide	0.937	0.870	...	36.1	49.8	68.0	506	36	75	- 87.9	- 115	1.34	180	4
Carbon dioxide	0.947	0.864	0.732	35.4	52.2	73.8	506	31.8	77	- 78.2	- 65	1.34	190	4
Sulphur dioxide	1.435	1.396	1.349	1.5	2.7	4.5	348	155.4	78.9	- 10.0	- 79	0.8	12	2
Chlorine*	1.468	1.426	1.380	3.7	5.8	8.7	316	146	98.5	- 33.6	- 102	0.8	22	2
Ammonia	0.634	0.614	0.592	4.2	7.1	11.4	1813	180	115	- 33.7	- 75	0.8	30	4
Phosgen	0.8	30	2

* For Chlorine, compare also the statements of Knietoch in the special part of this book.

TABLE 32.—ELECTRICAL UNITS.

1. The unit of quantity, the **coulomb**, is that quantity of current which precipitates 1·118 mg. silver from a solution of silver nitrate.

2. The unit of current, the **ampere**, is that current which conveys 1 coulomb through the circuit in 1 second.

1 **ampere-hour** is = the quantity of current which gives per hour 1 ampere, or per n hours, $\frac{1}{n}$ amperes = 3600 coulombs.

3. The unit of resistance, the **ohm**, is equal to the resistance of a column of mercury at 0° C. of a sectional area of 1×1 mm., 106·3 cm. long, possessing a mass of 14·4251 grams. Other units in use are the Siemens Unit = 0·944 ohms, and the British Association Unit (B.A.U.) = 0·989 ohms.

4. The unit of electromotive force, the **volt**, is the force which in a conductor with a resistance of 1 ohm gives a current = 1 ampere.

Electromotive force of a Daniell cell = 1·12 volts.

„ „ Bunsen cell, = 2 volts.

„ „ Clark cell = 1·4328 volts.

„ „ Weston cell = 0·0186 volt.

„ „ lead storage cell = 2·1-1·9 volts.

5. The **farad** is the capacity of a condenser in which a charge of 1 coulomb produces a difference of potential of 1 volt.

6. A **watt** or **volt-ampere** is the amount of *work* produced during 1 second by a current of 1 ampere under an electromotive force of 1 volt. It is = $\frac{1 \text{ metre-kilogram}}{9\cdot81}$ per second = 0·102 m.kg.; hence 1 horse-power = 735·5 watts. The British Board of Trade Unit is = 1000 watt hours.

A current of 1 ampere, at a resistance of w ohms, produces during t seconds a quantity of heat = 0·239 wt gram-calories. 1 cal. = 4·19 joules.

TABLE 33.—ELECTRO-CHEMICAL EQUIVALENTS.

The separation of a gram equivalent requires 96,540 coulombs = 26·86 ampere hours. 1 ampere hour is capable of yielding :—

At the Cathode.	Grams.	At the Anode.	Grams.
Silver	4·0248	Chlorine	1·322
Copper (from solutions of cupric salts)	1·186	Bromine	2·982
Zinc	1·219	Iodine	4·730
Nickel	1·094	Oxygen	0·2983
Hydrogen	0·0875	Potassium chlorate	0·7618
		Potassium hydroxide	2·094
		Sodium hydroxide .	1·494

TABLE 34.—MATHEMATICAL TABLES.

Circumference and area of circles, squares, cubes, square and cube roots.

n	πn ○	$\frac{\pi n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
1.0	3.142	0.7854	1.000	1.000	1.0000	1.0000
1.1	3.456	0.9503	1.210	1.331	1.0488	1.0323
1.2	3.770	1.1310	1.440	1.728	1.0955	1.0627
1.3	4.084	1.3273	1.690	2.197	1.1402	1.0914
1.4	4.398	1.5394	1.960	2.744	1.1832	1.1187
1.5	4.712	1.7672	2.250	3.375	1.2247	1.1447
1.6	5.027	2.0106	2.560	4.096	1.2649	1.1696
1.7	5.341	2.2698	2.890	4.913	1.3038	1.1935
1.8	5.655	2.5447	3.240	5.832	1.3416	1.2164
1.9	5.969	2.8353	3.610	6.859	1.3784	1.2386
2.0	6.283	3.1416	4.000	8.000	1.4142	1.2599
2.1	6.597	3.4636	4.410	9.261	1.4491	1.2806
2.2	6.912	3.8013	4.840	10.648	1.4832	1.3006
2.3	7.226	4.1548	5.290	12.167	1.5166	1.3200
2.4	7.540	4.5239	5.760	13.824	1.5492	1.3389
2.5	7.854	4.9087	6.250	15.625	1.5811	1.3572
2.6	8.168	5.3093	6.760	17.576	1.6125	1.3751
2.7	8.482	5.7256	7.290	19.683	1.6432	1.3925
2.8	8.797	6.1575	7.840	21.952	1.6733	1.4095
2.9	9.111	6.6052	8.410	24.389	1.7029	1.4260
3.0	9.425	7.0686	9.000	27.000	1.7321	1.4422
3.1	9.739	7.5477	9.610	29.791	1.7607	1.4581
3.2	10.053	8.0425	10.24	32.768	1.7889	1.4736
3.3	10.367	8.5530	10.89	35.937	1.8166	1.4888
3.4	10.681	9.0792	11.56	39.304	1.8439	1.5037
3.5	10.996	9.6211	12.25	42.875	1.8708	1.5183
3.6	11.310	10.179	12.96	46.656	1.8974	1.5326
3.7	11.624	10.752	13.69	50.653	1.9235	1.5467
3.8	11.938	11.341	14.44	54.872	1.9494	1.5605
3.9	12.252	11.946	15.21	59.319	1.9748	1.5741
4.0	12.566	12.566	16.00	64.000	2.0000	1.5874
4.1	12.881	13.203	16.81	68.921	2.0249	1.6005
4.2	13.195	13.854	17.64	74.088	2.0494	1.6134
4.3	13.509	14.522	18.49	79.507	2.0736	1.6261
4.4	13.823	15.205	19.36	85.184	2.0976	1.6386
4.5	14.137	15.904	20.25	91.125	2.1213	1.6510
4.6	14.451	16.619	21.16	97.336	2.1448	1.6631
4.7	14.765	17.349	22.09	103.828	2.1680	1.6751

TABLE 34—Continued.

n	πn ○	$\frac{\pi n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
4·8	15·080	18·096	23·04	110·592	2·1909	1·6869
4·9	15·394	18·857	24·01	117·649	2·2136	1·6985
5·0	15·708	19·635	25·00	125·000	2·2361	1·7100
5·1	16·022	20·428	26·01	132·651	2·2583	1·7213
5·2	16·336	21·237	27·04	140·608	2·2804	1·7325
5·3	16·650	22·062	28·09	148·877	2·3022	1·7435
5·4	16·965	22·902	29·16	157·464	2·3238	1·7544
5·5	17·279	23·758	30·25	166·375	2·3452	1·7652
5·6	17·593	24·630	31·36	175·616	2·3664	1·7758
5·7	17·907	25·518	32·49	185·193	2·3875	1·7863
5·8	18·221	26·421	33·64	195·112	2·4083	1·7967
5·9	18·535	27·340	34·81	205·379	2·4290	1·8070
6·0	18·850	28·274	36·00	216·000	2·4495	1·8171
6·1	19·164	29·225	37·21	226·981	2·4698	1·8272
6·2	19·478	30·191	38·44	238·328	2·4900	1·8371
6·3	19·792	31·173	39·69	250·047	2·5100	1·8469
6·4	20·106	32·170	40·96	262·144	2·5298	1·8566
6·5	20·420	33·183	42·25	274·625	2·5495	1·8663
6·6	20·735	34·212	43·56	287·496	2·5691	1·8758
6·7	21·049	35·257	44·89	300·763	2·5884	1·8852
6·8	21·363	36·317	46·24	314·432	2·6077	1·8945
6·9	21·677	37·393	47·61	328·509	2·6268	1·9038
7·0	21·991	38·485	49·00	343·000	2·6458	1·9129
7·1	22·305	39·592	50·41	357·911	2·6646	1·9220
7·2	22·619	40·715	51·84	373·248	2·6833	1·9310
7·3	22·934	41·854	53·29	389·017	2·7019	1·9399
7·4	23·248	43·008	54·76	405·224	2·7203	1·9487
7·5	23·562	44·179	56·25	421·875	2·7386	1·9574
7·6	23·876	45·365	47·76	438·976	2·7568	1·9661
7·7	24·190	46·566	59·29	456·533	2·7749	1·9747
7·8	24·504	47·784	60·84	474·552	2·7929	1·9832
7·9	24·819	49·017	62·41	493·089	2·8107	1·9916
8·0	25·133	50·266	64·00	512·000	2·8284	2·0000
8·1	25·447	51·530	65·61	531·441	2·8461	2·0083
8·2	25·761	52·810	67·24	551·368	2·8636	2·0165
8·3	26·075	54·106	68·89	571·787	2·8810	2·0247
8·4	26·389	55·418	70·56	592·704	2·8983	2·0328

TABLE 34—Continued.

n	πn ○	$\frac{\pi n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
8·5	26·704	56·745	72·25	614·125	2·9155	2·0408
8·6	27·018	58·088	73·96	636·056	2·9326	2·0488
8·7	27·332	59·447	75·69	658·503	2·9496	2·0567
8·8	27·646	60·821	77·44	681·472	2·9665	2·0646
8·9	27·960	62·211	79·21	704·969	2·9833	2·0724
9·0	28·274	63·617	81·00	729·000	3·0000	2·0801
9·1	28·588	65·039	82·81	753·571	3·0166	2·0878
9·2	28·903	66·476	84·64	778·688	3·0332	2·0954
9·3	29·217	67·929	86·49	804·357	3·0496	2·1029
9·4	29·531	69·398	88·36	830·584	3·0659	2·1105
9·5	29·845	70·882	90·25	857·375	3·0822	2·1179
9·6	30·159	72·382	92·16	884·736	3·0984	2·1253
9·7	30·473	73·898	94·09	912·673	3·1145	2·1327
9·8	30·788	75·430	96·04	941·192	3·1305	2·1400
9·9	31·102	76·977	98·01	970·299	3·1464	2·1472
10·0	31·416	78·540	100·00	1000·000	3·1623	2·1544
10·1	31·730	80·119	102·01	1030·301	3·1780	2·1616
10·2	32·044	81·713	104·04	1061·208	3·1937	2·1687
10·3	32·358	83·323	106·09	1092·727	3·2094	2·1757
10·4	32·673	84·949	108·16	1124·864	3·2249	2·1828
10·5	32·987	86·590	110·25	1157·625	3·2404	2·1897
10·6	33·301	88·247	112·36	1191·016	3·2558	2·1967
10·7	33·615	89·920	114·49	1225·043	3·2711	2·2036
10·8	33·929	91·609	116·64	1259·712	3·2863	2·2104
10·9	34·243	93·313	118·81	1295·029	3·3015	2·2172
11·0	34·558	95·033	121·00	1331·000	3·3166	2·2239
11·1	34·872	96·769	123·21	1367·631	3·3317	2·2307
11·2	35·186	98·520	125·44	1404·928	3·3466	2·2374
11·3	35·500	100·29	127·69	1442·897	3·3615	2·2441
11·4	35·814	102·07	129·96	1481·544	3·3754	2·2506
11·5	36·128	103·87	132·25	1520·875	3·3912	2·2572
11·6	36·442	105·68	134·56	1560·896	3·4059	2·2637
11·7	36·757	107·51	136·89	1601·613	3·4205	2·2702
11·8	37·071	109·36	139·24	1643·032	3·4351	2·2766
11·9	37·385	111·22	141·61	1685·159	3·4496	2·2831
12·0	37·699	113·10	144·00	1728·000	3·4641	2·2894
12·1	38·013	114·99	146·41	1771·561	3·4785	2·2957
12·2	38·327	116·90	148·84	1815·848	3·4928	2·3021

TABLE 34—Continued.

n	πn ○	$\frac{\pi n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
12·3	38·642	118·82	151·29	1860·867	3·5071	2·3084
12·4	38·956	120·76	153·76	1906·624	3·5214	2·3146
12·5	39·270	122·72	156·25	1953·125	3·5355	2·3208
12·6	39·584	124·69	158·76	2000·376	3·5496	2·3270
12·7	39·898	126·68	161·29	2048·383	3·5637	2·3331
12·8	40·212	128·68	163·84	2097·152	3·5777	2·3392
12·9	40·527	130·70	166·41	2146·689	3·5917	2·3453
13·0	40·841	132·73	169·00	2197·000	3·6056	2·3513
13·1	41·155	134·78	171·61	2248·091	3·6194	2·3573
13·2	41·469	136·85	174·24	2299·968	3·6332	2·3633
13·3	41·783	138·93	176·89	2352·637	3·6469	2·3693
13·4	42·097	141·03	179·56	2406·104	3·6606	2·3752
13·5	42·412	143·14	182·25	2460·375	3·6742	2·3811
13·6	42·726	145·27	184·96	2515·456	3·6878	2·3870
13·7	43·040	147·41	187·69	2571·353	3·7013	2·3928
13·8	43·354	149·57	190·44	2628·072	3·7148	2·3986
13·9	43·668	151·75	193·21	2685·619	3·7283	2·4044
14·0	43·992	153·94	196·00	2744·000	3·7417	2·4101
14·1	44·296	156·15	198·81	2803·221	3·7550	2·4159
14·2	44·611	158·37	201·64	2863·288	3·7683	2·4216
14·3	44·925	160·61	204·49	2924·207	3·7815	2·4272
14·4	45·239	162·86	207·36	2985·984	3·7947	2·4329
14·5	45·553	165·13	210·25	3048·625	3·8079	2·4385
14·6	45·867	167·42	213·16	3112·136	3·8210	2·4441
14·7	46·181	169·72	216·09	3176·523	3·8341	2·4497
14·8	46·496	172·03	219·04	3241·792	3·8471	2·4552
14·9	46·810	174·37	222·01	3307·949	3·8600	2·4607
15·0	47·124	176·72	225·00	3375·000	3·8730	2·4662
15·1	47·438	179·08	228·09	3442·951	3·8859	2·4717
15·2	47·752	181·46	231·04	3511·808	3·8987	2·4772
15·3	48·066	183·85	234·09	3581·577	3·9115	2·4825
15·4	48·381	186·27	237·16	3652·264	3·9243	2·4879
15·5	48·695	188·69	240·25	3723·875	3·9370	2·4933
15·6	49·009	191·13	243·36	3796·416	3·9497	2·4986
15·7	49·323	193·59	246·49	3869·893	3·9623	2·5039
15·8	49·637	196·07	249·64	3944·312	3·9749	2·5092
15·9	49·951	198·56	252·81	4019·679	3·9875	2·5146

TABLE 34—Continued.

n	πn ○	$\frac{\pi n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
16·0	50·265	201·06	256·00	4096·000	4·0000	2·5198
16·1	50·580	203·58	259·21	4173·281	4·0125	2·5251
16·2	50·894	206·13	262·44	4251·528	4·0249	2·5303
16·3	51·208	208·67	265·69	4330·747	4·0373	2·5355
16·4	51·522	211·24	268·96	4410·944	4·0497	2·5406
16·5	51·836	213·83	272·25	4492·125	4·0620	2·5458
16·6	52·150	216·42	275·56	4574·296	4·0743	2·5509
16·7	52·465	219·04	278·89	4657·463	4·0866	2·5561
16·8	52·779	221·67	282·24	4741·632	4·0988	2·5612
16·9	53·093	224·32	285·61	4826·809	4·1110	2·5663
17·0	53·407	226·98	289·00	4913·000	4·1231	2·5713
17·1	53·721	229·66	292·41	5000·211	4·1352	2·5763
17·2	54·035	232·35	295·84	5088·448	4·1473	2·5813
17·3	54·350	235·06	299·29	5177·717	4·1593	2·5863
17·4	54·664	237·79	302·76	5268·024	4·1713	2·5913
17·5	54·978	240·53	306·25	5359·375	4·1833	2·5963
17·6	55·292	243·29	309·76	5451·776	4·1952	2·6012
17·7	55·606	246·06	313·29	5545·233	4·2071	2·6061
17·8	55·920	248·85	316·84	5639·752	4·2190	2·6109
17·9	56·235	251·65	320·41	5735·339	4·2308	2·6158
18·0	56·549	254·47	324·00	5832·000	4·2426	2·6207
18·1	56·863	257·30	327·61	5929·741	4·2544	2·6256
18·2	57·177	260·16	331·24	6028·568	4·2661	2·6304
18·3	57·491	263·02	334·89	6128·487	4·2778	2·6352
18·4	57·805	265·90	338·56	6229·504	4·2895	2·6400
18·5	58·119	268·80	342·25	6331·625	4·3012	2·6448
18·6	58·434	271·72	345·96	6434·856	4·3128	2·6495
18·7	58·748	274·65	349·69	6539·203	4·3243	2·6543
18·8	59·062	277·59	353·44	6644·672	4·3359	2·6590
18·9	59·376	280·55	357·21	6751·269	4·3474	2·6637
19·0	59·690	283·53	361·00	6859·000	4·3589	2·6684
19·1	60·004	286·52	364·81	6967·871	4·3703	2·6731
19·2	60·319	289·53	368·64	7077·888	4·3818	2·6777
19·3	60·633	292·55	372·49	7189·057	4·3942	2·6824
19·4	60·947	295·59	376·36	7301·384	4·4045	2·6869
19·5	61·261	298·65	380·25	7414·875	4·4159	2·6916
19·6	61·575	301·72	384·16	7529·536	4·4272	2·6962
19·7	61·889	304·81	388·09	7642·373	4·4385	2·7008

TABLE 34—Continued.

n	πn ○	$\frac{\pi n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
19·8	62·204	307·91	392·04	7762·392	4·4497	2·7053
19·9	62·518	311·03	396·01	7880·599	4·4609	2·7098
20·0	62·832	314·16	400·00	8000·000	4·4721	2·7144
20·1	63·146	317·31	404·01	8120·601	4·4833	2·7189
20·2	63·460	320·47	408·04	8242·408	4·4944	2·7234
20·3	63·774	323·66	412·09	8365·427	4·5055	2·7279
20·4	64·088	326·85	416·16	8489·664	4·5166	2·7324
20·5	64·403	330·06	420·25	8615·125	4·5277	2·7368
20·6	64·717	333·29	424·36	8741·816	4·5387	2·7413
20·7	65·031	336·54	428·49	8869·743	4·5497	2·7457
20·8	65·345	339·80	432·64	8998·912	4·5607	2·7502
20·9	65·659	343·07	436·81	9129·329	4·5716	2·7545
21·0	65·973	346·36	441·00	9261·000	4·5826	2·7589
21·1	66·288	349·67	445·21	9393·931	4·5935	2·7633
21·2	66·602	352·99	449·44	9528·128	4·6043	2·7676
21·3	66·916	356·33	453·69	9663·597	4·6152	2·7720
21·4	67·230	359·68	457·96	9800·344	4·6260	2·7763
21·5	67·544	363·05	462·25	9938·375	4·6368	2·7806
21·6	67·858	366·44	466·56	10077·696	4·6476	2·7849
21·7	68·173	369·84	470·89	10218·313	4·6583	2·7893
21·8	68·487	373·25	475·24	10360·232	4·6690	2·7935
21·9	68·801	376·69	479·41	10503·459	4·6797	2·7978
22·0	69·115	380·13	484·00	10648·000	4·6904	2·8021
22·1	69·429	383·60	488·41	10793·861	4·7011	2·8063
22·2	69·743	387·08	492·84	10941·048	4·7117	2·8105
22·3	70·058	390·57	497·29	11089·567	4·7223	2·8147
22·4	70·372	394·08	501·76	11239·424	4·7329	2·8189
22·5	70·686	397·61	506·25	11390·625	4·7434	2·8231
22·6	71·000	401·15	510·76	11543·176	4·7539	2·8273
22·7	71·314	404·71	515·29	11697·083	4·7644	2·8314
22·8	71·628	408·28	519·84	11852·352	4·7749	2·8356
22·9	71·942	411·87	524·41	12008·989	4·7854	2·8397
23·0	72·257	415·48	529·00	12167·000	4·7958	2·8438
23·1	72·571	419·10	533·61	12326·391	4·8062	2·8479
23·2	72·885	422·73	538·24	12487·168	4·8166	2·8521
23·3	73·199	426·39	542·89	12649·337	4·8270	2·8562
23·4	73·513	430·05	547·56	12812·904	4·8373	2·8603

TABLE 34—Continued.

n	πn ○	$\frac{\pi n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
23·5	73·827	433·74	552·25	12977·875	4·8477	2·8643
23·6	74·142	437·44	556·96	13144·256	4·8580	2·8684
23·7	74·456	441·15	561·69	13312·053	4·8683	2·8724
23·8	74·770	444·88	566·44	13481·272	4·8785	2·8765
23·9	75·084	448·63	571·21	13651·919	4·8888	2·8805
24·0	75·398	452·39	576·00	13824·000	4·8990	2·8845
24·1	75·712	456·17	580·81	13997·521	4·9092	2·8885
24·2	76·027	459·96	585·64	14172·488	4·9192	2·8925
24·3	76·341	463·77	590·49	14348·907	4·9295	2·8965
24·4	76·655	467·60	595·36	14526·784	4·9396	2·9004
24·5	76·969	471·44	600·25	14706·125	4·9497	2·9044
24·6	77·283	475·29	605·16	14886·936	4·9598	2·9083
24·7	77·597	479·16	610·09	15069·223	4·9699	2·9123
24·8	77·911	483·05	615·04	15252·992	4·9799	2·9162
24·9	78·226	486·96	620·01	15438·249	4·9899	2·9201
25·0	78·540	490·87	625·00	15625·000	5·0000	2·9241
25·1	78·854	494·81	630·01	15813·251	5·0099	2·9279
25·2	79·168	498·76	635·04	16003·008	5·0199	2·9318
25·3	79·482	502·73	640·09	16194·277	5·0299	2·9356
25·4	79·796	506·71	645·16	16387·064	5·0398	2·9395
25·5	80·111	510·71	650·25	16581·375	5·0497	2·9434
25·6	80·425	514·72	655·36	16777·216	5·0596	2·9472
25·7	80·739	518·75	660·49	16974·593	5·0695	2·9510
25·8	81·053	522·79	665·64	17173·512	5·0793	2·9549
25·9	81·367	526·85	670·81	17373·979	5·0892	2·9586
26·0	81·681	530·93	676·00	17576·000	5·0990	2·9624
26·1	81·996	535·02	681·21	17779·581	5·1088	2·9662
26·2	82·310	539·13	686·44	17984·728	5·1185	2·9701
26·3	82·624	543·25	691·69	18191·447	5·1283	2·9738
26·4	82·938	547·39	696·96	18399·744	5·1380	2·9776
26·5	83·252	551·55	702·25	18609·625	5·1478	2·9814
26·6	83·566	555·72	707·56	18821·096	5·1575	2·9851
26·7	83·881	559·90	712·89	19034·163	5·1672	2·9888
26·8	84·195	564·10	718·24	19248·832	5·1768	2·9926
26·9	84·509	568·32	723·61	19465·109	5·1865	2·9963
27·0	84·823	572·56	729·00	19683·000	5·1962	3·0000
27·1	85·137	576·80	734·41	19902·511	5·2057	3·0037
27·2	85·451	581·07	739·84	20123·648	5·2153	3·0074

TABLE 34—Continued.

n	πn ○	$\frac{\pi n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
27·3	85·765	585·35	745·29	20346·417	5·2249	3·0111
27·4	86·080	589·65	750·76	20570·824	5·2345	3·0147
27·5	86·394	593·96	756·25	20796·875	5·2440	3·0184
27·6	86·708	598·29	761·76	21024·576	5·2535	3·0221
27·7	87·022	602·63	767·29	21253·933	5·2630	3·0257
27·8	87·336	606·99	772·84	21484·952	5·2725	3·0293
27·9	87·650	611·36	778·41	21717·639	5·2820	3·0330
28·0	87·965	615·75	784·00	21952·000	5·2915	3·0366
28·1	88·279	620·16	789·61	22188·041	5·3009	3·0402
28·2	88·593	624·58	795·24	22425·768	5·3103	3·0438
28·3	88·907	629·02	800·89	22665·187	5·3197	3·0474
28·4	89·221	633·47	806·56	22906·304	5·3291	3·0510
28·5	89·535	637·94	812·25	23149·125	5·3385	3·0546
28·6	89·850	642·42	817·96	23393·656	5·3478	3·0581
28·7	90·164	646·93	823·69	23639·903	5·3572	3·0617
28·8	90·478	651·44	829·44	23887·872	5·3665	3·0652
28·9	90·792	655·97	835·21	24137·569	5·3758	3·0688
29·0	91·106	660·52	841·00	24389·000	5·3852	3·0723
29·1	91·420	665·08	846·81	24642·171	5·3944	3·0758
29·2	91·735	669·66	852·64	24897·088	5·4037	3·0794
29·3	92·049	674·26	858·49	25153·757	5·4129	3·0829
29·4	92·363	678·87	864·36	25412·184	5·4221	3·0864
29·5	92·677	683·49	870·25	25672·375	5·4313	3·0899
29·6	92·991	688·13	876·16	25934·336	5·4405	3·0934
29·7	93·305	692·79	882·09	26198·073	5·4497	3·0968
29·8	93·619	697·47	888·04	26463·592	5·4589	3·1003
29·9	93·934	702·15	894·01	26730·899	5·4680	3·1038
30·0	94·248	706·86	900·00	27000·000	5·4772	3·1072
30·1	94·562	711·58	906·01	27270·901	5·4863	3·1107
30·2	94·876	716·32	912·04	27543·608	5·4954	3·1141
30·3	95·190	721·07	918·09	27818·127	5·5045	3·1176
30·4	95·504	725·83	924·16	28094·464	5·5136	3·1210
30·5	95·819	730·62	930·25	28372·625	5·5226	3·1244
30·6	96·133	735·42	936·36	28652·616	5·5317	3·1278
30·7	96·447	740·23	942·49	28934·443	5·5407	3·1312
30·8	96·761	745·06	948·64	29218·112	5·5497	3·1346
30·9	97·075	749·91	954·81	29503·629	5·5587	3·1380

TABLE 34—Continued.

n	πn ○	$\frac{\pi n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
31·0	97·389	754·77	961·00	29791·000	5·5678	3·1414
31·1	97·704	759·65	967·21	30080·231	5·5767	3·1448
31·2	98·018	764·54	973·44	30371·328	5·5857	3·1481
31·3	98·332	769·45	979·69	30664·297	5·5946	3·1515
31·4	98·646	774·37	985·96	30959·144	5·6035	3·1549
31·5	98·960	779·31	992·25	31255·875	5·6124	3·1582
31·6	99·274	784·27	998·56	31554·496	5·6213	3·1615
31·7	99·588	789·24	1004·89	31855·013	5·6302	3·1648
31·8	99·903	794·23	1011·24	32157·432	5·6391	3·1681
31·9	100·22	799·23	1017·61	32461·759	5·6480	3·1715
32·0	100·53	804·25	1024·00	32768·000	5·6569	3·1748
32·1	100·85	809·28	1030·41	33076·161	5·6656	3·1781
32·2	101·16	814·33	1036·84	33386·248	5·6745	3·1814
32·3	101·47	819·40	1043·29	33698·267	5·6833	3·1847
32·4	101·79	824·49	1049·76	34012·224	5·6921	3·1880
32·5	102·10	829·58	1056·25	34328·125	5·7008	3·1913
32·6	102·42	834·69	1062·76	34645·976	5·7056	3·1945
32·7	102·73	839·82	1069·29	34965·783	5·7183	3·1978
32·8	103·04	844·96	1075·84	35287·552	5·7271	3·2010
32·9	103·36	850·12	1082·41	35611·289	5·7358	3·2043
33·0	103·67	855·30	1089·00	35937·000	5·7447	3·2075
33·1	103·99	860·49	1095·61	36264·691	5·7532	3·2108
33·2	104·30	865·70	1102·24	36594·368	5·7619	3·2140
33·3	104·62	870·92	1108·89	36925·037	5·7706	3·2172
33·4	104·93	876·19	1115·56	37259·704	5·7792	3·2204
33·5	105·24	881·41	1122·25	37595·375	5·7879	3·2237
33·6	105·56	886·68	1128·96	37933·056	5·7965	3·2269
33·7	105·87	891·97	1135·69	38272·753	5·8051	3·2301
33·8	106·19	897·27	1142·44	38614·472	5·8137	3·2332
33·9	106·50	902·59	1149·21	38958·219	5·8223	3·2364
34·0	106·81	907·92	1156·00	39304·000	5·8310	3·2396
34·1	107·13	913·27	1162·81	39651·821	5·8395	3·2424
34·2	107·44	918·63	1169·64	40001·688	5·8480	3·2460
34·3	107·76	924·01	1176·49	40353·607	5·8566	3·2491
34·4	108·07	929·41	1183·36	40707·584	5·8751	3·2522
34·5	108·38	934·82	1190·25	41063·525	5·8736	3·2554
34·6	108·70	940·25	1197·16	41421·736	5·8821	3·2586
34·7	109·01	945·69	1204·09	41781·923	5·8906	3·2617

TABLE 34—Continued.

n	πn ○	$\frac{\pi n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
34·8	109·33	951·15	1211·04	42144·192	5·8991	3·2648
34·9	109·64	956·62	1218·01	42508·549	5·9076	3·2679
35·0	109·96	962·11	1225·00	42875·000	5·9161	3·2710
35·1	110·27	967·62	1232·01	43243·551	5·9245	3·2742
35·2	110·58	973·14	1239·04	43614·208	5·9326	3·2773
35·3	110·90	978·68	1246·09	43986·977	5·9413	3·2804
35·4	111·21	984·23	1253·16	44361·864	5·9497	3·2835
35·5	111·53	989·80	1260·25	44738·875	5·9581	3·2866
35·6	111·84	995·38	1267·36	45118·016	5·9665	3·2897
35·7	112·15	1000·98	1274·49	45499·293	5·9749	3·2927
35·8	112·47	1006·60	1281·64	45882·712	5·9833	3·2958
35·9	112·78	1012·23	1288·81	46268·279	5·9916	3·2989
36·0	113·10	1017·88	1296·00	46656·000	6·0000	3·3019
36·1	113·41	1023·54	1303·21	47045·881	6·0083	3·3050
36·2	113·73	1029·22	1310·44	47437·928	6·0166	3·3080
36·3	114·04	1034·91	1317·69	47832·147	6·0249	3·3111
36·4	114·35	1040·62	1324·96	48228·544	6·0332	3·3141
36·5	114·67	1046·35	1332·25	48627·125	6·0415	3·3171
36·6	114·98	1052·09	1339·56	49017·896	6·0497	3·3202
36·7	115·30	1057·84	1346·89	49430·863	6·0580	3·3232
36·8	115·61	1063·62	1354·24	49836·032	6·0663	3·3262
36·9	115·92	1069·41	1361·61	50243·409	6·0745	3·3292
37·0	116·24	1075·21	1369·00	50653·000	6·0827	3·3322
37·1	116·55	1081·03	1376·41	51064·811	6·0909	3·3352
37·2	116·87	1086·87	1383·84	51478·848	6·0991	3·3382
37·3	117·18	1092·72	1391·29	51895·117	6·1073	3·3412
37·4	117·50	1098·58	1398·76	52313·624	6·1155	3·3442
37·5	117·81	1104·47	1406·25	52734·375	6·1237	3·3472
37·6	118·12	1110·36	1413·76	53157·376	6·1318	3·3501
37·7	118·44	1116·28	1421·29	53582·633	6·1400	3·3531
37·8	118·75	1122·21	1428·84	54010·152	6·1481	3·3561
37·9	119·07	1128·15	1436·41	54439·939	6·1563	3·3590
38·0	119·38	1134·11	1444·00	54872·000	6·1644	3·3620
38·1	119·69	1140·09	1451·61	55306·341	6·1725	3·3649
38·2	120·01	1146·08	1459·24	55742·968	6·1806	3·3679
38·3	120·32	1152·09	1466·89	56181·887	6·1887	3·3708
38·4	120·64	1158·12	1474·56	56623·104	6·1967	3·3737

TABLE 34—Continued.

n	πn ○	$\pi \frac{n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
38·5	120·95	1164·16	1482·25	57066·625	6·2048	3·8767
38·6	121·27	1170·21	1489·96	57512·456	6·2129	3·8797
38·7	121·58	1176·28	1497·69	57960·603	6·2209	3·8825
38·8	121·80	1182·37	1505·44	58411·072	6·2289	3·8854
38·9	122·21	1188·47	1513·21	58863·869	6·2370	3·8883
39·0	122·52	1194·59	1521·00	59319·000	6·2450	3·3912
39·1	122·84	1200·72	1528·81	59776·471	6·2530	3·3941
39·2	123·15	1206·87	1536·64	60236·288	6·2610	3·3970
39·3	123·46	1213·04	1544·49	60698·457	6·2689	3·3999
39·4	123·78	1219·22	1552·36	61162·984	6·2769	3·4028
39·5	124·09	1225·42	1560·25	61629·875	6·2849	3·4056
39·6	124·41	1231·63	1568·16	62099·136	6·2928	3·4085
39·7	124·72	1237·86	1576·09	62570·773	6·3008	3·4114
39·8	125·04	1244·10	1584·04	63044·792	6·3087	3·4142
39·9	125·35	1250·36	1592·01	63521·199	6·3166	3·4171
40·0	125·66	1264·64	1600·00	64000·000	6·3245	3·4200
40·1	125·98	1293·93	1608·01	64481·201	6·3325	3·4228
40·2	126·29	1228·23	1616·04	64964·808	6·3404	3·4256
40·3	126·61	1256·56	1624·09	65450·827	6·3482	3·4285
40·4	126·92	1297·90	1632·16	65939·264	6·3561	3·4313
40·5	127·23	1288·25	1640·25	66430·126	6·3639	3·4341
40·6	127·55	1294·62	1648·36	66923·416	6·3718	3·4370
40·7	127·86	1301·00	1656·49	67419·143	6·3796	3·4398
40·8	128·18	1307·41	1664·64	67917·312	6·3875	3·4426
40·9	128·49	1313·82	1672·81	68417·929	6·3953	3·4454
41·0	128·81	1320·25	1681·00	68921·000	6·4031	3·4482
41·1	129·12	1326·70	1689·21	69426·531	6·4109	3·4510
41·2	129·43	1333·17	1697·44	69934·528	6·4187	3·4538
41·3	129·75	1339·65	1705·69	70444·997	6·4265	3·4566
41·4	130·06	1346·14	1713·96	70957·944	6·4343	3·4594
41·5	130·38	1352·65	1722·25	71473·375	6·4421	3·4622
41·6	130·69	1359·18	1730·56	71991·296	6·4498	3·4650
41·7	131·00	1365·72	1738·89	72511·719	6·4575	3·4677
41·8	131·32	1372·28	1747·24	73034·632	6·4653	3·4705
41·9	131·63	1378·85	1755·61	73560·059	6·4730	3·4733
42·0	131·95	1385·44	1764·00	74088·000	6·4807	3·4760
42·1	132·26	1392·05	1772·41	74618·461	6·4884	3·4788
42·2	132·58	1398·67	1780·84	75151·448	6·4961	3·4815

TABLE 34—Continued.

n	πn ○	$\frac{\pi n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
42·3	132·89	1405·31	1789·29	75686·967	6·5088	3·4843
42·4	133·20	1411·96	1797·76	76225·024	6·5115	3·4870
42·5	133·52	1418·63	1806·25	76765·625	6·5192	3·4898
42·6	133·83	1425·31	1814·76	77308·776	6·5268	3·4925
42·7	134·15	1432·01	1823·29	77854·483	6·5345	3·4952
42·8	134·46	1438·72	1831·84	78402·752	6·5422	3·4980
42·9	134·77	1445·45	1840·41	78953·589	6·5498	3·5007
43·0	135·09	1452·20	1849·00	79507·000	6·5574	3·5034
43·1	135·40	1458·96	1857·61	80062·991	6·5651	3·5061
43·2	135·72	1465·74	1866·24	80621·568	6·5727	3·5088
43·3	136·03	1472·54	1874·89	81182·737	6·5803	3·5115
43·4	136·35	1479·34	1883·56	81746·504	6·5879	3·5142
43·5	136·66	1486·17	1892·25	82312·875	6·5954	3·5169
43·6	136·97	1493·01	1900·96	82881·856	6·6030	3·5196
43·7	137·29	1499·87	1909·69	83453·453	6·6106	3·5223
43·8	137·60	1506·74	1918·44	84027·672	6·6182	3·5250
43·9	137·92	1513·63	1927·21	84604·519	6·6257	3·5277
44·0	138·23	1520·53	1936·00	85184·000	6·6333	3·5303
44·1	138·54	1527·45	1944·81	85766·121	6·6408	3·5330
44·2	138·86	1534·39	1953·64	86350·888	6·6483	3·5357
44·3	139·17	1541·34	1962·49	86938·307	6·6558	3·5384
44·4	139·49	1548·30	1971·36	87528·384	6·6633	3·5410
44·5	139·80	1555·28	1980·25	88121·125	6·6708	3·5437
44·6	140·12	1562·28	1989·16	88716·536	6·6783	3·5463
44·7	140·43	1569·30	1998·09	89314·623	6·6858	3·5490
44·8	140·74	1576·33	2007·04	89915·392	6·6933	3·5516
44·9	141·06	1583·37	2016·01	90518·849	6·7007	3·5543
45·0	141·37	1590·43	2025·00	91125·000	6·7082	3·5569
45·1	141·69	1597·51	2034·01	91733·851	6·7156	3·5595
45·2	142·00	1604·60	2043·04	92345·408	6·7231	3·5621
45·3	142·31	1611·71	2052·09	92959·677	6·7305	3·5648
45·4	142·63	1618·83	2061·16	93576·664	6·7379	3·5674
45·5	142·94	1625·97	2070·25	94196·375	6·7454	3·5700
45·6	143·26	1633·13	2079·36	94818·816	6·7528	3·5726
45·7	143·57	1640·30	2088·49	95443·993	6·7602	3·5752
45·8	143·88	1647·48	2097·64	96071·912	6·7676	3·5778
45·9	144·20	1654·68	2106·81	96702·579	6·7749	3·5805

TABLE 34—Continued.

n	πn ○	$\frac{\pi^2 n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
46·0	144·51	1661·90	2116·00	97336·000	6·7823	3·5830
46·1	144·83	1669·14	2125·21	97972·181	6·7897	3·5856
46·2	145·14	1676·39	2134·44	98611·128	6·7971	3·5882
46·3	145·46	1683·65	2143·69	99252·847	6·8044	3·5908
46·4	145·77	1690·93	2152·96	99897·344	6·8117	3·5934
46·5	146·08	1698·23	2162·25	100544·625	6·8191	3·5960
46·6	146·40	1705·54	2171·56	101194·696	6·8264	3·5986
46·7	146·71	1712·87	2180·89	101847·563	6·8337	3·6011
46·8	147·03	1720·21	2190·24	102503·232	6·8410	3·6037
46·9	147·34	1727·57	2199·61	103161·709	6·8484	3·6063
47·0	147·65	1734·94	2209·00	103823·000	6·8556	3·6088
47·1	147·97	1742·34	2218·41	104487·111	6·8629	3·6114
47·2	148·28	1749·74	2227·84	105154·048	6·8702	3·6139
47·3	148·60	1757·16	2237·29	105823·817	6·8775	3·6165
47·4	148·91	1764·60	2246·76	106496·424	6·8847	3·6190
47·5	149·23	1772·05	2256·25	107171·875	6·8920	3·6216
47·6	149·54	1779·52	2265·76	107850·176	6·8993	3·6241
47·7	149·85	1787·01	2275·29	108531·333	6·9065	3·6267
47·8	150·17	1794·51	2284·84	109215·352	6·9137	3·6292
47·9	150·48	1802·03	2294·41	109902·239	6·9209	3·6317
48·0	150·80	1809·56	2304·00	110592·000	6·9282	3·6342
48·1	151·11	1817·11	2313·61	111284·641	6·9354	3·6368
48·2	151·42	1824·67	2323·24	111980·168	6·9426	3·6393
48·3	151·74	1832·25	2332·89	112678·587	6·9498	3·6418
48·4	152·05	1839·84	2342·56	113379·904	6·9570	3·6443
48·5	152·37	1847·45	2352·25	114084·125	6·9642	3·6468
48·6	152·68	1855·08	2361·96	114791·256	6·9714	3·6493
48·7	153·00	1862·72	2371·69	115501·303	6·9785	3·6518
48·8	153·31	1870·38	2381·44	116214·272	6·9857	3·6543
48·9	153·62	1878·05	2391·21	116930·169	6·9928	3·6568
49·0	153·94	1885·74	2401·00	117649·000	7·0000	3·6593
49·1	154·25	1893·45	2410·81	118370·771	7·0071	3·6618
49·2	154·57	1901·17	2420·64	119095·488	7·0143	3·6643
49·3	154·88	1908·90	2430·49	119823·157	7·0214	3·6668
49·4	155·19	1916·65	2440·36	120553·784	7·0285	3·6692
49·5	155·51	1924·42	2450·25	121287·375	7·0356	3·6717
49·6	155·82	1932·21	2460·16	122023·936	7·0427	3·6742
49·7	156·14	1940·00	2470·09	122763·473	7·0498	3·6767

TABLE 34—Continued.

n	πn ○	$\frac{\pi n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
49·8	156·45	1947·82	2480·04	123505·992	7·0569	3·6791
49·9	156·77	1955·65	2490·01	124251·499	7·0640	3·6816
50·0	157·08	1968·50	2500·00	125000·000	7·0711	3·6840
51·0	160·22	2042·82	2601·00	132651·000	7·1414	3·7084
52·0	163·36	2123·72	2704·00	140608·000	7·2111	3·7325
53·0	166·50	2206·19	2809·00	148877·000	7·2801	3·7563
54·0	169·64	2290·22	2916·00	157464·000	7·3485	3·7798
55·0	172·78	2375·83	3025·00	166375·000	7·4162	3·8030
56·0	175·93	2463·01	3136·00	175616·000	7·4833	3·8259
57·0	179·07	2551·76	3249·00	185193·000	7·5498	3·8485
58·0	182·21	2642·08	3364·00	195112·000	7·6158	3·8709
59·0	185·35	2733·97	3481·00	205379·000	7·6811	3·8930
60·0	188·49	2827·44	3600·00	216000·000	7·7460	3·9149
61·0	191·63	2922·47	3721·00	226981·000	7·8102	3·9365
62·0	194·77	3019·07	3844·00	238328·000	7·8740	3·9579
63·0	197·92	3117·25	3969·00	250047·000	7·9373	3·9791
64·0	201·06	3216·99	4096·00	262144·000	8·0000	4·0000
65·0	204·20	3318·31	4225·00	274625·000	8·0623	4·0207
66·0	207·34	3421·20	4356·00	287496·000	8·1240	4·0412
67·0	210·48	3525·66	4489·00	300763·000	8·1854	4·0615
68·0	213·63	3631·69	4624·00	314432·000	8·2462	4·0817
69·0	216·77	3739·29	4761·00	328509·000	8·3066	4·1016
70·0	219·91	3848·46	4900·00	343000·000	8·3666	4·1213
71·0	223·05	3959·20	5041·00	357911·000	8·4261	4·1408
72·0	226·19	4071·51	5184·00	373248·000	8·4853	4·1602
73·0	229·33	4185·39	5329·00	389017·000	8·5440	4·1793
74·0	232·47	4300·85	5476·00	405224·000	8·6023	4·1983
75·0	235·62	4417·87	5625·00	421875·000	8·6603	4·2172
76·0	238·76	4536·47	5776·00	438976·000	8·7178	4·2358
77·0	241·90	4656·63	5929·00	456533·000	8·7750	4·2543
78·0	245·04	4778·37	6084·00	474552·000	8·8318	4·2727
79·0	248·18	4901·68	6241·00	493039·000	8·8882	4·2908
80·0	251·32	5026·56	6400·00	512000·000	8·9443	4·3089
81·0	254·47	5153·01	6561·00	531441·000	9·0000	4·3267
82·0	257·61	5281·03	6724·00	551368·000	9·0554	4·3445
83·0	260·75	5410·62	6889·00	571787·000	9·1104	4·3621
84·0	263·89	5541·78	7056·00	592704·000	9·1652	4·3795

TABLE 34—Continued.

n	πn ○	$\frac{\pi n^2}{4}$ ●	n^2	n^3	\sqrt{n}	$\sqrt[3]{n}$
85·0	267·03	5674·50	7225·00	614125·000	9·2195	4·3968
86·0	270·17	5808·81	7396·00	636056·000	9·2786	4·4140
87·0	273·32	5944·69	7569·00	658503·000	9·3274	4·4310
88·0	276·46	6082·18	7744·00	681472·000	9·3808	4·4480
89·0	279·60	6221·18	7921·00	704969·000	9·4330	4·4647
90·0	282·74	6361·74	8100·00	729000·000	9·4868	4·4814
91·0	285·88	6503·89	8281·00	753571·000	9·5394	4·4979
92·0	289·02	6647·62	8464·00	778688·000	9·5917	4·5144
93·0	292·17	6792·92	8649·00	804357·000	9·6437	4·5307
94·0	295·31	6939·78	8836·00	830584·000	9·6954	4·5468
95·0	298·45	7088·23	9025·00	857375·000	9·7468	4·5629
96·0	301·59	7238·24	9216·00	884736·000	9·7980	4·5789
97·0	304·73	7389·83	9409·00	912673·000	9·8489	4·5947
98·0	307·87	7542·98	9604·00	941192·000	9·8995	4·6104
99·0	311·02	7697·68	9801·00	970299·000	9·9499	4·6261
100·0	314·16	7854·00	100000·00	1000000·000	10·0000	4·6416

Approximately $\sqrt{a^2 \pm b} = a \pm \frac{b}{2a}$ and $\sqrt[3]{a^3 \pm b} = a \pm \frac{b}{3a^2}$

TABLE 35.—FORMULÆ FOR MENSURATION OF AREAS AND SOLID CONTENTS.

1.—Triangle.

$$\text{Area} = \frac{1}{2} \times \text{base} \times \text{height.}$$

If all the sides, a, b, c , are known and half their sum is represented by s , so that $s = \frac{a+b+c}{2}$ then

$$A = \sqrt{s(s-a)(s-b)(s-c)}$$

2.—Circle.

Area of circle, if d =diameter, r =radius, and $\pi=3\cdot14159$

$$A = \frac{\pi}{4}d^2 = r^2\pi \dots \left(\frac{\pi}{4} = 0\cdot7854\right)$$

$$d = 1\cdot12838\sqrt{A}$$

Area of segment of circle of an arc of α°

$$A = \left(\frac{\alpha}{180} \pi - \sin \alpha \right) \frac{r^2}{2}$$

Or, if d is the diameter and h the height of segment, calculate $\frac{h}{d}$ and find the value x , in the following table, corresponding to $\frac{h}{d}$; the square of the diameter multiplied by x , gives the area of the segment.

$$\text{Area of segment} = xd^2.$$

$\frac{h}{d}$	x	$\frac{h}{d}$	x	$\frac{h}{d}$	x	$\frac{h}{d}$	x
·01	·00133	·14	·06683	·27	·17109	·40	·29337
·02	·00375	·15	·07387	·28	·18002	·41	·30319
·03	·00687	·16	·08111	·29	·18905	·42	·31304
·04	·01054	·17	·08854	·30	·19817	·43	·32293
·05	·01468	·18	·09613	·31	·20737	·44	·33284
·06	·01924	·19	·10390	·32	·21667	·45	·34278
·07	·02417	·20	·11182	·33	·22603	·46	·35274
·08	·02944	·21	·11990	·34	·23547	·47	·36272
·09	·03501	·22	·12811	·35	·24498	·48	·37270
·10	·04087	·23	·13646	·36	·25455	·49	·38270
·11	·04701	·24	·14495	·37	·26418	·50	·39270
·12	·05338	·25	·15355	·38	·27386		
·13	·06000	·26	·16226	·39	·28359		

3.—Cone and Pyramid.

Solid content: $S = \frac{1}{3}$ base \times height.

Area of convex surface of right cone: When s = side of cone = $\sqrt{r^2 + h^2}$, where r = radius of base and h = height of cone, the area of convex surface will be

$$A = \pi rs.$$

4.—Cylinder.

Area of convex surface $A = 2\pi rh$.
Content of cylinder $S = \text{base} \times \text{height}$.

5.—Sphere.

Convex surface $A = 4\pi r^2$.
Surface of segment $A = 2\pi rh$, h = height of segment.
Solid content of sphere $S = \frac{4}{3}r^3\pi = 4\cdot1888r^3$.

Solid content of sphere $S = \frac{1}{6}\pi d^3 = 0.5236d^3$.

Radius $r = 0.62035 \sqrt[3]{\text{content}}$.

Content of segment of sphere: If a is the radius of the sectional area, h the height of the segment, and r the radius of the sphere,

$$S = \frac{1}{6}\pi h(3a^2 + h^2)$$

$$= \frac{1}{3}\pi h^2(3r - h).$$

Solid content of spherical zone: If a and b are the respective radii of the two terminal surfaces, and h the height,

$$S = \frac{1}{6}\pi h(3a^2 + 3b^2 + h^2).$$

TABLE 36.—WEIGHTS AND MEASURES OF DIFFERENT COUNTRIES.

1. **Metric System** (compulsory in France, Germany, Austria, the Netherlands, Belgium, Luxemburg, Switzerland, Italy, Greece, Turkey, Roumania, Spain, Portugal, and most of the South American Republics; optional in Great Britain, the United States, and Russia).
 - 1 metre (m.) = 443.296 Paris lignes = 3.280899 English feet = 3.18620 Prussian feet = 1.00000301 metre des archives.
 - 1 kilometre (km.) = 10 hectometres (hm.) = 0.6214 English mile = 0.1328 Prussian mile = 0.9875 Russian verst = 0.5390 nautical mile = 0.1347 geographical mile (15 to 1 degree of longitude).
 - 1 lieue (France) = 1 myriametre = 10 km.
 - 1 German mile = $7\frac{1}{2}$ km. = 0.996 Prussian mile = 4.66 English miles.
 - 1 hectare (ha.) = 100 ares (a.) = 10,000 sq. m. = 0.01 sq. km. = 2.471 English acres.
 - 1 litre (l.) = 0.001 cb. m. = 1000 c. cm. = 0.2201 gallon.
 - 1 hectolitre (hl.) = 0.1 cb. m. = 100 l. = 22.01 gallons.
 - 1 kilogram (kg.) = 1000 g. = weight of 1 litre of water at +4° C. = 2 German and Swiss pounds (zollpfund) = 0.999999842 kilogram prototype = 2.2046 pounds avoirdupois = 1.7857 Austrian pounds = 2.3511 Swedish pounds = 2.4419 Russian pounds.
 - 1 gram (g.) = 15.432 grains (English).
 - 1 quintal = 100 kg. = 196.84 lbs. avoirdupois = 1 cwt. 3 qr. 0.84 lb.
 - 1 metrical ton = 1000 kg. = 0.9842 English ton = 1.023 American short tons (at 2000 lbs.).

TABLE 36—*Continued.***2. Great Britain and Ireland.**

1 foot = 0·3047943 m.
 1 inch = 25·3995 mm.
 1 yard = 0·9143835 m.
 1 fathom = 2 yards.
 1 rod (pole, perch) = $5\frac{1}{2}$ yards = 5·029109 m.
 1 statute mile = 8 furlongs = 320 poles = 1760 yards = 5280 feet
 = 1·6093 kilometre (km.).
 1 nautical mile = $\frac{1}{60}$ th degree (at the equator).
 6082·66 feet = 1854·96 m.
 1 acre = 4 roods = 160 poles = 0·40467 ha. = 48,560 square feet = 4047
 square metres.
 1 square mile = 640 acres = 259·0 ha.
 1 gallon = 4 quarts = 8 pints = 277·274 cubic inches = 4·536 litres.
 1 cubic foot = 28·3153 l.
 1 cubic inch = 16·3862 c.cm.
 1 quarter = 8 bushels = 32 pecks = 64 gallons = 2·908 hl.
 1 bushel = 8 gallons = 0·3628 hl.
 1 fluid ounce = $\frac{1}{16}$ th pint = 28·35 c.cm.
 1 pound avoirdupois (lb.) = 16 ounces (oz.) = 7000 grains = 0·4535926
 kg.
 1 ounce avoirdupois = 437½ grains = 28·35 g.
 1 gallon = 10 lbs. water = 70,000 grains = 4·535926 kg. water.
 1 hundredweight (cwt.) = 4 quarters (qr.) = 8 stones = 112 lbs.
 = 50·8024 kg.
 1 ton = 20 cwt. = 2240 lbs. = 1016·648 kg.

Apothecaries' Weight.

1 pound troy = 12 ounces troy = 96 drams = 288 scruples = 5760
 grains = 373·24195 g.
 1 ounce troy = 8 drams = 24 scruples = 480 grains = 31·1035 g.
 1 ounce troy (for gold and precious stones) = 20 pennyweight
 (dwt.) = 480 grains = 31·1035 g.
 1 grain (common to avoirdupois and troy weight) = 0·06479895 g.

3. Austria (old measures and weights, now abolished for the metric system).

1 foot = 0·316102 m., at 12 inches of 12 lines each.
 3 ruthen = 5 klafter = 30 feet = 360 zoll.
 1 meile = 4000 klafter = 7586·455 m.
 1 maass = 1·415 l.
 1 eimer = 40 maass = 160 seidel.
 1 metze = 61·4995 l.
 1 Wiener pfund = 560·012 g.
 1 centner = 5 stein = 100 pfund = 3200 loth.

4. Denmark and Norway employ, as unit of measure, the Prussian foot, as unit of weight the units of the metrical system, viz., kilos, etc.

TABLE 36—Continued.

5. Prussia (old system, now abolished for the metric system).

- 1 foot (Rhenish foot) = 12 zoll (inches) = 144 linien = 0·313853 m.
 1 ruthe = 12 fuss = 3·76624 m.
 1 lachter (fathom) = 80 zoll = 2·09326 m.
 1 meile = 24,000 fuss = 7532·5 m.
 1 morgen = 180 square ruthen = 0·2553 ha.
 1 quart = 64 cubic inches = $\frac{1}{3}$ cubic foot = 1·14503 l.
 1 scheffel = 16 Metzen = 48 quarts = 0·54961 hl.
 1 tonne = 4 scheffel = 2·19846 hl.
 1 klafter = 108 cubic fuss = 3·3389 cb.m.
 1 schachtruthe = 144 cubic fuss = 4·4519 cb.m.
 1 pfund = 30 loth = 300 quentchen = 500 g.
 1 centner = 100 pfund = 50 kg. (Formerly 1 pfund = 32 loth = 467·711 g.; 1 centner = 110 pfund.)

6. Russia.

- 1 foot = 1 English foot.
 1 sashehn = 7 feet = 3 arshin = 12 tchetvert = 48 vershok = 2·13357 m.
 1 verst = 500 sashehn = 1066·78 m.
 1 dessatine = 2400 square sashehns = 10925 m.
 1 vedro = 10 krushky (stoof) = 12·299 l.
 1 tchetvert = 1 osmini = 4 payok = 8 tchetverik = 209·9 l.
 1 pound = 32 loth = 96 solotnik = 9216 doli = 0·9028 Eng. lb. = 409·531 g.
 1 berkovets = 10 pud = 400 pounds = 163·81 kg.
 1 pud = 40 pounds = 36·112 Eng. lb. = 16·3805 kg.

7. Sweden.

- 1 foot = 10 zoll (inches) = 100 lines = 0·97408 Eng. foot = 0·296901 m.
 1 famn (fathom) = 3 alnar (ells) = 6 feet = 5·58445 Eng. feet = 1·7814 m.
 1 mile = 6000 fathoms = 6·6417 Eng. statute miles = 10·6884 km.
 1 kanne = 100 cubic inches = 0·57694 Eng. gallon = 2·617 l.
 1 skalpund = 100 korn (at 100 art) = 0·9378 Eng. lb. = 425·3395 g.
 1 centner = 100 skalpund.
 1 skipspund = 20 liespund = 400 skalpund.

8. Switzerland. Metrical measure and weight. The following are sometimes still employed :—

- 1 fuss = 0·3000 m. = 0·9843 Eng. foot.
 1 juchart = 36 are = 0·88956 Eng. acre.
 1 maass = 1·51 l.
 1 saum = 100 maass = 151 l.

9. United States. Weights and measures as in Great Britain, but instead of the "long ton" (gross ton) of 2240 lb., more frequently the "short ton" (net ton) of 2000 lbs. = 907·1852 kg. = 0·89285 long ton, is employed.

TABLE 36—Continued.

Square Feet, Square Metre.

1 square metre (sq.m.)=10·764 square feet (English and Russian)
 =10·008 square feet (Austrian)=10·152 square feet (Prussian
 and Danish)=11·344 square feet (Swedish).

1 square foot (English and Russian)=0·09290 square metre.

Cubic Feet, Cubic Metre.

1 cubic metre (cb.m.)=35·316 cubic feet (English and Russian).
 1 " " =31·66 " (Austrian).
 1 " " =32·346 " (Prussian and Danish).
 1 " " =38·209 " (Swedish).
 1 cubic foot (English and Russian)=0·028315 cubic metre.

1 Kilogram per Running Metre

=0·6719 English pound per running foot.

=0·6277 zollpfund per Prussian foot.

1 Kilogram per Square Centimetre (for steam pressure)

=14·223 English pounds per square inch.

=13·681 zollpfund per Prussian square inch.

=13·878 zollpfund per Austrian square inch.

HORSE-POWER (per second).

Kg.-m.	Austria. Foot-pounds.	Prussia. Foot-pounds.	England. Foot-pounds.	Sweden. Foot-pounds.	Russia. Foot-pounds.
75	474·53	477·93	542·47	593·90	600·85
76·041	481·11	484·56	550	602·14	609·19

75 kilogram-metres taken as unit,
 550 English foot-pounds taken as unit,
 =1 Admiralty horse-power per second;
 or, 33,000 foot-pounds per minute.

TABLE 37.—TABLES FOR REDUCING ENGLISH TO METRICAL WEIGHTS AND MEASURES, AND VICE VERSA.

Reduction of Metrical Measure to English Measure.

Metre. Sq.m. Cub.m.	Feet.	Inches.	Square feet.	Square inches.	Cubic feet.	Cubic inches.
1	3·2809	39·3706	10·7642	1550·05	35·3161	61026·2
2	6·5618	78·7412	21·5284	3100·09	70·6322	122052·4
3	9·8427	118·1118	32·2926	4650·13	105·9488	183078·6
4	13·1235	157·4824	43·0568	6200·18	141·2644	244104·9
5	16·4044	196·8530	53·8210	7750·23	176·5805	305131·1
6	19·6853	236·2237	64·5852	9300·27	211·8966	366157·3
7	22·9662	275·5943	75·3494	10850·31	247·2126	427183·5
8	26·2471	314·9649	86·1136	12400·36	282·5287	488209·7
9	29·5280	354·3355	96·8778	13950·40	317·8448	549235·9

English Feet = Metres.

Ft.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	0·0000	0·3048	0·6096	0·9144	1·2192	1·5240	1·8288	2·1336	2·4384	2·7432
10	3·0479	3·3527	3·6575	3·9623	4·2671	4·5719	4·8767	5·1815	5·4863	5·7911
20	6·0959	6·4007	6·7055	7·0103	7·3151	7·6199	7·9247	8·2295	8·5343	8·8390
30	9·1438	9·4486	9·7534	10·0582	10·3630	10·6678	10·9726	11·2774	11·5822	11·8870
40	12·1917	12·497	12·801	13·106	13·411	13·716	14·021	14·325	14·630	14·935
50	15·240	15·545	15·849	16·154	16·459	16·764	17·068	17·373	17·678	17·983
60	18·288	18·592	18·897	19·202	19·507	19·812	20·116	20·421	20·726	21·031
70	21·336	21·640	21·945	22·250	22·555	22·860	23·164	23·469	23·774	24·079
80	24·384	24·688	24·993	25·298	25·603	25·908	26·212	26·517	26·822	27·127
90	27·432	27·736	28·041	28·346	28·651	28·955	29·260	29·565	29·870	30·175
100	30·479	30·784	31·089	31·394	31·699	32·003	32·308	32·613	32·918	33·223
110	33·527	33·832	34·137	34·442	34·747	35·051	35·356	35·661	35·966	36·271
120	36·575	36·880	37·185	37·490	37·795	38·099	38·404	38·709	39·014	39·318
130	39·623	39·928	40·233	40·538	40·843	41·147	41·452	41·757	42·062	42·366
140	42·671	42·976	43·281	43·586	43·890	44·195	44·500	44·805	45·110	45·414
150	45·719	46·024	46·329	46·634	46·938	47·243	47·548	47·853	48·158	48·462
160	48·767	49·072	49·377	49·682	49·986	50·291	50·596	50·901	51·206	51·510
170	51·815	52·120	52·425	52·729	53·034	53·339	53·644	53·948	54·253	54·558
180	54·863	55·168	55·473	55·777	56·082	56·387	56·692	56·997	57·301	57·606
190	57·911	58·216	58·521	58·825	59·130	59·435	59·740	60·045	60·349	60·654

English Inches = Millimetres.

Inch.	Millimetres.	Inches.	Millimetres.	Inches.	Millimetres.
$\frac{1}{16}$	0·39	1	25·4	7	177·8
$\frac{1}{8}$	0·79	2	50·8	8	203·2
$\frac{1}{4}$	1·59	3	76·2	9	228·6
$\frac{3}{8}$	3·17	4	101·6	10	254·0
$\frac{1}{2}$	6·35	5	127·0	11	279·4
$\frac{3}{4}$	12·70	6	152·4	12	304·8

English Square Feet = Square Metres.

Sq. ft.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	0·0000	0·0929	0·1858	0·2787	0·3716	0·4645	0·5574	0·6503	0·7432	0·8361
10	0·9290	1·0219	1·1148	1·2077	1·3006	1·3935	1·4864	1·5793	1·6722	1·7651
20	1·8580	1·9509	2·0438	2·1367	2·2296	2·3225	2·4154	2·5083	2·6012	2·6941
30	2·7870	2·8799	2·9728	3·0657	3·1586	3·2515	3·3444	3·4373	3·5302	3·6231
40	3·7160	3·8089	3·9018	3·9947	4·0876	4·1805	4·2734	4·3663	4·4592	4·5521
50	4·6450	4·7379	4·8308	4·9237	5·0166	5·1095	5·2024	5·2953	5·3882	5·4811
60	5·5740	5·6669	5·7598	5·8527	5·9456	6·0385	6·1314	6·2243	6·3172	6·4101
70	6·5030	6·5959	6·6888	6·7817	6·8746	6·9675	7·0604	7·1533	7·2462	7·3391
80	7·4320	7·5249	7·6178	7·7107	7·8036	7·8965	7·9894	8·0823	8·1752	8·2681
90	8·3610	8·4539	8·5468	8·6397	8·7326	8·8255	8·9184	9·0113	9·1042	9·1971

English Square Inches = Square Centimetres.

Sq. ins	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	0·0000	6·4514	12·9028	19·3542	25·8056	32·2570	38·7084	45·1598	51·6112	58·0626
10	64·514	70·9654	77·4168	83·8682	90·3196	96·7710	103·2224	109·6738	116·1252	122·5766
20	129·028	135·48	141·9316	148·3832	154·8348	161·2864	167·7380	174·1896	180·6412	187·0928
30	193·542	199·9936	206·4452	212·8968	219·3484	225·8000	232·2516	238·7032	245·1548	251·6064
40	258·056	264·5076	270·9592	277·4108	283·8624	290·3140	296·7656	303·2172	309·6688	316·1204
50	322·570	329·0216	335·4732	341·9248	348·3764	354·8280	361·2796	367·7312	374·1828	380·6344
60	387·084	393·5356	399·9872	406·4388	412·8904	419·3420	425·7936	432·2452	438·6968	445·1484
70	451·598	458·0496	464·5012	470·9528	477·4044	483·8560	490·3076	496·7592	503·2108	509·6624
80	516·112	522·5636	529·0152	535·4668	541·9184	548·3700	554·8216	561·2732	567·7248	574·1764
90	580·626	587·0776	593·5292	599·9808	606·4324	612·8840	619·3356	625·7872	632·2388	638·6904

English Cubic Feet = Cubic Metres.

Cub. ft.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	0·0000	0·0283	0·0566	0·0849	0·1133	0·1416	0·1699	0·1982	0·2265	0·2548
10	0·2832	0·3115	0·3398	0·3681	0·3964	0·4247	0·4530	0·4814	0·5097	0·5380
20	0·5663	0·5946	0·6229	0·6513	0·6796	0·7079	0·7362	0·7645	0·7928	0·8211
30	0·8494	0·8777	0·9061	0·9344	0·9627	0·9910	1·0194	1·0477	1·0760	1·1043
40	1·1326	1·1609	1·1892	1·2176	1·2459	1·2742	1·3025	1·3308	1·3591	1·3874
50	1·4158	1·4441	1·4724	1·5007	1·5290	1·5573	1·5857	1·6140	1·6423	1·6706
60	1·6989	1·7272	1·7555	1·7839	1·8122	1·8405	1·8688	1·8971	1·9254	1·9538
70	1·9821	2·0104	2·0387	2·0670	2·0953	2·1236	2·1520	2·1803	2·2086	2·2369
80	2·2652	2·2935	2·3219	2·3502	2·3785	2·4068	2·4351	2·4634	2·4917	2·5201
90	2·5484	2·5767	2·6050	2·6333	2·6616	2·6900	2·7183	2·7466	2·7749	2·8032

English Cubic Inches = Cubic Centimetres.

Cub. in.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	0·0000	16·886	32·772	49·159	65·545	81·931	98·317	114·70	131·09	147·48
10	168·86	180·25	196·63	213·02	229·41	245·79	262·18	278·56	294·95	311·34
20	327·72	344·11	360·50	376·88	393·27	409·65	426·04	442·43	458·81	475·20
30	491·59	507·97	524·36	540·74	557·13	573·52	589·90	606·29	622·67	639·06
40	655·45	671·83	688·22	704·61	720·99	737·38	753·76	770·15	786·54	802·92
50	819·81	835·69	852·08	868·47	884·85	901·24	917·63	934·01	950·40	966·78
60	988·17	999·56	1015·9	1032·3	1048·7	1065·1	1081·5	1097·9	1114·8	1130·6
70	1147·0	1168·4	1179·8	1196·2	1212·6	1229·0	1245·8	1261·7	1278·1	1294·5
80	1310·9	1327·8	1343·7	1360·1	1376·4	1392·8	1409·2	1425·6	1440·9	1458·4
90	1474·8	1491·1	1507·5	1523·9	1540·3	1556·7	1573·1	1589·5	1605·8	1622·2

English Pounds = Kilograms.

Lbs.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	0·0000	0·4536	0·9072	1·3608	1·8144	2·2680	2·7216	3·1751	3·6287	4·0823
10	4·5359	4·9895	5·4431	5·8967	6·3503	6·8039	7·2575	7·7111	8·1647	8·6183
20	9·0719	9·5254	9·9790	10·4326	10·8862	11·3400	11·7935	12·2471	12·7007	13·1543
30	13·6083	14·0619	14·5155	14·9691	15·4227	15·8763	16·3299	16·7835	17·2371	17·6907
40	18·1444	18·5979	19·0515	19·5051	19·9587	20·4123	20·8659	21·3195	21·7731	22·2267
50	22·6800	23·1336	23·5872	24·0408	24·4944	24·9480	25·4016	25·8552	26·3088	26·7624
60	27·2160	27·6696	28·1232	28·5768	29·0304	29·4840	29·9376	30·3912	30·8448	31·2984
70	31·7519	32·2055	32·6591	33·1127	33·5663	34·0199	34·4735	34·9271	35·3807	35·8343
80	36·2878	36·7414	37·1950	37·6486	38·1022	38·5558	39·0094	39·4630	39·9166	40·3702
90	40·8238	41·2774	41·7310	42·1846	42·6382	43·0918	43·5454	43·9990	44·4526	44·9062

English Tons = Kilograms.

Tons.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	0·0000	1016	2032	3048	4064	5080	6096	7112	8129	9145
10	10161	11177	12193	13209	14225	15241	16257	17273	18289	19305
20	20321	21337	22353	23369	24386	25402	26418	27434	28450	29466
30	30482	31498	32514	33530	34546	35562	36578	37594	38610	39627
40	40644	41659	42675	43691	44707	45723	46739	47755	48771	49787
50	50808	51819	52835	53851	54868	55884	56900	57916	58932	59948
60	60964	61980	62996	64012	65028	66044	67060	68076	69092	70108
70	71125	72141	73157	74173	75189	76205	77221	78237	79253	80269
80	81285	82302	83317	84333	85346	86366	87382	88398	89414	90430
90	91446	92464	93478	94494	95510	96526	97542	98558	99574	100590

English Grains = Grams.

Grains.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
—	0	·065	·1296	·194	·259	·324	·389	·454	·518	·583
10	·648	·713	·778	·842	·907	·972	1·037	1·102	1·166	1·231
20	1·296	1·361	1·426	1·490	1·555	1·620	1·685	1·749	1·814	1·879
30	1·944	2·009	2·074	2·138	2·203	2·268	2·333	2·397	2·462	2·527
40	2·592	2·657	2·721	2·786	2·851	2·916	2·981	3·045	3·110	3·175
50	3·240	3·305	3·369	3·434	3·499	3·564	3·629	3·693	3·758	3·823
60	3·888	3·953	4·018	4·082	4·147	4·212	4·277	4·341	4·406	4·471
70	4·586	4·651	4·716	4·780	4·845	4·910	4·975	5·039	5·104	5·169
80	5·184	5·249	5·314	5·378	5·443	5·508	5·573	5·637	5·702	5·767
90	5·822	5·887	5·952	6·016	6·081	6·146	6·211	6·276	6·340	6·405

Grams = English Grains.

Grams.	0.	·1.	·2.	·3.	·4.	·5.	·6.	·7.	·8.	·9.
0	0	1·543	3·086	4·629	6·172	7·716	9·259	10·802	12·345	13·888
1	15·432	16·975	18·518	20·061	21·604	23·148	24·691	26·234	27·777	29·320
2	30·864	32·407	33·950	35·493	37·036	38·580	40·123	41·666	43·209	44·752
3	46·296	47·839	49·382	50·925	52·468	54·012	55·555	57·098	58·641	60·184
4	61·728	63·271	64·814	66·357	67·900	69·444	70·987	72·530	74·073	75·616
5	77·160	78·703	80·246	81·789	83·332	84·876	86·419	87·962	89·505	91·048

- 1 English pound (lb.) per sq. foot = 4·883 kg. per sq. metre (sq.m.)
- 1 " " " sq. inch = 0·07031 kg. per sq.m.
- 1 " ton per sq. inch = 158 kg. per sq.cm.
- 1 " pound per cub. foot = 16·02 gm. per litre.
- 1 kilogram per sq. metre = 0·2048 lb. per sq. foot.
- 1 English grain per gallon = 0·014286 gm. per litre.
- 1 " " " English cub. foot = 2·287 gm. per cub. metre.
- 1 gm. per litre = 70 grains per gallon = 0·06248 lb. per cub. foot.
- 1 metre-kilogram (mkg.) = 7·235 foot-pounds.
- 1 foot-pound = 0·1382 mkg.
- 1 foot-pound per cub. foot = 4·8807 mkg. per cub. met.

TABLE 38.—WEIGHT OF SHEET METALS.

Weight of a Superficial Foot.

Thick-ness.	Wrought Iron.	Cast Iron.	Steel.	Copper.	Brass.	Lead.	Zinc.
Inch.	Lb.	Lb.	Lb.	Lb.	Lb.	Lb.	Lb.
$\frac{1}{16}$	2·53	2·34	2·55	2·89	2·73	3·71	2·34
$\frac{1}{8}$	5·05	4·69	5·10	5·78	5·47	7·42	4·69
$\frac{3}{16}$	7·58	7·03	7·66	8·67	8·20	11·13	7·03
$\frac{1}{4}$	10·10	9·38	10·21	11·76	10·94	14·83	9·38
$\frac{5}{16}$	12·63	11·72	12·76	14·45	13·67	18·54	11·72
$\frac{3}{8}$	15·16	14·06	15·31	17·34	16·41	22·25	14·06
$\frac{7}{16}$	17·68	16·41	17·87	20·23	19·14	25·96	16·41
$\frac{1}{2}$	20·21	18·75	20·42	23·13	21·88	29·67	18·75
$\frac{9}{16}$	22·73	21·09	22·97	26·02	24·61	33·38	21·09
$\frac{5}{8}$	25·27	23·44	25·52	28·91	27·34	37·08	23·44
$\frac{11}{16}$	27·79	25·78	28·07	31·80	30·08	40·79	25·78
$\frac{3}{4}$	30·31	28·13	30·63	34·69	32·81	44·50	28·13
$\frac{13}{16}$	32·84	30·47	33·18	37·58	35·55	48·21	30·47
$\frac{7}{8}$	35·37	32·81	35·73	40·47	38·28	51·92	32·81
$\frac{15}{16}$	37·90	35·16	38·28	43·36	41·02	55·63	35·16
1	40·42	37·50	40·83	46·25	43·75	59·33	37·50

TABLE 39.—COINAGE OF DIFFERENT COUNTRIES.

	Exact Value in		
	£	s.	d.
Austria—			
1 Vereins Thaler (=1 former Prussian Thaler)	0	2	11·24
1 Gulden=100 Neukreuzer	0	1	11·49
1 Maria Theresia Thaler	0	4	1·46
1 Dukaten	0	9	4·78
4 Gulden Gold=10 Francs ; 8 Gulden Gold =20 Francs			
Belgium=France.			
Brazil—			
1 Milreis=1000 Reales	0	2	3·48
Chili—			
1 Peso=100 Centavos	0	8	11·58
Denmark—			
1 Rigsbankdaler=6 Marks=90 Skillings	0	2	2·67
1 Krone=100 Oere	0	1	0·83
East India—			
1 Rupee=16 Annas	0	1	4
Egypt—			
1 Bag of Gold=80,000 Piastres	273	2	10
1 Piastre=40 Para.	0	0	2·5
France—			
1 Franc=100 Centimes	0	0	9·516
The 20-Franc piece contains 5·8065 g. fine gold	0	15	10·31
The 5-Franc piece contains 22·5 g. fine silver	0	3	11·58
German Empire—			
1 Mark=100 Pfennig	0	0	11·748
The 20-Mark piece contains 7·1685 g. fine gold	0	19	6·96
The 5-Mark piece contains 25 g. fine silver			...
Great Britain—			
1 Pound Sterling contains 7·3224 g. fine gold	1	0	0
1 Shilling contains 5·231 g. fine silver	0	1	0

TABLE 39—Continued.

	Exact Value in		
	£	s.	d.
Greece—			
1 Drachma = 100 Lepta = 1 Franc (= France).	0	0	9·516
Italy—			
1 Lira = 1 Franc (= France)	0	0	9·516
Japan—			
1 Gold Yen	0	4	1
Mexico—			
1 Piastre (Peso, Mexican Dollar) = 8 Reales = 100 Cents	0	4	3·5
1 Doblón = 16 Piastres	3	8	8
Netherlands—			
1 Guilder = 100 Cents	0	1	8
1 Willems d'Or	0	16	6·4
1 Ducat	0	9	4·5
Norway—			
1 Krone = 100 Oere	0	1	0·83
1 Species Daler = 120 Skillings	0	4	5·43
Persia—			
1 Toman = 10 Keran	0	9	0·31
1 Rupee Silver	0	1	6·2
Peru—			
1 Sol (Peso) = 10 Dineros = 100 Centavos	0	3	11·58
Portugal—			
1 Milreis (in accounts)	0	4	6·75
1 Milreis (silver)	0	4	0·46
1 Tostao = 100 Reis	0	0	4·8
Roumania—			
1 Piastre = 1 Franc (France)	0	0	9·516

TABLE 39—Continued.

	Exact value in		
	£	s.	d.
Russia—			
1 Silver Rouble = 100 Kopeks	0	3	2·06
1 Half-Imperial = 5 Rouble Gold = 5·9987 g. fine gold	0	16	4·61
1 Paper Rouble	0	2	7·7
Servia—			
1 Dinar = 1 Franc (= France)	0	0	9·516
Spain—			
1 Peseta = 1 Franc (= France)	0	0	9·516
1 Duro (Spanish Dollar) = 2 Escudos = 5 Pesetas = 20 Reales	0	3	11·58
Sweden—			
1 Kronor = 100 Oere	0	1	0·83
Switzerland = France.			
Turkey—			
1 Piastre = 40 Para = 120 Asper	0	0	2·1
1 Turkish Pound (Yuslik)	0	18	1
United States—			
1 Dollar = 10 Dimes = 100 Cents	0	4	1·15
1 Eagle = 10 Dollars = 15·0463 g. fine gold	2	1	1·16

SPECIAL PART



I. FUEL AND FURNACES.

A.—Fuel.

Should be tested in the case of lignite, peat, coal, coke. Refer to the Appendix as to sampling.

1. *Moisture*.—Heat 100 to 200 g. of coal to 105° C. (not above), for two hours, preventing access of air as much as possible. At a higher temperature the result might be too high, owing to escape of volatile matters, or too low, owing to a partial oxidation. The sample should be broken up quickly into pieces not smaller than a bean, otherwise too much water would evaporate during the process. Lignite and peat are heated to 100° C. for five or six hours, and repeatedly weighed, till no further diminution of weight takes place. Coke is heated to 110° C. for two hours.

All other tests are made with *air-dried* material. The average sample is weighed before taking the samples for the tests; it is then spread out in a thin layer and allowed to lie in ordinary dry air for forty-eight hours. It is then weighed again, and the results obtained with such air-dried fuel are calculated on the original (undried) material.

2. *Residual Coke (Fixed Carbon)*.—One g. of finely powdered coal is placed in a platinum crucible at least 1½ in. deep, provided with a tightly fitting cover. The crucible should then be heated by means of an ordinary Bunsen burner, the flame of which should not be less than 7 in. high. The crucible should be supported on a triangle of thin wire, and it should be so placed that the space between the bottom and the top of the burner is not more than 1½ in. The heating ought not to last longer than a few minutes, but must be continued as long as any appreciable quantity of inflammable matter escapes. If the flame be smaller, or the crucible be supported by a stout wire triangle, the yield of coke will be too high. The results should always be calculated upon coal or coke free from ash, in order to render them comparative. Good coal for reverberatory furnaces should yield from 60 to 70 per cent. of coke.

3. *Ash*.—This estimation is very simple for lignite or peat; coke requires a very high temperature; coal which cakes presents most difficulties. The latter must be powdered very finely, and heated up gradually, so that the volatile matters may escape before the powder can form a cake. If an analysis is only occasionally required, 1 to 3 g. of finely ground coal is heated in a platinum crucible, which is fitted in a hole into a stoneware

slab, or better, in asbestos board (Fig. 1). This is placed in a slanting position on a tripod stand. The slab serves to separate the air required for oxidation from the gases of the burner, and greatly hastens the combustion, which is thus completed in two hours, whereas without the slab it frequently remains incomplete even after eight or ten hours' heating. It is not advisable to use a blow-pipe, because the chance of mechanical loss is thereby greatly increased. If determinations have to be made frequently, it is preferable to effect the combustion in a muffle furnace, or still more quickly in a platinum boat placed in a heated porcelain tube, through which a current of oxygen is passed. When using the latter, the coal or coke should be broken in small pieces, and not ground fine, or else the oxygen does not come sufficiently into contact with the lower strata.

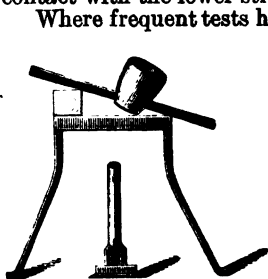


FIG. 1.

Where frequent tests have to be made, several platinum dishes can be placed in a muffle at the same time. It is best to cover the dishes or boats at first by a mica plate and to remove this only when the gases have been driven off, after which the ignition is continued, until no more black spots are visible and the weight remains constant.

4. *Sulphur* (Eschka's method).— Mix 0.5 to 1 g. of the finely ground coal with $1\frac{1}{2}$ times its weight of an intimate mixture of 2 parts of well-burnt magnesia and 1 part of anhydrous sodium carbonate. The mixture is made in a platinum crucible by means of a glass rod, and the crucible, without putting on the cover, is heated in an inclined position, in such manner that only its lower portion attains a red heat. This is most conveniently done by placing it in an asbestos board, provided with a hole, as shown in Fig. 1. The combustion of the sulphides to sulphates should be promoted by frequent stirring with a thick platinum wire; it will be finished in about an hour, during which time the grey colour of the mixture mostly passes into yellow, red, or brown. The calcined mass is covered with water and bromine water added, until the liquid shows a slight yellow colour. Then heat the whole to boiling, decant the liquid through a filter, and wash the residue with hot water. Add hydrochloric acid to the aqueous solution, boil till all the bromine has been removed and the liquid has been decolorised, and add a solution of barium chloride, drop by drop, always at a boiling heat, until the precipitation is complete. If the magnesia or the sodium carbonate employed are not quite free from sulphates, these must be separately estimated and the amount deducted from the total sulphur found. Even if the gas employed for heating the crucible

should contain a notable quantity of sulphur, there is no error caused by this, if the products of combustion are kept away from the contents of the crucible by the asbestos shield as shown in the figure. One part BaSO_4 indicates 0.1373 parts S.

5. *The calorific power* of fuel can be estimated by ascertaining the percentage of carbon and hydrogen, according to the ordinary methods of elementary analysis, and calculating the results according to Dulong's formula. In the case of coal it is necessary to take account of the volatile sulphur—that is, that which is determined by heating in a current of oxygen, passing the gases through neutralised hydrogen peroxide, and titrating the sulphuric acid formed. If the percentage of C, H, and (volatile) S, and that of the moisture (W), is known, the percentage of the oxygen is expressed by the equation:—

$$O = 100 - (C + H + S + W + \text{ash}).$$

The nitrogen contained in the coal may be neglected. The calorific power of the coal, expressed in gram-calories, is then

$$= 80.3 C + 288 \left(H - \frac{O}{8} \right) + 25 S - 6 W.$$

A direct estimation of the heating power of fuel can be made by means of the calorimetric bomb, of which a description is given in *Tech. Meth.*, vol. i., p. 254.

B.—Furnaces.

1. *Chimney Gases.*—In these, CO_2 , O, CO, and N (the latter by difference) are most conveniently estimated by the Orsat apparatus, shown in Fig. 2. This consists of a gas-burette, A, connected with the level-bottle B by means of a rubber tube. A is filled to the zero point with water, and by lowering B gas is aspirated, either from the supply tube C or from the absorption pipettes D, E, F. The gas is forced into each of these pipettes by opening its special tap and raising B. For reading the volume of gas in A, the bottle B must be held in such a position that the level of water is the same in A and B.

The absorption pipettes are charged as follows:—Tube D receives 110 c.c. of caustic potash solution of specific gravity 1.20 to 1.28. This absorbs CO_2 , and can serve for a long time. Tube E serves for absorbing the oxygen by means of very thin sticks of phosphorus, kept under water. This tube, when not in use, should be protected from the light by a covering of black paper. Any tarry matters getting into this tube render the phosphorus inactive, and must therefore be kept out by filtering the gas before entering into C, through asbestos, cotton-wool, or other material. The absorption of the oxygen by the phosphorus only

sets in at 16° C., better at 18° C. In case the room is at a lower temperature, the vessel E must be cautiously warmed up by a spirit-lamp. In tube F the carbon monoxide is absorbed. For this purpose a solution is prepared by shaking up in a closed bottle 250 g. cuprous chloride with a solution of 250 g. ammonium chloride in 750 c.c. water. When completed, a spiral of copper wire, reaching from top to bottom, is introduced into the stock bottle. This bottle is always kept well closed when

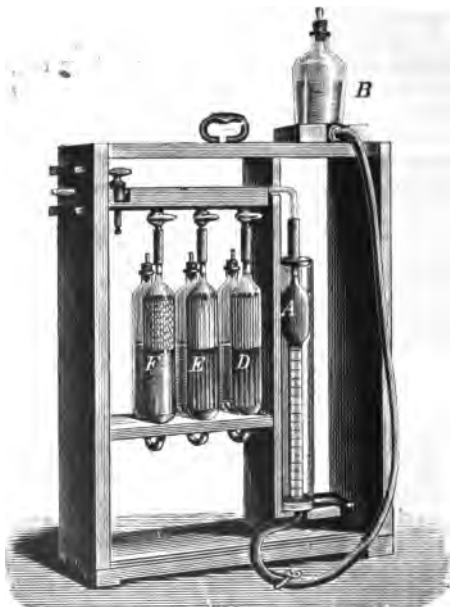


FIG. 2.

not in use. Before charging tube F, 3 vols. of the solution from the stock bottle are mixed with 1 vol. liquor ammonia, specific gravity 0.905. One c.c. of this mixture ought to absorb 16 c.cm. CO, but this requires prolonged shaking. The reagent in F must be frequently renewed; if this is neglected, it may even yield up some CO to gases containing too little of it. The reagent in F also absorbs ethylene, but this gas does not occur in chimney gases. Since the solution in F also absorbs oxygen, the latter must always be removed before employing pipette F.

For daily use it is mostly sufficient to test merely for CO_2 , by means of the caustic potash solution in pipette D.

Checking the working of Furnaces.—The estimation of CO_2 in the chimney gases, if combined with an observation of temperature, admits of checking both the efficiency of a furnace or boiler and the daily work of the firemen, according to a formula worked out by Lunge (*Zsch. f. angew. Chem.*, 1889, p. 240). A consecutive number, say from 10 to 15 tests for CO_2 , are made by an Orsat apparatus in the flue leading from the furnace to the chimney, and the mean volume percentage of CO_2 found is called n . At the same time, a thermometer with very long stem, tightly inserted in the testing hole in such manner that its bulb is well within the flue, but that the scale can be read off outside, is observed at frequent intervals, and the mean temperature of the gases is called t' , that of the air outside t . c is the specific heat of a cubic metre of CO_2 , expressed in gram-calories; c' that of N or O (see below). The total volume of exit-gases produced by the combustion of 1 kg. of carbon burnt on the grate is $= 1.854 + 1.854 \left(\frac{100-n}{n} \right)$ cubic metres, and the loss of heat in the exit-gases, expressed in gram-calories:—

$$L = 1.854(t' - t)c + 1.854(t' - t) \left(\frac{100-n}{n} \right) c'$$

The loss, expressed in per cent. of the heat theoretically given out by the carbon, is:—

$$\frac{100L}{8080}$$

The value of c' may be assumed for all temperatures $= 0.31$; that of c varies with the temperature, and must be taken as follows:—

If t' is below	150° C.,	$c = 0.41$.
„ between	150-200°	$= 0.43$.
„ „	200-250°	$= 0.44$.
„ „	250-300°	$= 0.45$.
„ „	300-350°	$= 0.46$.

Note.—The observations of n and t' must be made several times in succession, and the average value taken as final. For accurate investigations several series of tests must be made at different times of the day.

Instruments have been devised for a continuous approximate check of the percentage of CO_2 in chimney gases, such as Arndt's Oeconometer.

2. *Gas from Producers (Generators).*—In this usually only CO_2 and CO are estimated by means of Orsat's apparatus, as described, p. 97. Any ethylene present in the producer gas would

be absorbed and estimated together with the CO. *Hydrogen* can be estimated in the residue from absorbing CO_2 , CO C_2H_4 , and O by mixing it with a measured volume of air, and passing the mixture over gently heated platinum or palladium asbestos.* The estimation is most conveniently done in Lunge's modification of Orsat's apparatus, Fig. 3. The indicating letters correspond to those in Fig. 2, but there is an additional U-tube, G, connected with a capillary, H, of refractory glass. H contains platinum or



FIG. 3.

palladium asbestos and can be heated by the small spirit lamp I, turning on a pivot. The U-tube G is filled with water. The gas freed from CO_2 , CO C_2H_4 , and O (if this be present) is mixed in the gas-burette A with as much air as the space will allow, and

* This can be obtained ready-made or is prepared by soaking a few threads of long soft asbestos in a strong solution of platinum or palladium chloride, mixed with a saturated solution of sodium formate and enough sodium carbonate to produce an alkaline reaction. After one hour's soaking the asbestos is dried completely in a water-bath, whereby the metal is precipitated in a very minute state of division. The soluble salts are then washed out by hot water and the asbestos again dried

a reading is taken. This air will suffice for a quantity of hydrogen corresponding to $\frac{1}{10}$ of the employed volume of air (*i.e.*, twice the volume of oxygen contained in that air). If more H be present, which will only occur with "water gas," either less than 100 c.c. of gas must be employed at the commencement for the analysis, or the residual gas is mixed with oxygen instead of with air. The capillary tube H is heated very gently by means of the lamp I, and the gaseous mixture is quickly passed once through it into G and back again, when one end of the platinum asbestos should become red hot. The residual gas is again measured and $\frac{3}{8}$ of the diminution in volume calculated as hydrogen. If methane (marsh gas, CH_4) is to be estimated, the residue from the last operation is mixed with more air and burnt by means of an electrically heated palladium or platinum wire, enclosed in a capillary tube. If a capillary platinum tube is employed, filled

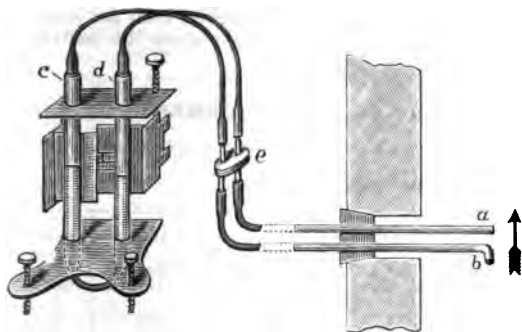


FIG. 4.



FIG. 5.

with a few platinum wires, so as to leave a very small space for the gases to pass through, the electric heating may be replaced by that of a broad gas flame, producing a strong red heat.

3. *Speed of Draught.*—A convenient apparatus for measuring this in chemical works, where any fine mechanism would soon be ruined, is Fletcher's anemometer, based upon the movement of a column of ether in a U-tube (described in Lunge's *Sulphuric Acid and Alkali*, 3rd edition, vol. i., p. 564). Fig. 4 shows this in the simpler form, leaving out the microscopes, which are quite unnecessary for reading the divisions of the scale or the vernier. The ends of the glass tubes *a b* should be placed rather less than one-sixth of the diameter of the flue from its inner wall. The straight end of *a* ought to be as exactly parallel as possible to the

direction of the draughts; the end of *b* ought to be exactly at a right angle to this, and so that the current blows straight into it. Without this precaution a mistake is made, which is avoided by the arrangement shown in Fig. 5, and proposed by Hurter, viz., employing tubes with ends bent in opposite directions. The tubes *a b* communicate with the ether tube *c d*; the draught causes the ether to rise in *a* by aspiration and to fall in *b* by the pressure of the air blowing into the tube. The difference of level between *c* and *d* is read off by means of the scale and vernier. The sliding disc *e* is then turned through 180°, whereby the currents are reversed. There will now be a difference of levels in the opposite direction, but equal in amount to the first, if the observation is correct. The sum of these two differences is the "anemometer reading" given in the tables.

The following tables show the application of the readings of the Anemometer for calculating the speed of draughts, both for instruments graduated on the inch scale and for those on the metrical scale.

a.—TABLE TO SHOW THE SPEED OF CURRENTS OF AIR.

At a temperature of 15° C. = 60° F.; Barometer, 760 mm. = 29.92 inches.

A.—Readings in Inches.

Anemometer Reading. Inches.	Speed. Feet per Second.	Anemometer Reading. Inches.	Speed. Feet per Second.	Anemometer Reading. Inches.	Speed. Feet per Second.	Anemometer Reading. Inches.	Speed. Feet per Second.
·01	2·855	·16	11·42	·32	16·15	·95	27·83
·02	4·088	·17	11·77	·34	16·65	1·00	28·55
·03	4·945	·18	12·11	·36	17·13	1·25	31·93
·04	5·710	·19	12·45	·38	17·60	1·50	34·97
·05	6·384	·20	12·77	·40	18·06	1·75	37·77
·06	6·993	·21	13·08	·45	19·15	2·00	40·37
·07	7·554	·22	13·39	·50	20·18
·08	8·075	·23	13·70	·55	21·17
·09	8·565	·24	13·99	·60	22·12
·10	9·028	·25	14·28	·65	23·02
·11	0·469	·26	14·56	·70	23·89
·12	9·891	·27	14·84	·75	24·73
·13	10·29	·28	15·11	·80	25·54
·14	10·68	·29	15·38	·85	26·32
·15	11·06	·30	15·64	·90	27·08

B.—Readings in Millimetres.

Read- ing.	Speed.	Read- ing.	Speed.	Read- ing.	Speed.	Read- ing.	Speed.	Read- ing.	Speed.	Read- ing.	Speed.
mm.	m.	mm.	m.	mm.	m.	mm.	m.	mm.	m.	mm.	m.
0.1	0.575	1.4	2.040	2.7	2.888	5.0	8.855	10.0	5.452	19.0	7.515
0.2	0.771	1.5	2.111	2.8	2.885	5.2	8.981	10.5	5.586	20.0	7.710
0.3	0.944	1.6	2.181	2.9	2.985	5.4	4.006	11.0	5.718	21	7.900
0.4	1.090	1.7	2.248	3.0	2.986	5.6	4.080	11.5	5.846	22	8.066
0.5	1.205	1.8	2.313	3.2	3.077	5.8	4.152	12.0	5.972	23	8.268
0.6	1.341	1.9	2.376	3.4	3.179	6.0	4.223	12.5	6.095	24	8.446
0.7	1.442	2.0	2.438	3.6	3.271	6.5	4.395	13.0	6.216	25	8.620
0.8	1.560	2.1	2.498	3.8	3.361	7.0	4.561	13.5	6.334	30	9.448
0.9	1.686	2.2	2.557	4.0	3.448	7.5	4.721	14.0	6.450	35	10.199
1.0	1.724	2.3	2.615	4.2	3.469	8.0	4.876	15.0	6.667	40	10.908
1.1	1.808	2.4	2.671	4.4	3.616	8.5	5.026	16.0	6.896	45	11.565
1.2	1.839	2.5	2.726	4.6	3.698	9.0	5.172	17.0	7.108	50	12.190
1.3	1.966	2.6	2.779	4.8	3.777	9.5	5.314	18.0	7.314		

β.—CORRECTIONS FOR TEMPERATURE.

Column *a* shows the temperature of the chimney or flue, column *b* the factor for multiplying the figure found in Table *a* in order to arrive at the real speed of the current of gas.

A.—Readings in Degrees Fahrenheit.

Fahr. <i>a.</i>	<i>b.</i>	<i>a.</i>	<i>b.</i>	<i>a.</i>	<i>b.</i>	<i>a.</i>	<i>b.</i>
0	1.0634	90	0.9723	180	0.9012	380	0.7865
5	1.0577	95	0.9679	185	0.8977	400	0.7763
10	1.0520	100	0.9636	190	0.8943	425	0.7663
15	1.0464	105	0.9593	195	0.8909	450	0.7556
20	1.0409	110	0.9551	200	0.8875	475	0.7454
25	1.0355	115	0.9509	210	0.8808	500	0.7356
30	1.0302	120	0.9468	220	0.8743	525	0.7261
35	1.0250	125	0.9428	230	0.8680	550	0.7171
40	1.0198	130	0.9388	240	0.8614	575	0.7085
45	1.0148	135	0.9348	250	0.8557	600	0.7000
50	1.0098	140	0.9309	260	0.8497	650	0.6841
55	1.0049	145	0.9270	270	0.8438	700	0.6691
60	1.0000	150	0.9232	280	0.8380	750	0.6552
65	0.9952	155	0.9194	290	0.8324	800	0.6420
70	0.9905	160	0.9156	300	0.8269	850	0.6297
75	0.9858	165	0.9119	320	0.8163	900	0.6181
80	0.9812	170	0.9083	340	0.8060	950	0.6070
85	0.9767	175	0.9047	360	0.7960	1000	0.5964

B.—Readings in Degrees Centigrade.

a. t° C.	b.	a. t° C.	b.	a. t° C.	b.	a. t° C.	b.	a. t° C.	b.	a. t° C.	b.
-10	1·046	18	0·995	42	0·956	66	0·922	140	0·885	260	0·785
-5	1·086	20	0·991	44	0·953	68	0·919	150	0·825	270	0·728
0	1·027	22	0·988	46	0·950	70	0·916	160	0·815	280	0·721
2	1·023	24	0·985	48	0·947	75	0·909	170	0·806	290	0·715
4	1·020	26	0·981	50	0·944	80	0·905	180	0·797	300	0·709
6	1·016	28	0·978	52	0·941	85	0·897	190	0·788	320	0·697
8	1·012	30	0·975	54	0·938	90	0·890	200	0·780	340	0·685
10	1·009	32	0·972	56	0·935	95	0·884	210	0·772	360	0·676
12	1·005	34	0·968	58	0·933	100	0·878	220	0·764	400	0·654
14	1·003	36	0·965	60	0·930	110	0·867	230	0·756	450	0·631
15	1·000	38	0·962	62	0·927	120	0·856	240	0·749	500	0·608
16	0·998	40	0·959	64	0·924	130	0·845	250	0·742		

A very simple and cheaper instrument is Seger's Differential Anemometer, Fig. 6. The U-tube A is surmounted by two enlargements, B and C. D is a sliding scale, adjustable by slits *aa* and screw-pins *bb*. The tube is filled with two non-miscible liquids of nearly equal specific gravity; for instance, paraffin oil and dilute spirits of wine (coloured). The line of contact, at X, is the zero point of the scale D. If an aspirating force is acting on the surface of the liquid in C, the level of the liquid will be raised in C, and the point X will be lowered in a multiplied ratio, corresponding to the difference in the sectional areas of the narrow part of A and the enlargements in C, say 1 : 20.

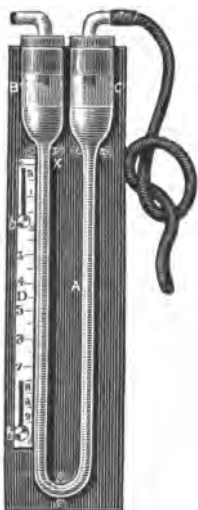


FIG. 6.

C.—Temperature.

The measurement of temperatures up to about 300° C. calls for no special remark, as the ordinary mercurial thermometers are always used. For higher temperatures a large number of *pyrometers* have been constructed. All of these are unreliable after prolonged use, many of them even from the very beginning, and they require a frequent control of their indications by calorimetric methods. Among these "empirical" pyrometers those mostly used are: Gauntlett's (up to 900° C. or 1600° F.), Steinle and Hartung's graphite pyrometer (up to 1200° C.), or Klinghammer's

Thalpotasimeter. In many cases Prinsep's metallic alloys, of definite fusing points, and Seger's cones, do good service; the fusing points corresponding to the commercial forms of these have been given on p. 37.

The calorimetric control can be effected by any of the well-known calorimeters, such as Mahler's or Fischer's, but is a somewhat difficult and complicated operation, and the working of the air pyrometer is even more so.

Most of the drawbacks formerly connected with pyrometry have been removed by the construction of Le Chatelier's *Thermo-electric Pyrometer*. Its working part is shown in Fig. 7. It consists of a thermo-couple, composed of wire *a* of pure platinum and a wire *b*, of an alloy of 90 parts of platinum + 10 parts of rhodium, soldered to the former. These wires are insulated by porcelain tubes *c, d*, about 3 feet long, and protected on the outside, against heating gases, by the iron pipe *e, e*. The wires are

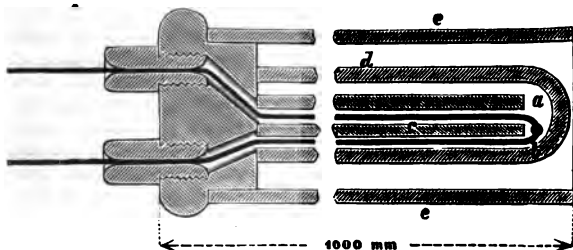


FIG. 7.

connected with platinum or copper wires, leading to a galvanometer, and the indications of the needle of the latter show the temperature at the point where *a* and *b* are soldered together. The temperature scale marked on the galvanometer is fixed by comparing it with an air pyrometer at the works where the instruments are made.

The following rules must be observed for the use of this pyrometer. The galvanometer should be placed in a horizontal position and so as to be protected against mechanical oscillations, preferably on a wall-bracket, and this may be at some distance from the pyrometer itself—*e.g.*, in the manager's office. Before moving the galvanometer from its place, the needle should be always arrested. After fixing it on its bracket, the arresting-screw is cautiously loosened, until the needle begins to move. If it does not point to zero, after being placed in a horizontal position, this must be effected by moving the adjusting screws. The electric resistance of the conducting wire should not appreciably exceed 1 ohm; up to distances of about 300 feet this will be

attained by employing insulated copper wire of $\frac{1}{32}$ -inch thickness. The junction of the couple with the conducting wires ought not to be much above the ordinary temperature. If one of the wires should break, the contact can be re-established by twisting the ends tightly together for a length of about $\frac{1}{2}$ inch; it is preferable to fuse them together in an oxyhydrogen flame. If the temperature within the furnace does not exceed 1000° C., the pyrometer may be left permanently inside; for higher temperatures, which would cause the iron pipe to soften and to burn away too rapidly, the pyrometer should be taken out and introduced merely for taking an observation, which may be done ten minutes afterwards. Even then it is best to provide a fire-clay slab on which the instrument can rest. Le Chatelier's pyrometer may be employed for temperatures up to 1500° C. For higher temperatures, up to 2100° , W. C. Heraeus (Hanau, Germany) has constructed a thermocouple, consisting of a wire of pure iridium, fused to another wire of an alloy of 90 parts iridium + 10 ruthenium.

For such high temperatures Wanner's pyrometer is now frequently used. It allows a photometric comparison of the polarised light from a small electric lamp with that of the furnace, etc., to be tested, by means of an instrument like a telescope; it is easy to handle, and is serviceable for approximately measuring temperatures above 1500° C., where Le Chatelier's pyrometer cannot be employed. It is also more convenient than the latter for estimating temperatures inside the furnace at some distance from the front of the furnaces. (Supplied by Townson & Mercer, London.)

D.—Feed-Water for Steam-Boilers, etc.

1. *Hardness*.—The English degrees of hardness are based on the unit of 1 part CaCO_3 , or its equivalent of MgCO_3 , in 70,000 parts of water (grains to the gallon). The French degrees signify each 1 part CaCO_3 (or MgCO_3) in 100,000 water, the German degrees that of 1 part CaO (or MgO) in 100,000 water.

The testing for hardness was formerly mostly effected by Clark's soap test. The methods to be described here are both simpler and more accurate than the soap test.

(a) *Temporary Hardness* (alkalinity) is that which is removed by prolonged boiling, by which operation nearly all the CaCO_3 and some of the MgCO_3 is precipitated. This can be estimated with sufficient approximation by testing the water alkalimetrically, employing $\frac{1}{2}$ normal hydrochloric acid and methyl orange as indicator, at the ordinary temperature, until the first reddish tint appears. When employing 200 c.c. of the water for this test, the number of c.c. of $\frac{1}{2}$ normal acid used, multiplied by 3.5, indicates the English degrees of temporary hardness (for French degrees multiply by 5, for German degrees by 2.8).

Where feed-water, purified by means of sodium carbonate, is

tested in this way, an error may be caused by the presence of an excess of Na_2CO_3 , which makes the hardness appear too high. In such cases the 200 c.c. of water employed should be boiled in a porcelain dish for some time, the precipitated carbonates removed by filtration, and the filtrate titrated as above. The acid then used corresponds to the Na_2CO_3 and a little unprecipitated MgCO_3 .

(b) *Total Hardness*.—Add to 200 c.c. of the feed-water hydrochloric acid in slight excess, boil down to about 50 c.c.; wash this into a 100 c.c. flask, neutralise exactly with caustic soda solution, employing methyl orange as indicator; add 20 c.c. of a mixture of equal volumes of $\frac{1}{2}$ normal caustic soda solution and $\frac{1}{2}$ normal sodium carbonate solution, boil, allow to cool, fill up the flask to the 100 c.c. mark with distilled water, pour through a dry filter, and estimate the unsaturated alkali in 50 c.c. of the filtrate by $\frac{1}{2}$ normal hydrochloric acid and methyl orange. Multiply the c.c. of acid used by 2, and deduct this from 20; the remainder = a shows the alkali consumed for precipitating the alkaline earths contained in 200 c.c. of water. The total hardness is hence, = $3.5a$ in English degrees, $5a$ in French, $2.8a$ in German degrees. This process is accurate also, in presence of magnesia. By deducting the degrees of alkalinity found in a from the total hardness found in b , the *permanent hardness* is obtained—*i.e.*, that which is caused by calcium sulphate.

Water having a total hardness of less than 8° (English) is considered as *soft*, from 8° to 15° as *moderately hard*, above 15° as *hard*.

(c) *Residue on Evaporation*.—In the case of water containing but little MgO , a convenient check for the total hardness—*i.e.*, the sum of alkalinity a and permanent hardness b —is afforded by evaporating 500 c.c. down to dryness, heating to decompose the organic matter, moistening with a solution of CO_2 in distilled water, and drying at 110°C . Since the degrees of hardness are all calculated for CaO , the value of c will not be quite equal to $a + b$, if any considerable quantity of magnesia is present, and this indirectly proves the presence of more magnesia than usual.

2. *Estimation of the Reagents (lime water and sodium carbonate) required for Purifying Water*.—Add to 500 c.c. of the water 10 c.c. of a $\frac{1}{2}$ normal sodium carbonate solution, evaporate to dryness, take up the residue with a small quantity of water, filter through a small filter, wash till there is no further alkaline reaction, and estimate the unconsumed sodium carbonate in the filtrate plus washings by titrating with methyl orange and $\frac{1}{2}$ normal hydrochloric acid. If a c.c. of $\frac{1}{2}$ normal sodium carbonate are used in the titration, then $2a \times 0.0106$ shows the grams of pure sodium carbonate required for removing the calcium sulphate—*i.e.* the *permanent hardness*.

The amount of lime water required for removing the *temporary hardness* is estimated as follows:—To 500 c.c. of water add 100

c.c. of clear lime water, after having previously determined its percentage of CaO by titrating with $\frac{1}{2}$ normal hydrochloric acid and phenolphthalein (methyl orange is not applicable in this case, because this would indicate also the CaCO₃, present in small quantities along with Ca(OH)₂, which would be wrong). Heat the mixture during half an hour in a covered flask (to keep out CO₂), allow to cool, pour through a dry filter, and titrate, without delay, 500 c.c. of the filtrate. The HCl now used, increased by one-fifth (since the original 500 c.c. of water had been brought to 600 c.c.), shows the quantity of lime not used up. By deducting this from the CaO originally contained in 100 c.c. of the lime water, the quantity of CaO required for destroying the temporary hardness of $\frac{1}{2}$ litre of the water to be tested, is ascertained.

II. SULPHURIC ACID MANUFACTURE.

A.—Brimstone.

1. *Moisture*.—This should be estimated by drying an average sample of 100 g. at 70° for a few hours, in an oven or water-bath. The sample must be prepared without losing any moisture during the operation; the brimstone for this purpose must, therefore, not be ground, but only coarsely crushed, as quickly as possible.

2. *Bituminous Substances* (Fresenius).—Remove the sulphur by heating the sample for some time a little over 200° C., taking care that it does not take fire, weigh the residue, and deduct the ash found in No. 3.

3. *Ash*.—Burn 10 g. in a porcelain dish and weigh the residue. Some samples of brimstone contain carbonaceous matter. In this case (which is easily recognised by the appearance of the sample) the flame must be removed immediately after the sulphur has been burned, and before the carbon has taken fire, so that the latter is not calculated as sulphur.

4. *Arsenic*.—Treat 10 g. brimstone with dilute liquor ammonia at 70° to 80° C. To dissolve the As₂S₃, filter, neutralise the filtrate exactly with dilute nitric acid, and titrate with decinormal silver nitrate solution, until a drop gives a brown colour with a solution of neutral potassium chromate. Each c.c. of the silver nitrate solution indicates 0·041 per cent. As₂S₃. If the arsenic should be present as ferric or calcium arsenate (this never occurs in the case of native brimstone, but it may do so in the case of sulphur recovered from Leblanc soda residue), the sample must be extracted with carbon bisulphide, the residue oxidised by aqua regia, and the sulphur estimated as in pyrites (see below).

5. *Direct Estimation of Sulphur* (Macagno, *Chem. News*, v., 43, p. 192).—Fifty g. of the finely ground brimstone are dis-

solved in 200 c.c. carbon bisulphide by digesting in a stoppered bottle at the ordinary temperature, and the specific gravity of the liquid = s is estimated. This must be reduced to the specific gravity at 15° C. = S , by means of the formula (valid up to 25° C.) $S = s + 0.0014(t - 15)$. The following table gives, for each value of S , the percentage in this solution, which number must be multiplied by 4 to indicate the percentage of sulphur in the sample of brimstone :—

Specific Gravities of Solutions of Sulphur in Carbon Bisulphide.

Spec. Grav.	% S	Spec. Grav.	% S	Spec. Grav.	% S	Spec. Grav.	% S	Spec. Grav.	% S
1.271	0	1.296	6.0	1.321	12.1	1.346	18.1	1.371	25.6
1.272	0.2	1.297	6.3	1.322	12.3	1.347	18.4	1.372	26.0
1.273	0.4	1.298	6.5	1.323	12.6	1.348	18.6	1.373	26.5
1.274	0.6	1.299	6.7	1.324	12.8	1.349	18.9	1.374	26.9
1.275	0.9	1.300	7.0	1.325	13.1	1.350	19.0	1.375	27.4
1.276	1.2	1.301	7.2	1.326	13.3	1.351	19.3	1.376	28.1
1.277	1.4	1.302	7.5	1.327	13.5	1.352	19.6	1.377	28.5
1.278	1.6	1.303	7.8	1.328	13.8	1.353	19.9	1.378	29.0
1.279	1.9	1.304	8.0	1.329	14.0	1.354	20.1	1.379	29.7
1.280	2.1	1.305	8.2	1.330	14.2	1.355	20.4	1.380	30.2
1.281	2.4	1.306	8.5	1.331	14.5	1.356	20.6	1.381	30.8
1.282	2.6	1.307	8.7	1.332	14.7	1.357	21.0	1.382	31.4
1.283	2.9	1.308	8.9	1.333	15.0	1.358	21.2	1.383	31.9
1.284	3.1	1.309	9.2	1.334	15.2	1.359	21.5	1.384	32.6
1.285	3.4	1.310	9.4	1.335	15.4	1.360	21.8	1.385	33.2
1.286	3.6	1.311	9.7	1.336	15.6	1.361	22.1	1.386	33.8
1.287	3.9	1.312	9.9	1.337	15.9	1.362	22.3	1.387	34.5
1.288	4.1	1.313	10.2	1.338	16.1	1.363	22.7	1.388	35.2
1.289	4.4	1.314	10.4	1.339	16.4	1.364	23.0	1.389	36.1
1.290	4.6	1.315	10.6	1.340	16.6	1.365	23.2	1.390	36.7
1.291	4.8	1.316	10.9	1.341	16.9	1.366	23.6	1.391	37.2
1.292	5.0	1.317	11.1	1.342	17.1	1.367	24.0		
1.293	5.3	1.318	11.3	1.343	17.4	1.368	24.3		
1.294	5.6	1.319	11.6	1.344	17.6	1.369	24.8		
1.295	5.8	1.320	11.8	1.345	17.9	1.370	25.1		

6. *Selenium* is found by fusing a sample with potassium nitrate, dissolving the mass in hydrochloric acid, and treating with sulphur dioxide, which precipitates the selenium.

7. *The degree of fineness* of ground brimstone is estimated in France by means of Chancel's sulphurimeter, *i.e.* a glass tube, closed at one end, provided with a glass stopper at the other, and graduated in 100 parts. In this, the ground brimstone is shaken up for some time with pure, anhydrous ether, and after allowing the tube to rest in a vertical position, the number of divisions occupied by the brimstone is read off (degrees Chancel).

B.—Spent Oxide of Gas-works. See "Coal Gas."

C.—Pyrites.

1. *Moisture*.—The ground pyrites is dried at 105° C. till the weight remains constant. For the following tests the pyrites is not employed in the dried state, but the finely ground average sample, kept in a well-sealed bottle. Compare the Appendix as to taking and reducing an average sample.

The analytical results are calculated for dry pyrites, for which purpose a special estimation of moisture is made with the average sample.

2. *Sulphur*.—About 0.5 g. of pyrites is treated with about 10 c.c. of a mixture of 3 vols. nitric acid (specific gravity 1.4) and 1 vol. strong hydrochloric acid, both ascertained to be absolutely free from sulphuric acid, due care being taken to avoid all spurt-ing. Quite exceptionally, the separation of a little free sulphur will be observed; if this takes place, the sulphur must be oxidised by adding a little potassium chlorate. Evaporate to dryness on a water-bath, add 5 c.c. hydrochloric acid, evaporate once more (no nitrous fumes ought to escape now), add 1 c.c. concentrated hydrochloric acid and 100 c.c. hot water, filter through a small filter, and wash with hot water. The insoluble residue may be dried, ignited, and weighed. It may contain, besides silicic acid and silicates, the sulphates of barium, lead, and even calcium, the sulphur of which, as being useless, is purposely neglected. The filtrate and washings are saturated with ammonia, avoiding much excess and keeping the liquid hot for about ten or fifteen minutes before filtration, but *not* boiling, till all the ammonia is expelled (in which case the precipitate contains some basic sulphate). The precipitated ferric hydroxide is filtered and washed. This can be done in from half to one hour, by employing the following precautions: (1) Filter hot, and wash on the filter with hot water, avoiding channels in the mass, but so that the whole precipitate is thoroughly churned up with the water each time (washing by decantation would produce too great a bulk of liquid); (2) employ sufficiently dense but rapid filtering paper; (3) use funnels, made at an angle of exactly 60°, whose tube is not too wide, and is *completely filled* by the liquid running through. A filter pump may also be employed, with the usual precautions. Wash till about 1 c.c. of the washings, on adding BaCl_2 shows no opalescence, even after a few minutes. (If there is any doubt on this point, the complete absence of basic sulphates should be investigated by drying the precipitated ferric hydroxide, fusing it with pure sodium carbonate, and testing the aqueous solution of the melt for sulphates.)

The filtrate and washings should not appreciably exceed 300 c.c., or else should be concentrated by evaporation. Acidulate with pure hydrochloric acid in very slight excess, preferably by adding acid till methyl orange is just reddened, and then adding

just 1 c.c. of strong HCl. Then heat to boiling, remove the burner, and add a solution of BaCl₂ previously heated to boiling. A large excess of BaCl₂ must be decidedly avoided. For 0.5 g. pyrites, 20 c.c. of a 10 per cent. solution of BaCl₂ is always more than sufficient. This is roughly measured off in a test-tube, provided with a mark, and heated in the same tube; it is then poured into the hot liquid *all at once*, not drop by drop. It is true that this procedure will cause a little barium chloride to be carried down along with the sulphate, but the error caused by this just compensates the opposite error, caused by the slight solubility of barium sulphate in the hot solution, containing free HCl and ammonium chloride.

After precipitation the liquid is left to stand for half an hour, when the precipitate should be completely settled. It is quite unnecessary to wait for a longer time, as is sometimes prescribed; this is not merely a waste of time, but it unnecessarily retards the work by the cooling of the liquid. Decant the clear portion as carefully as possible through a filter, pour 100 c.c. boiling water on the precipitate, and stir up. Wait two or three minutes, when the liquid ought to have settled completely, and decant again. Repeat the treatment with boiling water, and the decantation, three or four times, till the liquid ceases to give an acid reaction. Wash the precipitate on to the filter, dry, and ignite. It should be a perfectly white and loose powder. One part of it is equal to 0.13733 sulphur (factors on p. 14).

3. *Copper*.—The method employed at the Duisburg Copper Works, in its most recent form, is as follows:—Of the powdered pyrites, dried at 100° C., 5 g. is gradually dissolved in 60 c.c. of nitric acid, spec. grav. 1.2, in a flask placed in a slanting position. When the first violent reaction is over, the flask is heated and the evaporation continued until thick, white fumes of sulphuric acid escape. Dissolve the dry residue in 50 c.c. hydrochloric acid, spec. grav. 1.19, add 2 g. sodium hypophosphite, dissolved in 5 c.c. water, for the purpose of removing the arsenic and reducing the ferric chloride, boil for some time, then add an excess of concentrated hydrochloric acid, diluted with about 300 c.c. hot water, pass hydrogen sulphide into the liquid, separate the precipitate from the liquid by filtration, and wash it well. Pierce the filter paper with a glass rod, wash the precipitate back into the precipitating flask, dissolve the sulphides adhering to the filter and the principal portion of the precipitate by means of nitric acid, and evaporate the contents of the flask to dryness on the water-bath. Treat the residue with nitric acid and water, neutralise with ammonia, and add sulphuric acid in slight excess. After the liquid has cooled down, separate the clear liquid from the insoluble lead sulphate, etc., wash out the flask, and filter with water containing a little sulphuric acid, add to the filtrate 3 to 8 c.c. nitric acid, spec. grav. 1.4, and precipitate the copper electrolytically.

From the ascertained percentage of copper deduct 0·01 per cent. for bismuth and antimony.

4. *Lead* remains in the residue from the treatment with aqua regia (No. 2) or nitric acid (No. 3), as lead sulphate. This is extracted from the residue (preferably that from the nitric acid treatment) by heating with a concentrated solution of ammonium acetate. The solution is evaporated, with addition of a little pure sulphuric acid, the evaporation completed in a porcelain crucible, and the residue dried and ignited. One part $\text{PbSO}_4 = 0\cdot6829 \text{ Pb}$.

5. *Zinc* is sometimes estimated in pyrites, because the sulphur combined with it is hardly recoverable in the pyrites burners. The following method (communicated to the author by Messrs Hassreidter and Prost) should be employed in this case, in lieu of Schaffner's method described subsequently for zinc blende, because in the case of pyrites the presence of iron renders gravimetric preferable to volumetric analysis:—Dissolve 1 g. pyrites in aqua regia, as described on p. 110, expel the nitric acid, take up the residue with about 5 c.c. concentrated nitric acid, dilute with water, treat the acid solution with H_2S in order to precipitate lead, etc., filter, expel the H_2S from the filtrate by boiling, and oxidise the liquid with aqua regia. When cooled down, add ammonium carbonate, until the precipitate formed redissolves, but slowly, then add ammonium acetate, boil for a short time, and filter the liquid from the precipitated basic ferric sulphate. As this contains a little zinc, dissolve it in hydrochloric acid, precipitate it again as above, and repeat this treatment until no more zinc is found in the filtrate. The united filtrates are concentrated by evaporation. Then precipitate the zinc in the hot solution by H_2S , allow to stand for twenty-four hours, pour off the clear liquid, filter, wash the ZnS , dissolve it (without removing the filter) in dilute HCl , boil off the H_2S , precipitate with sodium carbonate, wash the ZnCO_3 , dry and ignite it. One part $\text{ZnO} = 0\cdot8034 \text{ Zn}$. For very accurate work the SiO_2 , Fe_2O_3 , and Al_2O_3 retained in the ZnO should be estimated and deducted, but this is very rarely necessary.

6. *The Carbonates* (of Ca, etc.) are sometimes estimated in pyrites, because they convert a certain quantity of sulphur into sulphate. Since their quantity is always small, the CO_2 is estimated directly by expelling with strong acids, and is easily estimated gravimetrically by absorbing it with soda-lime, etc., or, more accurately and quickly, by the volumetrical process of Lunge and Rittener, which will be described in connection with the analysis of carbonated soda liquors.

7. *Arsenic*.—Reich's method, modified by M'Cay:—Decompose 0·5 g. pyrites with concentrated nitric acid in a porcelain crucible, remove the free acid by evaporation, but not to complete dryness, add 4 g. sodium carbonate, heat on the sand-bath until the mass is quite dry, add 4 g. potassium nitrate, and heat until the mass

has fused quietly for ten minutes. After cooling, wash it with hot water, acidulate the filtered solution with a little nitric acid, heat for some time till all CO_2 is expelled, add silver nitrate, and neutralise carefully with dilute ammonia. The precipitate formed contains all the arsenic as Ag_3AsO_4 . Dissolve it in dilute nitric acid, and either estimate the silver volumetrically by ammonium thiocyanate (Volhard's method), or evaporate the solution in a porcelain dish, dry, and weigh the residue. One part $\text{Ag}_3\text{AsO}_4 = 0.1621 \text{ As}$, or 1 part $\text{Ag} = 0.2316 \text{ As}$.

D.—Burnt Pyrites (Cinders).

1. *Sulphur*.—Mix exactly 2 g. sodium bicarbonate of known alkalimetric value, in a nickel crucible of 20 or 30 c.c. capacity, intimately with 3.200 g. of ground cinders, by means of a glass rod flattened at the end. Heat the crucible with a small gas-flame, the point of which reaches just to the bottom of the crucible, for ten minutes. Stir the mass up again, heat it for fifteen minutes with a stronger flame, but not to the fusing point. During the heating the crucible should be covered, and no stirring should take place during this time, to prevent the escaping CO_2 from carrying away any dust. Empty the contents of the crucible into a porcelain dish, wash it out with water, add a concentrated solution of sodium chloride, free from magnesium chloride and perfectly neutral (without this addition it is difficult to avoid some ferric oxide passing through the filter later on), boil for ten minutes, filter, wash the insoluble residue till there is no alkaline reaction, allow the filtrate, etc., to cool down, and titrate it with methyl orange and normal hydrochloric acid (1 c.c. = 0.05305 Na_2CO_3 , indicating 0.01603 S). If we call the number of c.c. of the acid required by 2 g. bicarbonate = a , and the c.c. of acid used for titrating = b , the percentage of sulphur in the cinders corresponds to $\frac{a-b}{2}$.

2. *Copper* is estimated as in fresh pyrites (p. 111), but the solution of 1 g. of the sample is effected by hydrochloric acid with only a few drops of nitric acid, and no deduction for Bi and Sb is made from the electrolytically estimated Cu.

3. *Iron*.—Dissolve 0.5 cinders in concentrated hydrochloric acid by prolonged heating; reduce the boiling solution by zinc, free from iron, or more conveniently by stannous chloride, the excess of the latter being removed by a little mercuric chloride solution; pour the solution thus obtained into a half-litre of water, to which about 2 g. manganous sulphate has been added, and which has been just reddened by one or two drops of potassium permanganate. Determine the iron by titrating with decinormal potassium permanganate, each c.c. of which indicates 0.00559 g., or in 0.5 g. cinders 1.118 per cent. Fe.

E.—Zinc Blende.

1. *Total Sulphur*.—Decompose 0.5 of the finely ground sample with pure fuming nitric acid, cooling the beaker until the first violent reaction is over, and add hydrochloric acid, drop by drop, gently heating, until the decomposition is finished. Remove the iron by precipitation with ammonia, as in the case of pyrites (p. 112), and precipitate the sulphate by adding the requisite quantity of a dilute hot solution of barium chloride, all at once, in which case the BaSO_4 remaining in solution is just compensated by the BaCl_2 carried down with the precipitate (compare p. 111).

2. *Zinc*.—The following modification of Schaffner's method is now employed at the Rhenish and Belgian zinc works, as communicated to the author by Messrs Hassreidter and Prost:—Treat 2.5 g. of the finely ground blende (dried at 100°C .) in a 250 c.c. Erlenmeyer flask with 12 c.c. fuming nitric acid, first without heating, then heating gently until no more red vapours come off. Add 20 to 25 c.c. concentrated hydrochloric acid, evaporate to dryness on a sand-bath, dissolve in 5 c.c. hydrochloric acid and a little water, heat for some time, add 50 or 60 c.c. water, and heat to 60 or 70°C . until everything except gangue and sulphur has passed into solution. Pass a moderate current of H_2S into the solution, and gradually add, with continuous stirring, 50 to 100 c.c. water, until all Pb and Cd have been precipitated. This will be recognised by the fact that the bubbles of gas evolved are transparent. Any excessive dilution or too much prolonged treatment with H_2S must be avoided. Filter and wash with 100 c.c. sulphuretted hydrogen water, to which 5 c.c. hydrochloric acid has been added, until a drop of the filtrate gives no reaction for zinc with ammonium sulphide. Boil the filtrate and washings (together about 300 c.c.) in order to expel the H_2S (test with lead paper), and oxidise the ferrous salt by adding 5 c.c. concentrated nitric acid and 10 c.c. hydrochloric acid. When partially cooled down, put the solution into a half-litre flask, add 100 c.c. liquor ammoniæ (specific gravity 0.9 to 0.91) and 10 c.c. of a cold saturated solution of ammonium carbonate, shake well and allow to cool. This solution we call A.

In the meantime an ammoniacal zinc solution of known strength, the "titre," is prepared by dissolving a quantity of chemically pure zinc, approximately equal to that contained in the ore, in another half-litre flask, in 5 c.c. nitric acid + 20 c.c. hydrochloric acid, adding 250 c.c. water, 100 c.c. liquor ammoniæ, and 10 c.c. of ammonium carbonate solution, shaking up and allowing to stand till cool. (If manganese be present, add 10 c.c. hydrogen peroxide before adding the liquor ammoniæ.) This solution we call B. When all is cool, fill both flasks up to the mark, and filter the solution A (made from the ore) through a dry pleated filter. For the titration itself take from each of the solutions A

and B 100 c.c., run this into stout glass cylinders ("battery glasses") and dilute each with 200 c.c. water. The titration is effected with a concentrated solution of commercial crystallised sodium sulphide, diluted with ten or twenty times its volume of water and indicating per c.c. 0.005 to 0.010 g. Zn. This solution is placed in two 50 c.c. burettes, standing side by side, and is run by turns into the zinc solutions A and B. At first 2 or 3 c.c. less than is ultimately required is run in. Agitate the solutions and place at the same time a drop of each, by means of a thin glass rod, on to a strip of sensitive lead paper. After the action has lasted fifteen or twenty seconds, blow away the drops by means of a small wash-bottle and continue the addition of Na_2S , until both drops, after acting for the same time, produce a slight but distinct brownish colour of the same intensity. If too much liquid has been used in these drop tests, the titration must be repeated once or twice; at all events, the final reaction must take place equally in both glasses, and the readings must be accurate to 0.05 c.c.

If we call the quantity of pure zinc weighed out as "titre" a , that of the c.c. sodium sulphide solution used for the "titre" b , and the c.c. used for 100 c.c. of the ore solution ($=0.5$ g. ore) c , the expression $\frac{40 ac}{b}$ gives the percentage of zinc in the ore.

For exact estimations, a quantity of ferric chloride, equal to the content of iron in the ore, is added to the "titre," in order to meet the objection that the ferric hydroxide may carry down a little zinc.

Some blendes, containing a large proportion of silicates, obstinately resist the ordinary methods of testing (Jensch, *Zsch. f. angew. Chem.*, 1894, p. 155).

3. *Lead*.—The sulphides precipitated in No. 2 are, if necessary, digested with a concentrated solution of sodium sulphide; then dilute, filter, wash the residue, dissolve it (together with the filter) in dilute nitric acid, filter, add an excess of sulphuric acid, evaporate to dryness, and weigh the lead as sulphate. One part $\text{PbSO}_4 = 0.6829$ Pb.

4. *Lime and Magnesia* are estimated, because they form sulphates in the roasting process. Digest 2 to 5 g. blende with 50 c.c. dilute sulphuric acid (1:10), with application of heat, decant the clear portion; repeat this treatment once or twice, wash the residue, expel the H_2S from the filtrates by boiling, oxidise with bromine water, precipitate with ammonium carbonate, and in the filtrate precipitate first the calcium by ammonium oxalate (weigh this as CaO after strongly igniting), and in the filtrate from this the magnesium by ammonium phosphate (compare pp. 146 and 147).

5. *Arsenic* is estimated as described on p. 112.

6. *Carbon Dioxide* may be estimated as in pyrites, p. 112. This

is of interest, even when CaO and MgO are estimated, since blende contains sometimes ferrous and zinc carbonate.

7. *Available Sulphur*.—From the total sulphur found in No. 1 (p. 114) deduct :

For each part of Pb found in No. 3, 0·1550 part.					
“	“	CaO	“	“	4, 0·5715 “
“	“	MgO	“	“	4, 0·7944 “

The remainder indicates the sulphur available for the manufacture of sulphuric acid. The S of BaSO₄, etc., remains in the residue from the dissolving process.

F.—Cinders from Blende.

1. *Sulphur* (according to Lunge and Stierlin, *Zsch. f. angew. Chem.*, 1906, p. 26).—The process is carried out as described for pyrites cinders on p. 113, but 2 g. ground potassium chlorate is added to the mixture. The bottom of the crucible should finally be at a red heat, but the contents should merely frit together, not fuse entirely. The crucible must be covered during the heating, and its contents must not be stirred up. The calculation is as on p. 113—that is, the percentage of S = $\frac{a-b}{2}$.

An addition of potassium chlorate is already required in the case of cinders from iron pyrites containing much zinc. In case the cinders contain upwards of 6 per cent. S, the mixture should be : 1·603 g. cinders, 2·000 NaHCO₃, 4·0 KClO₃, 2–3 ferric oxide (free from S). The percentage of sulphur is then = $a-b$, where a is the c.c. of normal acid corresponding to the 2·000 bicarbonate, b the c.c. of acid required for titration after the heating.

This process is also applicable to fresh (unroasted) blende, by using the following mixture : 0·3206 g. blende, 2·000 NaHCO₃, 2 KClO₃, 2 Fe₂O₃ ; percentage of S = 5 ($a-b$).

A crude test is made by the foreman at the works, in this manner : he heats a sample of the cinders with 10 c.c. hydrochloric acid (1 : 2 water) in a flask, holding in its neck a strip of paper soaked in a neutral or faintly alkaline solution of lead acetate, and he judges of the more or less complete state of roasting by the depth of the brown colour developed on the paper.

2. *Zinc*, as on p. 112.

G.—Gases.

1. *Burner Gases*.—(a) SO₂ is estimated by Reich's method. The gas is aspirated through a solution of iodine, contained in a wide-necked 200 c.c. bottle, and coloured blue by starch solution, till the colour is just discharged. This bottle is connected with a larger bottle, fitted as an aspirator by having a tap near the

bottom, or by a siphon with a pinchcock. Water is run from this into a graduated 250 c.c. jar. The iodine bottle is shaken up during the aspirating, and at the moment when the colour is discharged, the tap of the aspirator is closed and the volume of water in the jar is read off. It is equal to the volume of the water run out, increased by that of the SO_2 absorbed. The absorbing bottle is charged with 10 c.c. of a decinormal solution of iodine (12.697 g. iodine per litre, preparation and valuation in the Appendix), along with about 50 c.c. of water, a little starch solution, and a little sodium bicarbonate. The above quantity of iodine is = 0.032 g. SO_2 = 10.93 c.c. at 0°C . and a pressure of 760 mm. The latter figure, multiplied by 100 and divided by 10.93 c.c. + the volume of the water run out, yields the percentage of SO_2 in the gas by volume.

This calculation is saved by the following table, in which the 10.93 c.c. are taken into account.

c.c. Water in the Measuring Jar.	Per cent. SO_2 by Volume.	c.c. Water in the Measuring Jar.	Per cent. SO_2 by Volume.
80.1	12.0	125.7	8.0
84.1	11.5	134.8	7.5
88.4	11.0	145.2	7.0
93.2	10.5	157.2	6.5
98.4	10.0	171.2	6.0
104.1	9.5	187.8	5.5
110.5	9.0	207.8	5.0
117.7	8.5		

In this no notice is taken of temperature and barometer. If these are to be observed, the volume read off is reduced to 0° and 760 mm. by the Tables 20 and 21, and then looked up in the above table.

(b) Since Reich's test takes no account of the SO_3 always present in burner gases, it is preferable to estimate the *total acids* ($\text{SO}_2 + \text{SO}_3$), either along with the test (a) or exclusively. This is performed in the same apparatus, but the absorbing-bottle is preferably provided with a gas entrance tube, closed at the bottom and perforated by numerous pin-holes, through which the gas issues in small bubbles. The gas is passed through a solution of decinormal sodium hydroxide, coloured by phenolphthalein, until the colour is just discharged. The calculation is made as for pure SO_2 , employing the table given in (a) (Lunge, *Zsch. f. angew. Chem.*, 1890, p. 563).

In both cases—(a) and (b)—an error is sometimes caused by arsenious oxide collecting in the aspirating tube; this is avoided by filtering the gases through asbestos.

2. *Chamber Gases.*—These are analysed like No. 3.

3. *Chamber Exit Gases.*—(a) *Oxygen*—Before estimating this, the acids are removed from the gas by washing with a solution of potassium or sodium hydroxide. Single samples can be taken at

odd times during the day, but it is recommended to take an average sample for the whole day, by aspirating at least 10 or 20 litres of gas, and analysing a portion of this. The estimation of oxygen is best made by moist phosphorus in an Orsat apparatus (p. 97) with two absorbing tubes, one of which is filled with potassium hydroxide solution for removing the acids, the other with small pieces of phosphorus. The manipulation is exactly as in testing flue gases, but it should be observed that the temperature must be at least 16° , better 18° C., otherwise the tube must be warmed a little.

(b) *Sulphur and Nitrogen Acids.*—The different acid compounds of sulphur and nitrogen are estimated together, whatever their degree of oxidation. The following methods agree in the main with those published by the British Alkali Makers' Association in 1878, but are improved in some analytical details. A continuous test over twenty-four hours is taken of the gases escaping from the exit pipes of the Gay-Lussac towers, aspirating at least one cubic foot per hour by means of any aspirator acting at a constant rate and recording the volume of gas = V by means of gauging the aspirator or by a gas meter. The volume V is reduced to 0° C. and 760 mm. pressure (= 32° F. and 29.92 inches *) by the Tables 20 and 21, and is called V^1 . In order to allow comparisons, the number of cubic feet of chamber space per pound of sulphur burnt and passing into the chambers is recorded, excluding towers, but including tunnels, the amount of sulphur being taken by the weekly average, each firm to state the distance of the testing hole from the point at which the gases leave the Gay-Lussac towers. The absorption apparatus consists of four bottles or tubes, containing not less than 100 c.c. of absorbing liquid each, with a depth of at least 3 in. in each bottle, the aperture of inlet tubes not to exceed $\frac{1}{50}$ in. in diameter, and to be measured by a standard wire. The first three bottles each contain 100 c.c. of normal caustic soda solution (31.05 g. per litre), the fourth 100 c.c. distilled water. The caustic soda used must be free from nitrogen acids. The gases are tested (1) for total acidity, stated in grains of SO_3 per cubic foot of gas, or in grams per cubic metre; (2) sulphur acids; (3) nitrogen acids, both stated in grains of S and N per cubic foot (or grams per cubic metre). The analysis is carried out as follows:—The contents of the four bottles are united, taking care not to unnecessarily augment the bulk of the liquids, and are divided into three equal parts, one of which is reserved for accidents, etc. The first part is titrated with normal sulphuric acid (49.04 g. SO_4H_2 per litre), to ascertain total acidity. The number of cubic centimetres of acid necessary

* The law prescribes the cubic feet to be measured at 60° F. and 80 inches, which necessitates the use of other tables or factors than those mentioned in the text, but the difference is hardly perceptible, and certainly within the limits of experimental error.

for neutralisation is called x . The second part of the liquid is gradually poured into a warm solution of potassium permanganate, strongly acidified with pure sulphuric acid. A small excess of permanganate must be present, and must be afterwards reduced by the addition of a few drops of sulphurous acid solution, until only a faint red tint is visible. Now all nitrogen acids are present as HNO_3 , but no excess of SO_2 . The HNO_3 is estimated by its action on FeSO_4 . Twenty-five c.c. of a solution, containing per litre 100 g. crystallised ferrous sulphate and 100 c.c. pure sulphuric acid (the same solution which is used for estimating MnO_2 , p. 154) are put into a flask, 20 c.c. to 25 c.c. pure concentrated sulphuric acid is added, the mixture is allowed to cool, and the other mixture, treated with permanganate, etc., is added. The flask is closed by a cork with glass tubes. A current of CO_2 passes through and issues beneath the surface of some water, to prevent entrance of air. First, all the air is expelled in this way by means of an apparatus giving a constant current of CO_2 ; then the solutions are introduced, and the contents of the flask are heated to boiling, till the dark colour produced by the formation of NO has changed to a clear light yellow. This takes from a quarter of an hour to one hour, according to the quantity of NO_2H present and that of the sulphuric acid added. The unoxidised ferrous sulphate is titrated by a seminormal permanganate solution (yielding 0.004 g. oxygen per cubic centimetre—compare Appendix). The cubic centimetres used = y . Since the titre of the iron solution changes somewhat quickly, it should be tested daily by taking out 25 c.c. with the same pipette as is used for the above operation, and ascertaining the amount of permanganate required for oxidising it = z c.c. The data required are found by the following equations:—

1. Total Acidity in grams per cubic metre =

$$\text{SO}_3 = \frac{0.120(100 - x)}{\sqrt{V}}$$

2. Sulphur in grams per cubic metre =

$$= \frac{0.008(600 - 6x - z + y)}{\sqrt{V}}$$

3. Nitrogen in grams per cubic metre =

$$\text{N} = \frac{0.007(z - y)}{\sqrt{V}}$$

1. Total Acidity in grains per cubic foot =

$$\text{SO}_3 = \frac{1.852(100 - x)}{\sqrt{V}}$$

2. Sulphur in grains per cubic foot =

$$\text{S} = \frac{0.12346(600 - 6x - z + y)}{\sqrt{V}}$$

3. Nitrogen in grains per cubic foot =

$$\text{N} = \frac{0.10803(z - y)}{\sqrt{V}}$$

The legal limit for total acidity in the lead-chamber process is 4 grains of SO_3 per cubic foot, before admixture with air, smoke or other gases; for the contact process, the "best practicable means" are to be adopted.*

* Alkali Act, 1906.

For the purposes of the Alkali Act, it is sufficient, in lieu of the above process, to estimate *total acidity* only by the test described on p. 118, employing decinormal soda solution and phenolphthalein.

(c) *Nitric Oxide* (NO) may be present in the exit gases after passing through the absorbing bottles. If it is to be estimated, an absorption tube (Fig. 8)* is interposed between the tubes of the apparatus described above and the aspirator. This tube con-

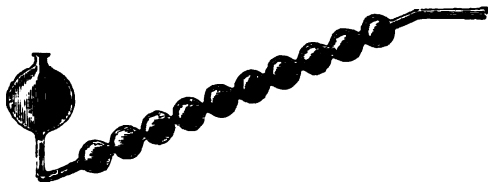


FIG. 8.

tains 30 c.c. of seminormal permanganate and 1 c.c. of sulphuric acid, specific gravity 1.25. The gas is passed through for twenty-four hours, and the tube then emptied and washed out. Now add 50 c.c. ferrous sulphate solution, corresponding to 2 z permanganate (compare last paragraph), and retitrate the decolorised liquid with permanganate. The quantity of the latter now used is called *u*. The NO has consumed $(30 + u - 2z)$ c.c. permanganate, which is equal—

In grams of nitrogen per cubic metre of the volume V_1 .

$$N = \frac{0.007(30 + u - 2z)}{3V_1}$$

In grains of nitrogen per cubic foot.

$$N = \frac{0.10803(30 + u - 2z)}{3V_1}$$

H.—Sulphuric Acid.

1. *Specific Gravity*.—The specific gravity tables of sulphuric acid refer of course to *chemically pure* acid. Since, in the case of high-grade acids, the impurities always present in commercial acids quite sensibly increase the specific gravity, the table in the case of acids over 90 per cent. H_2SO_4 should only be employed for the private use of the works, but *sales should always be effected on the basis of a real analysis*, as described later on under No. 8, p. 136.

The following table is based on that which the author formerly worked out from a series of very careful investigations, carried on with Isler and Naef; some corrections introduced by the Imperial German Standards Commission are incorporated.

It should be noted that the highest percentages show lower specific gravities than those just below, the maximum being at 99.35 per cent. H_2SO_4 .

* This shape of bulb-tubes has been found to be far superior to any other form of absorption-tubes tried.

1. SPECIFIC GRAVITY OF SULPHURIC ACID
AT 60° F.

Specific Gravity.	Degrees Twaddell.	100 parts by weight contain		Kilo per litre. H ₂ SO ₄ .	1 Cubic Foot of Acid 60° F.	
		SO ₃ .	H ₂ SO ₄ .		Weighs lbs. avoird.	Contains lbs. avoird. H ₂ SO ₄ .
1·200	40	22·30	27·32	0·328	74·82	20·44
1·205	41	22·82	27·95	0·337	75·14	21·00
1·210	42	23·33	28·58	0·346	75·45	21·57
1·215	43	23·84	29·21	0·355	75·76	22·14
1·220	44	24·36	29·84	0·364	76·07	22·71
1·225	45	24·88	30·48	0·373	76·38	23·28
1·230	46	25·39	31·11	0·382	76·69	23·85
1·235	47	25·88	31·70	0·391	77·00	24·41
1·240	48	26·35	32·28	0·400	77·32	24·97
1·245	49	26·83	32·86	0·409	77·63	25·54
1·250	50	27·29	33·43	0·418	77·94	26·10
1·255	51	27·76	34·00	0·426	78·25	26·66
1·260	52	28·22	34·57	0·435	78·56	27·23
1·265	53	28·69	35·14	0·444	78·87	27·79
1·270	54	29·15	35·71	0·454	79·19	28·35
1·275	55	29·62	36·29	0·462	79·50	28·92
1·280	56	30·10	36·87	0·472	79·81	29·48
1·285	57	30·57	37·45	0·481	80·12	30·04
1·290	58	31·04	38·03	0·490	80·43	30·60
1·295	59	31·52	38·61	0·500	80·74	31·17
1·300	60	31·99	39·19	0·510	81·06	31·74
1·305	61	32·46	39·77	0·519	81·37	32·32
1·310	62	32·94	40·35	0·529	81·68	32·89
1·315	63	33·41	40·93	0·538	81·99	33·46
1·320	64	33·88	41·50	0·548	82·30	34·03
1·325	65	34·35	42·08	0·557	82·62	34·60
1·330	66	34·80	42·66	0·567	82·93	35·18
1·335	67	35·27	43·20	0·577	83·24	35·79
1·340	68	35·71	43·74	0·586	83·55	36·40
1·345	69	36·14	44·28	0·596	83·86	37·01
1·350	70	36·58	44·82	0·605	84·17	37·63

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SPECIFIC GRAVITY OF SULPHURIC ACID—Continued.

Specific Gravity.	Degrees Twaddell.	100 parts by weight contain		Kilo per litre. H ₂ SO ₄ .	1 Cubic Foot of Acid 60° F.	
		SO ₃ .	H ₂ SO ₄ .		Weighs lbs. avoird.	Contains lbs. avoird. H ₂ SO ₄ .
1·355	71	37·02	45·35	0·614	84·49	38·24
1·360	72	37·45	45·88	0·624	84·80	38·85
1·365	73	37·89	46·41	0·633	85·11	39·46
1·370	74	38·32	46·94	0·643	85·42	40·07
1·375	75	38·75	47·47	0·653	85·73	40·68
1·380	76	39·18	48·00	0·662	86·04	41·29
1·385	77	39·62	48·53	0·672	86·36	41·91
1·390	78	40·05	49·06	0·682	86·67	42·52
1·395	79	40·48	49·59	0·692	86·98	43·13
1·400	80	40·91	50·11	0·702	87·29	43·74
1·405	81	41·33	50·63	0·711	87·60	44·36
1·410	82	41·76	51·15	0·721	87·92	44·97
1·415	83	42·17	51·66	0·730	88·23	45·58
1·420	84	42·57	52·15	0·740	88·54	46·18
1·425	85	42·96	52·63	0·750	88·85	46·78
1·430	86	43·36	53·11	0·759	89·16	47·38
1·435	87	43·75	53·59	0·769	89·47	47·99
1·440	88	44·14	54·07	0·779	89·79	48·59
1·445	89	44·53	54·55	0·789	90·10	49·19
1·450	90	44·92	55·03	0·798	90·41	49·79
1·455	91	45·31	55·50	0·808	90·72	50·39
1·460	92	45·69	55·97	0·817	91·03	50·99
1·465	93	46·07	56·43	0·827	91·35	51·59
1·470	94	46·45	56·90	0·837	91·66	52·19
1·475	95	46·83	57·37	0·846	91·97	52·79
1·480	96	47·21	57·83	0·856	92·28	53·39
1·485	97	47·57	58·28	0·866	92·59	54·00
1·490	98	47·95	58·74	0·876	92·90	54·60
1·495	99	48·34	59·22	0·886	93·22	55·20
1·500	100	48·73	59·70	0·896	93·53	55·84
1·505	101	49·12	60·18	0·906	93·84	56·47
1·510	102	49·51	60·65	0·916	94·15	57·10

SPECIFIC GRAVITY OF SULPHURIC ACID—*Continued.*

Specific Gravity.	Degrees Twaddell.	100 parts by weight contain		Kilo per litre. H ₂ SO ₄ .	1 Cubic Foot of Acid 60° F.	
		SO ₃ .	H ₂ SO ₄ .		Weighs lbs. avoird.	Contains lbs. avoird. H ₂ SO ₄ .
1·515	103	49·89	61·12	0·926	94·46	57·73
1·520	104	50·28	61·59	0·936	94·77	58·36
1·525	105	50·66	62·06	0·946	95·09	59·00
1·530	106	51·04	62·53	0·957	95·40	59·62
1·535	107	51·43	63·00	0·967	95·71	60·26
1·540	108	51·78	63·43	0·977	96·02	60·89
1·545	109	52·12	63·85	0·987	96·33	61·52
1·550	110	52·46	64·26	0·996	96·65	62·15
1·555	111	52·79	64·67	1·006	96·96	62·78
1·560	112	53·22	65·20	1·017	97·27	63·49
1·565	113	53·59	65·65	1·027	97·58	64·10
1·570	114	53·95	66·09	1·038	97·89	64·79
1·575	115	54·32	66·53	1·048	98·20	65·42
1·580	116	54·65	66·95	1·058	98·52	66·04
1·585	117	55·03	67·40	1·068	98·83	66·67
1·590	118	55·37	67·83	1·078	99·14	67·77
1·595	119	55·73	68·26	1·089	99·45	67·96
1·600	120	56·09	68·70	1·099	99·76	68·60
1·605	121	56·44	69·13	1·110	100·07	69·29
1·610	122	56·79	69·56	1·120	100·39	69·92
1·615	123	57·15	70·00	1·131	100·70	70·60
1·620	124	57·49	70·42	1·141	101·01	71·20
1·625	125	57·84	70·85	1·151	101·32	71·85
1·630	126	58·18	71·27	1·162	101·64	72·54
1·635	127	58·53	71·70	1·172	101·95	73·16
1·640	128	58·88	72·12	1·182	102·26	73·79
1·645	129	59·22	72·55	1·193	102·57	74·47
1·650	130	59·57	72·96	1·204	102·88	75·16
1·655	131	59·92	73·40	1·215	103·19	75·84
1·660	132	60·26	73·81	1·225	103·50	76·47
1·665	133	60·60	74·24	1·236	103·82	77·16

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SPECIFIC GRAVITY OF SULPHURIC ACID—Continued.

Specific Gravity.	Degrees Twaddell.	100 parts by weight contain		Kilo per litre. H ₂ SO ₄ .	1 Cubic Foot of Acid 60° F.	
		SO ₃ .	H ₂ SO ₄ .		Weights lbs. avoird.	Contains lbs. avoird. H ₂ SO ₄ .
1·670	134	60·95	74·66	1·246	104·13	77·78
1·675	135	61·29	75·08	1·259	104·44	78·59
1·680	136	61·63	75·50	1·268	104·75	79·16
1·685	137	61·98	75·86	1·278	105·07	80·12
1·690	138	62·29	76·30	1·289	105·38	80·81
1·695	139	62·64	76·73	1·301	105·69	81·51
1·700	140	63·00	77·17	1·312	106·00	82·21
1·705	141	63·35	77·60	1·323	106·31	82·90
1·710	142	63·70	78·04	1·334	106·62	83·60
1·715	143	64·07	78·48	1·346	106·94	84·29
1·720	144	64·43	78·92	1·357	107·25	84·99
1·725	145	64·78	79·36	1·369	107·56	85·69
1·730	146	65·14	79·80	1·381	107·87	86·38
1·735	147	65·50	80·24	1·392	108·18	87·08
1·740	148	65·86	80·68	1·404	108·49	87·77
1·745	149	66·22	81·12	1·416	108·80	88·47
1·750	150	66·58	81·56	1·427	109·12	89·17
1·755	151	66·94	82·00	1·439	109·43	89·86
1·760	152	67·30	82·44	1·451	109·74	90·56
1·765	153	67·76	83·01	1·465	110·05	91·45
1·770	154	68·17	83·41	1·478	110·36	92·26
1·775	155	68·60	84·02	1·491	110·68	93·07
1·780	156	68·98	84·50	1·504	110·99	93·81
1·785	157	69·47	85·10	1·519	111·30	94·74
1·790	158	69·96	85·70	1·534	111·61	95·67
1·795	159	70·45	86·30	1·549	111·92	96·60
1·800	160	70·96	86·92	1·565	112·23	97·69
1·805	161	71·50	87·60	1·581	112·67	98·69
1·810	162	72·08	88·30	1·598	112·98	99·75
1·815	163	72·69	89·05	1·621	113·29	101·19

SPECIFIC GRAVITY OF SULPHURIC ACID—Continued.

Specific Gravity.	Degrees Twaddell.	100 parts by weight contain		Kilo per litre. H ₂ SO ₄ .	1 Cubic Foot of Acid 60° F.	
		SO ₃ .	H ₂ SO ₄ .		Weighs lbs. avoird.	Contains lbs. avoird. H ₂ SO ₄ .
1·820	164	73·51	90·05	1·689	113·61	102·31
1·821	...	73·63	90·20	1·643	113·67	102·56
1·822	...	73·80	90·40	1·647	113·73	102·89
1·823	...	73·96	90·60	1·651	113·80	103·06
1·824	...	74·12	90·80	1·656	113·85	103·38
1·825	165	74·29	91·00	1·661	113·92	103·68
1·826	...	74·49	91·25	1·666	113·99	104·00
1·827	...	74·69	91·50	1·671	114·04	104·31
1·828	...	74·86	91·70	1·676	114·11	104·62
1·829	...	75·03	91·90	1·681	114·19	104·93
1·830	166	75·19	92·10	1·685	114·23	105·18
1·831	...	75·46	92·43	1·692	114·30	105·62
1·832	...	75·69	92·70	1·698	114·36	105·99
1·833	...	75·89	92·97	1·704	114·42	106·38
1·834	...	76·12	93·25	1·710	114·47	106·74
1·835	167	76·35	93·56	1·717	114·54	107·43
1·836	...	76·57	93·80	1·722	114·61	107·49
1·837	...	76·90	94·20	1·730	114·67	107·99
1·838	...	77·23	94·60	1·739	114·73	108·55
1·839	...	77·55	95·00	1·748	114·80	109·12
1·840	168	78·04	95·60	1·759	114·86	109·80
1·8405	...	78·33	95·95	1·765	114·89	110·18
1·8410	...	78·69	96·30	1·784	114·92	110·73
1·8415	...	79·47	97·35	1·792	114·95	111·86
1·8410	...	80·16	98·20	1·808	114·92	112·86
1·8405	...	80·43	98·52	1·814	114·89	113·23
1·8400	...	80·59	98·72	1·816	114·86	113·36
1·8395	...	80·63	98·77	1·817	114·83	113·48
1·8390	...	80·93	99·12	1·823	114·80	113·80
1·8385	...	81·08	99·31	1·826	114·76	113·98

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2. TABLE FOR REDUCING THE SPECIFIC GRAVITIES OF SULPHURIC ACID OF VARIOUS STRENGTHS TO ANY OTHER TEMPERATURE (DEGREES C.).

0°.	5°.	10°.	15°.	20°.	25°.	30°.	35°.	40°.	45°.	50°.
1·857	1·852	1·846	1·840	1·835	1·830	1·825	1·821	1·816	1·811	1·806
1·847	1·841	1·836	1·830	1·825	1·820	1·815	1·810	1·805	1·800	1·795
1·837	1·831	1·825	1·820	1·815	1·809	1·804	1·799	1·794	1·789	1·784
1·827	1·821	1·815	1·810	1·805	1·799	1·793	1·788	1·783	1·778	1·773
1·817	1·811	1·806	1·800	1·794	1·788	1·783	1·777	1·772	1·766	1·761
1·807	1·801	1·796	1·790	1·784	1·778	1·773	1·767	1·762	1·756	1·751
1·797	1·791	1·786	1·780	1·774	1·768	1·763	1·757	1·752	1·746	1·741
1·786	1·781	1·776	1·770	1·765	1·759	1·754	1·748	1·743	1·737	1·732
1·776	1·770	1·765	1·760	1·755	1·749	1·744	1·738	1·733	1·728	1·723
1·765	1·760	1·755	1·750	1·745	1·740	1·735	1·730	1·725	1·720	1·715
1·754	1·750	1·745	1·740	1·735	1·730	1·726	1·721	1·716	1·711	1·706
1·744	1·740	1·735	1·730	1·725	1·720	1·716	1·711	1·706	1·701	1·696
1·734	1·730	1·725	1·720	1·715	1·710	1·706	1·701	1·696	1·691	1·686
1·724	1·720	1·715	1·710	1·705	1·700	1·696	1·691	1·686	1·681	1·676
1·714	1·710	1·705	1·700	1·695	1·690	1·686	1·681	1·676	1·671	1·667
1·704	1·700	1·695	1·690	1·685	1·680	1·676	1·671	1·666	1·661	1·656
1·694	1·690	1·685	1·680	1·675	1·670	1·666	1·661	1·656	1·651	1·646
1·684	1·680	1·675	1·670	1·665	1·660	1·656	1·651	1·646	1·641	1·637
1·674	1·670	1·665	1·660	1·655	1·650	1·646	1·641	1·636	1·632	1·628
1·664	1·660	1·655	1·650	1·645	1·640	1·636	1·632	1·627	1·622	1·618
1·654	1·650	1·645	1·640	1·635	1·631	1·626	1·622	1·617	1·612	1·608
1·644	1·640	1·635	1·630	1·625	1·621	1·616	1·612	1·607	1·602	1·598
1·634	1·630	1·625	1·620	1·615	1·611	1·606	1·602	1·597	1·592	1·588
1·624	1·620	1·615	1·610	1·605	1·601	1·596	1·592	1·587	1·582	1·578
1·614	1·610	1·605	1·600	1·595	1·591	1·586	1·582	1·577	1·572	1·568
1·604	1·600	1·595	1·590	1·585	1·581	1·576	1·572	1·567	1·562	1·558
1·594	1·589	1·584	1·580	1·575	1·570	1·566	1·562	1·558	1·553	1·548
1·584	1·579	1·574	1·570	1·566	1·561	1·556	1·552	1·548	1·543	1·539
1·574	1·569	1·564	1·560	1·556	1·552	1·547	1·543	1·539	1·534	1·530
1·568	1·563	1·558	1·554	1·549	1·544	1·539	1·534	1·530	1·525	1·521
1·552	1·548	1·544	1·540	1·536	1·532	1·528	1·524	1·520	1·516	1·512
1·542	1·538	1·534	1·530	1·526	1·522	1·518	1·514	1·510	1·506	1·502
1·532	1·528	1·524	1·520	1·516	1·512	1·508	1·504	1·500	1·497	1·492
1·522	1·518	1·514	1·510	1·506	1·502	1·498	1·494	1·490	1·486	1·482
1·512	1·508	1·504	1·500	1·496	1·492	1·488	1·484	1·480	1·476	1·472
1·502	1·498	1·494	1·490	1·486	1·482	1·478	1·474	1·470	1·466	1·462
1·492	1·488	1·484	1·480	1·476	1·472	1·468	1·465	1·461	1·457	1·453
1·482	1·478	1·474	1·470	1·466	1·462	1·458	1·455	1·451	1·447	1·443
1·472	1·468	1·464	1·460	1·456	1·452	1·448	1·445	1·442	1·438	1·434
1·462	1·458	1·454	1·450	1·446	1·442	1·438	1·435	1·432	1·429	1·425
1·452	1·448	1·444	1·440	1·436	1·432	1·429	1·426	1·423	1·420	1·416
1·442	1·438	1·434	1·430	1·426	1·422	1·419	1·416	1·413	1·409	1·405
1·432	1·428	1·424	1·420	1·416	1·413	1·410	1·406	1·402	1·398	1·394
1·422	1·418	1·414	1·410	1·406	1·403	1·399	1·396	1·392	1·388	1·384
1·412	1·408	1·404	1·400	1·396	1·393	1·389	1·386	1·382	1·378	1·374
1·402	1·398	1·394	1·390	1·386	1·383	1·379	1·376	1·372	1·368	1·364
1·392	1·388	1·384	1·380	1·376	1·373	1·370	1·366	1·362	1·359	1·355
1·382	1·378	1·374	1·370	1·366	1·363	1·360	1·356	1·352	1·349	1·346
1·372	1·368	1·364	1·360	1·356	1·353	1·350	1·346	1·344	1·340	1·336
1·362	1·358	1·354	1·350	1·346	1·343	1·340	1·336	1·334	1·330	1·326

SULPHURIC ACID MANUFACTURE

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TABLE 2—Continued.

55°.	60°.	65°.	70°.	75°.	80°.	85°.	90°.	95°.	100°.
1·801	1·796	1·792	1·787	1·782	1·778	1·774	1·770	1·766	1·762
1·790	1·787	1·781	1·776	1·770	1·766	1·762	1·757	1·752	1·748
1·779	1·774	1·769	1·764	1·759	1·754	1·749	1·744	1·739	1·734
1·767	1·762	1·757	1·752	1·747	1·741	1·736	1·731	1·726	1·721
1·755	1·750	1·744	1·739	1·734	1·729	1·724	1·719	1·714	1·708
1·746	1·741	1·735	1·730	1·725	1·720	1·715	1·710	1·705	1·700
1·736	1·731	1·726	1·721	1·716	1·712	1·707	1·702	1·697	1·692
1·727	1·722	1·717	1·712	1·707	1·702	1·697	1·693	1·688	1·683
1·718	1·713	1·708	1·703	1·698	1·693	1·688	1·684	1·679	1·674
1·710	1·705	1·700	1·695	1·690	1·685	1·681	1·676	1·671	1·667
1·702	1·697	1·692	1·688	1·683	1·678	1·674	1·669	1·664	1·660
1·692	1·687	1·683	1·678	1·673	1·668	1·664	1·659	1·654	1·650
1·682	1·677	1·673	1·668	1·663	1·659	1·654	1·649	1·644	1·640
1·672	1·667	1·663	1·658	1·653	1·649	1·644	1·639	1·635	1·630
1·662	1·657	1·653	1·648	1·644	1·639	1·634	1·630	1·625	1·620
1·652	1·647	1·642	1·638	1·634	1·630	1·625	1·620	1·615	1·610
1·642	1·637	1·632	1·628	1·624	1·620	1·615	1·611	1·606	1·602
1·633	1·628	1·623	1·619	1·615	1·611	1·606	1·602	1·597	1·593
1·623	1·619	1·614	1·610	1·606	1·602	1·597	1·593	1·588	1·584
1·614	1·610	1·605	1·600	1·596	1·592	1·588	1·583	1·579	1·575
1·604	1·600	1·595	1·591	1·586	1·582	1·578	1·574	1·570	1·565
1·594	1·590	1·585	1·581	1·577	1·573	1·569	1·565	1·561	1·556
1·584	1·580	1·576	1·572	1·568	1·564	1·560	1·556	1·552	1·547
1·574	1·570	1·566	1·562	1·558	1·554	1·550	1·546	1·542	1·537
1·564	1·560	1·556	1·552	1·548	1·544	1·540	1·536	1·531	1·527
1·554	1·550	1·545	1·541	1·537	1·533	1·529	1·525	1·521	1·516
1·544	1·539	1·535	1·531	1·527	1·523	1·519	1·515	1·510	1·506
1·535	1·531	1·526	1·522	1·518	1·514	1·510	1·505	1·501	1·496
1·526	1·522	1·517	1·513	1·509	1·504	1·500	1·496	1·492	1·487
1·517	1·513	1·509	1·504	1·500	1·495	1·491	1·487	1·483	1·478
1·508	1·504	1·500	1·496	1·491	1·486	1·482	1·478	1·473	1·469
1·498	1·494	1·490	1·485	1·481	1·476	1·472	1·468	1·463	1·459
1·488	1·484	1·480	1·476	1·472	1·467	1·462	1·458	1·453	1·449
1·478	1·474	1·470	1·466	1·462	1·457	1·452	1·448	1·443	1·438
1·468	1·464	1·460	1·455	1·451	1·446	1·442	1·438	1·433	1·428
1·458	1·454	1·450	1·442	1·441	1·437	1·433	1·429	1·424	1·419
1·449	1·445	1·441	1·436	1·432	1·428	1·424	1·419	1·414	1·410
1·439	1·435	1·431	1·427	1·423	1·418	1·414	1·409	1·405	1·401
1·430	1·426	1·422	1·418	1·413	1·409	1·405	1·400	1·396	1·392
1·421	1·417	1·413	1·409	1·404	1·400	1·396	1·391	1·387	1·383
1·412	1·407	1·403	1·399	1·395	1·391	1·386	1·382	1·378	1·374
1·401	1·397	1·393	1·389	1·385	1·380	1·376	1·372	1·368	1·364
1·390	1·386	1·382	1·378	1·374	1·370	1·366	1·362	1·358	1·353
1·380	1·376	1·372	1·368	1·364	1·360	1·356	1·352	1·348	1·343
1·370	1·366	1·362	1·358	1·354	1·350	1·346	1·342	1·338	1·333
1·360	1·356	1·352	1·348
1·351	1·346	1·342	1·338
1·342	1·337	1·334	1·329
1·332	1·327	1·323	1·319
1·322	1·317	1·314	1·310

TABLE 2—Continued.

0°.	5°.	10°.	15°.	20°.	25°.	30°.	35°.	40°.	45°.	50°.
1·852	1·848	1·844	1·840	1·836	1·833	1·830	1·827	1·824	1·820	1·816
1·841	1·837	1·833	1·830	1·827	1·824	1·821	1·818	1·814	1·810	1·806
1·830	1·826	1·823	1·820	1·817	1·814	1·811	1·808	1·804	1·801	1·297
1·820	1·816	1·813	1·810	1·807	1·804	1·801	1·298	1·294	1·291	1·287
1·810	1·806	1·803	1·800	1·297	1·294	1·291	1·288	1·284	1·281	1·277
1·800	1·296	1·293	1·290	1·287	1·284	1·280	1·277	1·274	1·270	1·267
1·290	1·286	1·283	1·280	1·277	1·274	1·270	1·267	1·264	1·260	1·256
1·280	1·276	1·273	1·270	1·267	1·264	1·260	1·257	1·254	1·250	1·246
1·270	1·266	1·263	1·260	1·257	1·254	1·251	1·248	1·245	1·241	1·237
1·260	1·256	1·253	1·250	1·247	1·244	1·241	1·238	1·235	1·231	1·227
1·250	1·246	1·243	1·240	1·237	1·234	1·230	1·227	1·224	1·220	1·217
1·240	1·236	1·233	1·230	1·227	1·224	1·220	1·217	1·214	1·210	1·207
1·230	1·226	1·223	1·220	1·217	1·214	1·210	1·207	1·204	1·200	1·197
1·220	1·216	1·213	1·210	1·206	1·204	1·200	1·197	1·194	1·190	1·187
1·210	1·206	1·203	1·200	1·196	1·193	1·190	1·186	1·183	1·180	1·176
1·200	1·196	1·193	1·190	1·186	1·183	1·180	1·176	1·173	1·169	1·165
1·190	1·186	1·183	1·180	1·176	1·173	1·170	1·166	1·163	1·159	1·155
1·180	1·176	1·173	1·170	1·166	1·163	1·160	1·156	1·153	1·149	1·146
1·169	1·166	1·163	1·160	1·157	1·153	1·150	1·147	1·144	1·141	1·138
1·159	1·156	1·153	1·150	1·147	1·143	1·140	1·137	1·134	1·131	1·128
1·149	1·146	1·143	1·140	1·137	1·134	1·131	1·128	1·125	1·122	1·119
1·138	1·135	1·133	1·130	1·127	1·125	1·122	1·119	1·116	1·113	1·110
1·128	1·125	1·123	1·120	1·118	1·115	1·112	1·110	1·107	1·104	1·102
1·118	1·115	1·113	1·110	1·108	1·105	1·102	1·100	1·097	1·094	1·092
1·108	1·105	1·103	1·100	1·097	1·094	1·092	1·090	1·087	1·084	1·082
1·098	1·095	1·093	1·090	1·087	1·084	1·082	1·080	1·077	1·074	1·072
1·088	1·085	1·083	1·080	1·077	1·074	1·072	1·070	1·067	1·064	1·062
1·078	1·075	1·073	1·070	1·067	1·064	1·062	1·060	1·057	1·054	1·052
1·068	1·065	1·063	1·060	1·057	1·054	1·052	1·050	1·048	1·044	1·042
1·058	1·055	1·053	1·050	1·047	1·044	1·042	1·040	1·038	1·034	1·032
1·048	1·045	1·043	1·040	1·037	1·034	1·032	1·030	1·028	1·024	1·022
1·038	1·035	1·033	1·030	1·027	1·024	1·022	1·020	1·018	1·014	1·012
1·028	1·025	1·023	1·020	1·017	1·014	1·012	1·010	1·008	1·004	1·002
1·018	1·015	1·013	1·010	1·007	1·004	1·002	1·000	0·998	0·994	0·992

TABLE 2—Continued.

55°.	60°.	65°.	70°.	75°.	80°.	85°.	90°.	95°.	100°.
1·812	1·908	1·804	1·800
1·802	1·298	1·294	1·290
1·298	1·289	1·284	1·280
1·288	1·279	1·274	1·270
1·278	1·269	1·265	1·260
1·268	1·259	1·255	1·250
1·252	1·248	1·244	1·240
1·242	1·238	1·234	1·230
1·238	1·224	1·224	1·220
1·228	1·214	1·214	1·210
1·210	1·209	1·204	1·200
1·204	1·200	1·196	1·190
1·194	1·190	1·185	1·180
1·188	1·179	1·175	1·170
1·172	1·168	1·164	1·160
1·162	1·158	1·154	1·150
1·152	1·148	1·144	1·140
1·148	1·139	1·135	1·131
1·135	1·131	1·127	1·123
1·125	1·122	1·118	1·114
1·116	1·113	1·109	1·106
1·107	1·104	1·100	1·097
1·099	1·096	1·092	1·088
1·089	1·086	1·082	1·078
1·079	1·075	1·072	1·068
1·069	1·065	1·062	1·058
1·069	1·065	1·062	1·048
1·049	1·045	1·042	1·038
1·036	1·035	1·032	1·028
1·039	1·025	1·022	1·018
1·019	1·015	1·012	1·008
1·009	1·005	1·002	0·998
0·999	0·995	0·992	0·988
0·989	0·985	0·982	0·978

**3. SPECIFIC GRAVITIES OF COMMERCIAL (NORDHAUSEN)
OIL OF VITRIOL.**

(Messel, *Journ. Soc. Chem. Ind.*, 1885, p. 573.)

Specimens.	Percentage of SO ₂ .	Specific Gravity	
		At 80° F. = 26·6° C.	At 60° F. = 15·5° C.
...	8·3	1·842	1·852
Liquid	30·0	1·930	1·940
Crystalline mass, resembling nitre .	40·0	1·956	1·970
Do. do.	44·5	1·961	1·975
Do. do.	46·2	1·963	1·977
...	59·4	1·980	1·994
Liquid	60·8	1·992	2·006
Do.	65·0	1·992	2·006
Do.	69·4	2·002	2·016
Crystallised	72·8	1·984	1·988
Do.	80·0	1·959	1·973
Do.	82·0	1·953	1·967

4. SPECIFIC GRAVITIES AND PERCENTAGE OF FUMING (NORDHAUSEN) OIL OF VITRIOL AT DIFFERENT TEMPERATURES.

Density at					SO ₃ Per Cent.
15°.	20°.	25°.	30°.	35°.	
1·8417	1·8371	1·8323	1·8287	1·8240	76·67
1·8427	1·8378	1·8333	1·8295	1·8249	77·49
1·8428	1·8388	1·8351	1·8302	1·8255	78·34
1·8437	1·8390	1·8346	1·8300	1·8257	79·04
1·8427	1·8386	1·8351	1·8297	1·8250	79·99
1·8420	1·8372	1·8326	1·8281	1·8234	80·46
1·8398	1·8350	1·8305	1·8263	1·8218	80·94
1·8446	1·8400	1·8353	1·8307	1·8262	81·37
1·8509	1·8466	1·8418	1·8371	1·8324	81·91
1·8571	1·8522	1·8476	1·8432	1·8385	82·17
1·8697	1·8647	1·8595	1·8545	1·8498	82·94
1·8790	1·8742	1·8687	1·8640	1·8592	83·25
1·8875	1·8823	1·8767	1·8713	1·8661	83·84
1·8942	1·8888	1·8833	1·8775	1·8722	84·12
1·8990	1·8940	1·8890	1·8830	1·8772	84·33
1·9034	1·8984	1·8930	1·8874	1·8820	84·67
1·9072	1·9021	1·8950	1·8900	1·8845	84·82
1·9095	1·9042	1·8986	1·8932	1·8866	84·99
1·9121	1·9063	1·8993	1·8948	1·8892	85·14
1·9250	1·9193	1·9135	1·9082	1·9023	85·54
1·9290	1·9236	1·9183	1·9129	1·9073	85·68
1·9368	1·9310	1·9250	1·9187	1·9122	85·88
1·9447	1·9392	1·9334	1·9279	1·9222	86·51
1·9520	1·9465	1·9402	1·9338	1·9278	86·72
1·9584	1·9528	1·9466	1·9406	1·9340	87·03
1·9632	1·9573	1·9518	1·9457	1·9398	87·46
cryst.	cryst.	1·9740	1·9666	1·9740	88·00

The above table is only intended for control in works, but not for commercial purposes, because the specific gravity is anything but a certain guide for the percentage of Nordhausen acid, and altogether fails as such, for strengths just below the monohydrate. The table was not made for chemically pure acids, but for commercial acid.

5. FREEZING AND MELTING POINTS OF SULPHURIC ACID.*

Specific Gravity at 15°.	Freezing Point.	Melting Point.
1·671	Liquid at -20°	...
1·691	Liquid at -20°	...
1·712	Liquid at -20°	...
1·727	-7·5°	-7·5°
1·732	-8·5°	-8·5°
1·749	-0·2°	+4·5°
1·767	+1·6°	+6·5°
1·778	+8·5°	+8·5°
1·790	+4·5°	+8·0°
1·807	-9·0°	-6·0°
1·822	Liquid at -20°	...
1·840	Liquid at -20°	...

* Lunge, *Berichte d. deutsch. chem. Ges.*, 1881, s. 2649.

6. BOILING POINTS OF SULPHURIC ACID.

(Lunge, *Ber. d. d. chem. Ges.*, 11, 370.)

Per Cent. SO ₄ H ₂ .	Specific Gravity.	Boiling Point.	Per Cent. SO ₄ H ₂ .	Specific Gravity.	Boiling Point.	Per Cent. SO ₄ H ₂ .	Specific Gravity.	Boiling Point.
		Degrees.			Degrees.			Degrees.
5	1·031	101	56	1·459	133	82	1·758	218·5
10	1·069	102	60	1·503	141·5	84	1·773	227
15	1·107	103·5	62·5	1·530	147	86	1·791	238·5
20	1·147	105	65	1·557	153·5	88	1·807	251·5
25	1·184	106·5	67·5	1·585	161	90	1·818	262·5
30	1·224	108	70	1·615	170	91	1·824	268
35	1·265	100	72	1·639	174·5	92	1·830	274·5
40	1·307	114	74	1·661	180·5	93	1·834	281·5
45	1·352	118·5	76	1·688	189	94	1·837	288·5
50	1·399	124	78	1·710	199	95	1·840	295
53	1·428	128·5	80	1·733	207			

Monohydrate (100 per cent.) boils at 338° (Marignac).

7. FUSING POINTS* OF SULPHURIC ACID AND OF
NORDHAUSEN OIL OF VITRIOL. (KNIETSCH.)

Sulphuric Acid.				Nordhausen Oil of Vitriol.	
Percentage of SO ₃ (as H ₂ SO ₄).	Fusing Point. °C.	Percentage of SO ₃ (as H ₂ SO ₄).	Fusing Point. °C.	Percentage of free SO ₃ .	Fusing Point. °C.
Per cent.		Per cent.		Per cent.	
1 SO ₃	- 0·6	69 SO ₃	+ 7·0	0 SO ₃	+ 10·0
2 "	- 1·0	70 "	+ 4·0	5 "	+ 3·5
3 "	- 1·7	71 "	- 1·0	10 "	- 4·8
4 "	- 2·0	72 "	- 2·0	15 "	- 11·2
5 "	- 2·7	73 "	- 16·2	20 "	- 11·0
6 "	- 3·6	74 "	- 25·0	25 "	- 0·6
7 "	- 4·4	75 "	- 34·0	30 "	+ 15·2
8 "	- 5·3	76 }	- 32·0	35 "	+ 26·0
9 "	- 6·0	77 }	- 33·0	40 "	+ 33·8
10 "	- 6·7	78 }	- 16·5	45 "	+ 34·8
11 "	- 7·2	79 "	- 5·2	50 "	+ 28·5
12 "	- 7·9	80 "	+ 3·0	55 "	+ 18·4
13 "	- 8·2	81 "	+ 7·0	60 "	+ 0·7
14 "	- 9·0	82 "	+ 8·2	65 "	+ 0·8
15 "	- 9·3	83 "	- 0·8	70 "	+ 9·0
16 "	- 9·8	84 "	- 9·2	75 "	+ 17·2
17 "	- 11·4	85 "	- 11·0	80 "	+ 22·0
18 "	- 13·2	86 "	- 2·2	85 "	+ 33·0 (27) †
19 "	- 15·2	87 "	+ 13·5	90 "	+ 34·0 (25)
20 "	- 17·1	88 "	+ 26·0	95 "	+ 36·0 (26)
21 "	- 22·5	89 "	+ 34·2	100 "	+ 40·0 (15)
22 "	- 31·0	90 "	+ 34·2		
23 "	- 40·1	91 "	+ 25·8		
... "	} below	92 "	+ 14·2		
... "		93 "	+ 0·8		
61 "	- 40·0	94 "	+ 4·5		
62 "	- 20·0	95 "	+ 14·8		
63 } 60°	- 11·5	96 "	+ 20·3		
64 } Bé	- 4·8	97 "	+ 29·2		
65 "	- 4·2	98 "	+ 33·8		
66 "	+ 1·2	99 "	+ 36·0		
67 } 62°	+ 8·0	100 "	+ 40·0		
68 } Bé	+ 8·0				

* "Fusing Point" is understood to be the temperature to which the mercury of the thermometer, dipping into the solidifying liquid, rises and at which it remains constant. It should be noticed that large quantities of Nordhausen oil of vitriol, such as exist in transportation vessels, frequently do not behave in accord with the above data, because during the carriage and storage a separation often takes place in the acid, crystals of a different concentration being formed, which of course possess a correspondingly different fusing point.

† The figures in parentheses signify the fusing points of freshly made Nordhausen oil of vitriol, which has not polymerised.

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8. PERCENTAGE OF SO₃ IN NORDHAUSEN OIL OF VITRIOL.

Found by Titrating.	Contains per cent.		Found by Titrating.	Contains per cent.		Found by Titrating.	Contains per cent.	
	SO ₃ .	SO ₄ H ₂ .		SO ₃ .	SO ₄ H ₂ .		SO ₃ .	SO ₄ H ₂ .
81-6326	100	0	87-8775	66	34	93-9387	33	67
81-8163	99	1	88-0612	65	35	94-1224	32	68
82-0000	98	2	88-2448	64	36	94-3061	31	69
82-1836	97	3	88-4285	63	37	94-4897	30	70
82-3674	96	4	88-6122	62	38	94-6734	29	71
82-5510	95	5	88-7959	61	39	94-8571	28	72
82-7346	94	6	88-9795	60	40	95-0408	27	73
82-9183	93	7	89-1632	59	41	95-2244	26	74
83-1020	92	8	89-3469	58	42	95-4081	25	...
83-2857	91	9	89-5306	57	43	95-5918	24	...
83-4693	90	10	89-7142	56	44	95-7755	23	...
83-6530	89	11	89-8979	55	45	95-9591	22	...
83-8367	88	12	90-0816	54	46	96-1428	21	...
84-0204	87	13	90-2653	53	47	96-3265	20	...
84-2040	86	14	90-4489	52	48	96-5102	19	...
84-3877	85	15	90-6326	51	49	96-6938	18	...
84-5714	84	16	90-8163	50	50	96-8775	17	...
84-7551	83	17	91-0000	49	51	97-0612	16	...
84-9387	82	18	91-1836	48	52	97-2448	15	...
85-1224	81	19	91-3673	47	53	97-4285	14	...
85-3061	80	20	91-5510	46	54	97-6122	13	...
85-4897	79	21	91-7346	45	55	97-7959	12	...
85-6734	78	22	91-9183	44	56	97-9795	11	...
85-8571	77	23	92-1020	43	57	98-1632	10	...
86-0408	76	24	92-2857	42	58	98-3469	9	...
86-2244	75	25	92-4693	41	59	98-5306	8	...
86-4081	74	26	92-6530	40	60	98-7142	7	...
86-5918	73	27	92-8367	39	61	98-8979	6	...
86-7755	72	28	93-0204	38	62	99-0816	5	...
86-9591	71	29	93-2040	37	63	99-2653	4	...
87-1428	70	30	93-3877	36	64	99-4489	3	...
87-3265	69	31	93-5714	35	65	99-6326	2	...
87-5102	68	32	93-7551	34	66	99-8163	1	...
87-6938	67	33						

9. The Quantitative Examination of Free Sulphuric Acid.

The quantitative examination of free sulphuric acid is made by titrating a weighed quantity. It is not sufficiently accurate to measure the acid by a pipette, etc., especially in the case of concentrated acid. The titration is performed by means of standard sodium hydroxide solution, and the results are expressed in terms of H_2SO_4 .

Weigh from 2 to 3 g. acid in a glass-tap pipette (Fig. 11, p. 144), after cleaning the latter on the outside; run its contents into at least 100 c.c. water, and weigh the pipette again, *without* washing it out. This enables another pipette full of acid to be taken and tested, without washing and drying the instrument, and so forth. The same procedure is also very well adapted for slightly fuming mixtures of sulphuric and nitric acid, and for Nordhausen oil of vitriol (*cf.* p. 144).

The standard sodium hydroxide solution is "normal," *i.e.*, containing 0.04005 NaOH g. per litre. It is controlled by means of standard hydrochloric acid (0.03646 g. HCl per litre), the strength of which has been fixed by pure sodium carbonate. The method is described in detail in the Appendix.

As indicator, methyl orange is used always in the cold, and so much only is taken that the colour produced is just visible. Nitrous acid destroys this colouring matter, but ordinary commercial acid never contains sufficient to cause any trouble, and even "nitrous vitriol" or fuming nitric acid can be titrated with methyl orange, if the indicator is added (or renewed) shortly before the last quantity of alkali has been added; or else an excess of alkali is added, then methyl orange, and titrated back. Nitrous acid behaves towards methyl orange like the strong mineral acids; that is, the change of colour takes place when the compound $NaNO_2$ has been formed.

10. Examination of Sulphuric Acid for other Substances.

(a) *Nitrous Acid* (Nitrososulphuric Acid) is titrated with seminormal permanganate. (Preparation in the Appendix.) This can be done without loss of NO as follows (Lunge, *Berliner Berichte*, x., 1075):—Put the nitrous vitriol into a burette fitted with a glass tap, and run it slowly into a measured quantity of permanganate, diluted with five times its volume of tepid water (30° C. to 40° C.), and agitate continuously till the colour just vanishes. Sometimes during this process a little manganese dioxide is separated, which makes it difficult to recognise the end of the reaction, but this is avoided by keeping the temperature

not above 40° and by diluting the permanganate, say to 200 c.c. (The same method holds good for the analysis of *sodium nitrite*, but in this case the permanganate solution must be previously acidulated to such an extent that the NaNO_2 solution is immediately decomposed when run into the permanganate.) Each cubic centimetre of the permanganate indicates 0.009502 g. N_2O_3 , hence more or less of it is employed, according as to whether an acid containing more or less N_2O_3 is titrated. For chamber acid, employ at most 5 c.c.; for good Gay-Lussac acid, up to 50 c.c. of permanganate. If the quantity of permanganate is called x , and that of the vitriol consumed for decolorising it y , the quantity of N_2O_3 present in grams per litre of acid is:—

$$\begin{array}{l} \text{Calculated as} \\ \text{as} \end{array} \quad \begin{array}{l} \text{NO}_2\text{H} = \frac{9 \cdot 502x}{y} \\ \text{NaNO}_3 = \frac{15 \cdot 75x}{y} \\ \text{NaNO}_3 = \frac{21 \cdot 258x}{y} \end{array}$$

The following table, p. 137, saves the calculation for all cases in which $x=50$. The column y gives the number of cubic centimetres of nitrous vitriol used, a the percentage in grams per litre, and b the percentage by weight, for acid of 140° Tw. (For other strengths the percentage by weight is calculated by dividing the figures of column a by $10 \times$ specific gravity.)

(b) *Total Nitrogen Acids*.—These are contained in sulphuric acid as N_2O_3 , or more correctly as nitrososulphuric acid, $\text{SO}_2(\text{OH})(\text{ONO})$, and NO_3H . NO can be present only in minute quantity, and only in absence of NO_3H . N_2O_4 is decomposed by sulphuric acid into nitrososulphuric and nitric acid. The estimation made according to (a) only indicates N_2O_3 . The total nitrogen acids are converted into NO by shaking up the nitrous vitriol with mercury; the quantity of NO formed is estimated by volume (Crum's reaction). This is done by Lunge's *nitrometer*. Fill the graduated limb a with mercury by raising the level tube b ; put the three-way cock so that it communicates with any of the openings; run the nitrous vitriol into the top cup of a from a 1 c.c. pipette graduated in $\frac{1}{15}$ c.c., employing only 0.5 c.c. of very strong, but up to 5 c.c. of very weak nitrous vitriol; lower the level tube, open the cock carefully so that the vitriol runs in without any air entering; pour 2 or 3 c.c. of pure strong sulphuric acid, free from nitrogen compounds, into the cup; let this acid enter the nitrometer, and repeat the washing of the cup with 1 or 2 c.c. of pure acid. Start the evolution of gas by taking the tube a out of the clamp, inclining it several times till almost horizontal, and suddenly righting it again, so that mercury and acid are well

mixed ; shake for one or two minutes till no more gas is evolved. Place the tubes so that the mercury in *b* is as much higher than that in *a* as is required for balancing the acid in *a* ; this requires

TABLE FOR ESTIMATING NITROUS VITRIOL.

Employ 50 c.c. of seminormal permanganate. The results are expressed as NO_2H and NO_2Na . The column *y* refers to acid of 140°Tw. as unit :—

Acid consumed. <i>y</i> . c.c.	NO_2H .		NO_2Na .		Acid consumed. <i>y</i> . c.c.	NO_2H .		NO_2Na .	
	<i>a</i> . g. per litre.	<i>b</i> . per cent.	<i>a</i> . g. per litre.	<i>b</i> . per cent.		<i>a</i> . g. per litre.	<i>b</i> . per cent.	<i>a</i> . g. per litre.	<i>b</i> . per cent.
10	78.75	4.61	106.29	6.22	36	21.88	1.28	29.58	1.73
11	71.59	4.19	96.63	5.65	37	21.28	1.24	28.72	1.68
12	65.63	3.84	88.58	5.18	38	20.72	1.21	27.97	1.64
13	60.58	3.54	81.76	4.78	39	20.19	1.18	27.25	1.59
14	56.25	3.29	75.92	4.44	40	19.69	1.15	26.53	1.55
15	52.50	3.07	70.86	4.14	41	19.21	1.12	25.83	1.51
16	49.22	2.88	66.43	3.88	42	18.75	1.10	25.31	1.48
17	46.32	2.71	62.52	3.65	43	18.27	1.07	24.66	1.44
18	43.75	2.56	59.05	3.45	44	17.90	1.05	24.16	1.41
19	41.45	2.42	55.95	3.27	45	17.76	1.02	23.57	1.38
20	39.38	2.30	53.15	3.11	46	17.12	1.00	23.11	1.35
21	37.50	2.19	50.61	2.96	47	16.72	0.978	22.57	1.32
22	35.80	2.09	48.32	2.83	48	16.41	0.960	22.15	1.30
23	34.24	2.00	46.21	2.70	49	16.04	0.938	21.65	1.27
24	32.81	1.92	44.28	2.59	50	15.75	0.921	21.26	1.24
25	31.50	1.84	42.52	2.49	55	14.32	0.837	19.33	1.13
26	30.29	1.77	40.88	2.39	60	13.13	0.768	17.72	1.04
27	29.17	1.71	39.37	2.30	65	12.12	0.709	16.36	0.957
28	28.13	1.65	37.97	2.22	70	11.25	0.658	15.18	0.888
29	27.16	1.59	36.66	2.14	75	10.50	0.614	14.17	0.829
30	26.25	1.54	35.43	2.07	80	9.85	0.576	13.29	0.777
31	25.40	1.49	34.28	2.00	85	9.26	0.542	12.50	0.731
32	24.61	1.44	33.22	1.94	90	8.73	0.511	11.78	0.689
33	23.86	1.40	32.20	1.88	95	8.29	0.485	11.19	0.654
34	23.16	1.35	31.26	1.83	100	7.88	0.461	10.64	0.622
35	22.50	1.32	30.37	1.78					

N.B.—The figures in column *a* also indicate 0.01 lb. avoirdupois per gallon, or nearly ounces per cubic foot.

1 mm. of Hg for $6\frac{1}{2}$ mm. of acid. An exact reading can only be obtained when the gas has attained the temperature of the room and all froth has subsided. Read off the volume of the gas, also

a thermometer hung up close by, and the barometer. In order to check the levelling, open the cock, when the level of *a* should not change. If it rises, the pressure has been in excess, and the reading must be increased a little, say by 0.1 c.c. If it sinks, the reverse is the case, *i.e.*, always in the opposite sense to the change of level. Another plan is, to put a little acid into the cup before opening the cock. This will be sucked in if the pressure was too low, or raised if too high. With adroit manipulation the reading can then soon be corrected. Finally, lower the graduated tube *a*, lest any air should enter on opening the tap; open the tap, raise the tube *b*, force the gas and all acid into the cup, and turn the tap so that the acid flows through into a vessel held below; the last portions are drawn off by blotting-paper. The nitrometer is then ready for the next experiment.

A test must always be made to see whether the glass tap is gas-tight. It will hardly remain so without greasing it occasionally with vaseline, but this ought to be done very slightly, so as to avoid any grease getting into the bore, for if the grease comes in contact with acid, troublesome froth is formed.*

c.c. NO read off.	a. Absolute weight mg.	b. Per cent. by weight, when employing 1 c.c. acid of 140° Tw. in the Nitrometer.
Nitrogen, N ₂	0.6257	0.0866
Nitric oxide, NO	1.3402	0.0784
Nitrogen trioxide, N ₂ O ₃	1.6975	0.0993
Nitric acid, real, HNO ₃	2.8144	0.1646
Sodium nitrate, NaNO ₃	3.7986	0.2221
Potassium nitrate, KNO ₃	4.5176	0.2642

(Multiples of these figures are given in Table 5, p. 17.)

This process is interfered with by the presence of sulphurous acid, the best test for which is the smell. To remove it, the acid is stirred up with a very small quantity of powdered potassium permanganate. Any great excess of this acid makes the process very troublesome and inaccurate.

In highly concentrated acids a notable quantity (up to 3 per cent. by volume) of NO may be dissolved; therefore a little water must be added to such acids in the nitrometer, sufficient to reduce

* Such froth may also be formed in the presence of too much water, by the separation of mercuric sulphate, but this hardly ever happens in the case of nitrous vitriol, and even in the analysis of sodium nitrate only when the description given for the estimation is not properly adhered to.

their strength to about 90 per cent. H_2SO_4 . The volume of NO read off is reduced to $0^\circ C.$ and 760 mm. ($32^\circ F.$ and 29.92 in.) by means of the tables, pages 38 and 44 or 50, and calculated for the nitrogen compounds present by the table on p. 138, in which column *a* gives milligrams, *b* per cent. by weight, when employing 1 c.c. acid of $140^\circ Tw.$

Nitrometers (and gas-volumeters) should of course be obtained from a reliable dealer, so that the correctness of the graduations and the tightness of the taps can be depended upon.

The reduction to 0° and 760 mm. can be effected without thermometer and barometer, and without the use of any tables, by means of Lunge's *Gas-volumeter*, Fig. 9, which serves also for numerous other analytical operations. It consists of the gas-measuring tube A, the reduction tube B, and the level tube C, all connected by thick rubber tubing with the three-way tube *a*.

B and C are held in two arms of the same clamp, so as to be each either individually movable in its own arm, or both together by means of the common clamp. Tube A may be an ordinary nitrometer with three-way tap and funnel; it is, however, best employed merely as a gas-measuring tube, and for some purposes this tube is made to hold upwards of 100 c.c., in which case the upper portion is in the shape of a bulb, the division beginning below this, say, at 90 or 100 c.c. The most convenient shape, which serves both for small and large quantities of gas, is a tube possessing a bulb in the middle, and graduated above this from 0 (at the tap) to 40 c.c., below the bulb from 100 to 140 c.c. A two-way tap, *g*, allows communication either with the straight outlet tube *h*, or with the right-angle tube *e*.

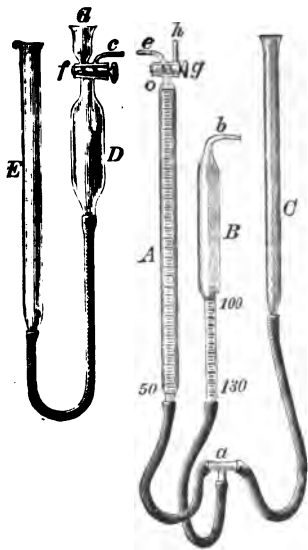


FIG. 9.

Instead of carrying out the decomposition in tube A, it is decidedly preferable to employ for this purpose a separate tube, D, provided with a two-way tap, *f*, a funnel, *d*, and an exit tube, *c*, corresponding to the tube *e* on A. D has its own level tube E. All these tubes are held in clamps, which can be moved up and down on the two bars of a heavy iron stand.

The "reduction tube" B is enlarged at the top, and the narrow

portion below is graduated from 100 to 125 c.c. in $\frac{1}{10}$ c.c. It contains a volume of dry air which at 0° and 760 mm. pressure would occupy exactly 100 c.c. This is obtained by taking, once for all, a reading of the thermometer and the barometer, and calculating what would be the volume of 100 c.c. of dry air under the prevailing atmospheric conditions. In reading the barometer, a deduction must be made for the expansion of the mercury, viz., 1 mm. between 0° and 12°, 2 mm. between 13° and 19°, 3 mm. between 20° and 25°. For calculating the volume of 100 c.c. air at "normal conditions" from the observed temperature t and the barometric reading b (corrected as above), we have the formula :—

$$V = \frac{100(273+t)760}{273b}$$

A drop of concentrated sulphuric acid is previously introduced through the open end of b , most conveniently by suction. After setting the level in B to the point indicated by the equation, the capillary end of b is sealed by fusing it up; in order to prevent the heat from expanding the air in B, a cardboard shield is put between the flame and B.

This is avoided by replacing the open capillary tube b by Lunge's "beaker-tap" (*Ber.*, 1892, p. 3157), and still better by Göckel's gas-tap with annular mercury seal (supplied by Dr Göckel, Wilhelmstrasse, 49, Berlin, W.).

The "laboratory vessel" or "decomposition tube" D, in which the reaction is carried out, is provided with the fittings of an ordinary nitrometer, viz., the three-way tap f , the cup d , the lateral outlet c , and the special level tube E. It holds about 150 c.c., and is not graduated. Mercury is poured in through E. By raising E, the vessel D is completely filled with mercury, till it begins to run out at c . The tap f is shut, the end of c closed by a glass or rubber cap, and the nitrous vitriol placed in d ; this is sucked into D, then some pure acid sucked in, to wash the cup and tap, tap f closed (no bubbles of air must remain below it!), and the decomposition brought about in the usual manner by shaking the vitriol with the mercury, to evolve all the nitrogen acids as NO. The tubes D and A are then brought opposite to each other (A having been previously filled, by raising C, with mercury till it flows out at e); c and e are joined by a short piece of rubber tubing till they touch, so that no air remains in the space between; C is lowered, E raised, and by cautiously opening tap f , the NO contained in D is transferred into A. As soon as all the gas is in A, and the acid following it has filled the narrow tube e , tap g is closed. Now tube C is raised till the mercury in B has risen to the mark 100, and B and C are simultaneously moved up or down, as may be required, till the levels in A and B coincide, that in B being still at 100 c.c. Since the air in B is

now compressed to the point which it would occupy in the dry state at 0° and 760 mm., and the gas in A is placed under exactly the same pressure (the temperature of these two parallel tubes being presumably the same), the reading in A gives the volume of NO reduced to the same conditions of 0° and 760 mm. The temperature in A and B must be exactly the same; this is ensured by the conductivity of the mercury, but in the case of large quantities of NO it is necessary to wait at least ten minutes before finally adjusting the levels.

If only one gas-volumeter is available, and that is adjusted for moist gases (as is required for other purposes), it may be used also for dry gases, but it is then necessary to avoid any sulphuric acid passing from D into A, and to suck a drop of water into A, before transferring the gas into it from D. Another way for measuring dry gases with a moist reduction tube is as follows: observe the temperature; take the tension of aqueous vapour corresponding to this from the table, p. 54= f , and adjust the mercury in the measuring tube A higher by f mm. than in the reduction tube B, where, as usual, the mercury is adjusted by means of the level tube C to the point marking 100.00 c.c. If, on the other hand, a reduction tube has been prepared for dry gases, by introducing a drop of concentrated acid, it may be used also for moist gases (as in the testing of manganese ore, bleaching powder, potassium permanganate, etc.), by adjusting the mercury in A f mm. lower than in B.

(c) *Relative Proportions of the three Nitrogen Acids.*—In order to find from the result of the permanganate titration and from the estimation of total nitrogen in the nitrometer (as NO) the relative proportions of N_2O_3 , N_2O_4 , and NO_2H in a mixture of all three nitrogen acids absorbed by sulphuric acid, we may employ the following formula:—

a = c.c. NO found in the nitrometer.

b = c.c. O, calculated from the permanganate titration.

(1 c.c. O = 1.4278 mg.; 1 c.c. seminormal permanganate = 0.004 g. = 2.8015 c.c. oxygen.)

x = vols. NO, corresponding to the N_2O_3 present.

y = „ NO, „ „ N_2O_4 „

z = „ NO, „ „ NO_2H „

If $4b$ be $> a$,

$$x = 4b - a; \quad y = 2(a - 2b), \quad \text{or} \quad = a - x.$$

If $4b$ be $< a$,

$$y = 4b; \quad z = a - 4b.$$

(d) *Qualitative Test for Traces of Nitrogen Acids.*—These can be detected by means of diphenylamine. Dissolve a few grams

of diphenylamine in 100 parts of pure sulphuric acid. This should be completely free from nitrogen oxides, and can be made so, if not at hand, by boiling with a trace of ammonium sulphate. Dilute the acid with $\frac{1}{2}$ th volume of water before dissolving the diphenylamine. This solution may be employed at once, or kept, as it keeps quite well. Pour about 2 c.c. of the vitriol to be tested into a test-tube, and add about 1 c.c. of the diphenylamine solution so that the layers mix only gradually. In the case of dilute acids, or other lighter liquids, proceed in the opposite manner. The slightest traces of nitrogen acids are proved by the appearance of a brilliant blue colour at the area of contact of the liquids.

The smallest traces of nitrous acid are detected, even in the presence of nitric acid, by the reagent proposed by Griess, as modified by Hovsøy and by Lunge. This reagent is prepared by (1) dissolving 0.5 g. sulphanilic acid in 150 c.c. dilute acetic acid; (2) boiling 0.1 g. solid α -naphthylamine with 20 c.c. water, pouring the colourless liquid off from the purple residue, and mixing it with 150 c.c. dilute acetic acid. The two solutions are united, and can thus be kept for an indefinite time in a bottle, well protected against air (which often contains traces of nitrogen acids). Add a few c.c. of this solution to the solution to be tested, and heat to 70° or 80°. If as little as 1 part nitrous acid be present in 1000 million parts of the liquid, a red colour is formed in about one minute. More concentrated solutions of HNO_3 , say 1:1000, do not yield the blue colour, but a yellow solution.

In the presence of selenium the diphenylamine test fails, as Se gives the same reaction as nitrogen acids. In that case test for somewhat large quantities of nitrogen acids by the decoloration of indigo solution; for traces, by the reddening of a solution of brucine sulphate.

(e) *Selenium* in sulphuric acid can be recognised by adding to the acid a strong solution of ferrous sulphate, when a brownish-red precipitate will make its appearance, which cannot be confused with the colour produced by NO , or else by the green colour, produced in a solution of codein.

(f) *Examination for Lead*.—Dilute the acid, if concentrated, with an equal volume of water and twice its volume of alcohol. Allow the mixture to stand for some time, filter any precipitate of PbSO_4 , wash it with dilute alcohol, and dry and ignite in a porcelain crucible, burning the filter separately. 1 g. $\text{PbSO}_4 = 0.68293$ g. Pb.

(g) *Examination for Iron*.—Boil the acid, if free from nitrogen, with a drop of nitric acid to oxidise the iron. Dilute a little, allow to cool, and add solution of potassium thiocyanate. A red colour proves the presence of iron. If there is not too little, it can be quantitatively estimated in another sample by heating with pure zinc (free from iron), pouring off from the zinc, washing the latter, allowing to cool, and titrating with permanganate.

This is best employed as $\frac{1}{10}$ th normal, indicating 0.002795 g. Fe per cubic centimetre. Not less than 50 c.c. of the acid should be taken for this test, as it generally contains very little iron.

The smallest traces of iron can be estimated colorimetrically (Lunge, *Zsch. f. angew. Chem.*, 1896, p. 3).

(h) *Arsenic* is detected qualitatively by the well-known methods of Marsh or of Reinsch. For quantitative estimation dilute 20 c.c. of the acid with water, and treat with a current of SO_2 , until there is a strong smell of the gas. This reduces As_2O_5 to As_2O_3 , but that requires a pretty long time and a considerable excess of SO_2 . Now drive off the excess by heating and passing a current of CO_2 , neutralise exactly with Na_2CO_3 and a little NaHCO_3 , and titrate with decinormal iodine and starch. 1 c.c. of the iodine solution indicates 0.00495 g. As_2O_3 . (Any considerable proportion of iron should be previously removed.)

(i) *Chlorides*.—Boil 10 c.c. of the acid in a flask, pass the vapours on to the surface of a little water, contained in a flask, and estimate the absorbed HCl acidimetrically, or after neutralising with Na_2CO_3 , by titrating with decinormal silver nitrate (p. 145).

11. Analysis of Fuming Sulphuric Acid (Nordhausen Oil of Vitriol) and of Sulphuric Anhydride.

The substance is either weighed in glass bulbs or in a glass-tap tube. The former are very thin bulbs of about 2 cm. diameter, ending on each side in a capillary tube. Melt the acid, if solid, till it is completely homogeneous, and suck 3 g. to 5 g. into the bulb, which ought to be half-filled with it. The sucking is best done by means of a bottle closed with a rubber cork, through which passes a tightly fitting glass tap, connected at its free end with a rubber tube. Suction is applied to the latter, the tap closed, the rubber tube drawn over one of the capillary ends of the weighing bulb, and by opening the tap a sufficient quantity of acid admitted into the bulb. The tube is cleaned outside, and one of the capillary ends is sealed off. The other end can be left open without fear of any loss of SO_3 or attraction of moisture during weighing. The weighing is best done on a small platinum crucible with two nicks, on which the ends of the bulb can rest. If the latter should be accidentally broken, the acid runs into the crucible, not on the balance. Put the bulb, after weighing, open end downwards into a small Erlenmeyer flask, into the neck of

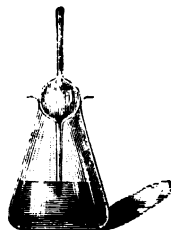


FIG. 10.

which it ought to fit exactly (Fig. 10), and which contains so much water that the capillary tube dips well into it, to prevent any loss of SO_2 on mixing the acid with water. Break off the other point, allow the acid to run out, squirt a few drops of water into the upper capillary, and ultimately rinse the whole bulb tube by repeated aspiration of water. Dilute the liquid to 500 c.c. and take 50 c.c. for each test. This is done with $\frac{1}{2}$ normal sodium carbonate solution (1 c.c. = 0.008006 g. SO_2), and methyl orange as indicator. From the acidity found, that due to SO_2 is deducted, which is ascertained by titrating another sample with iodine.



Fig. 11.

Lunge and Rey's glass-tap pipette (Fig. 11) (the taps of which must be tight without greasing!) is more convenient than the bulb tube. Shut the lower tap *c*, open the upper tap *a*, apply suction (with the mouth) at *d*, and shut *a* whilst sucking. Immerse the point *e* in the acid to be tested, and open *c*; the partial vacuum in bulb *b* suffices for drawing up enough acid, which must not be allowed to reach the tap *c*. Shut *c*, clean the point *e*, put the pipette in the outer glass vessel *f*, and weigh. Take the pipette out of *f*, place it point downwards in water, and slowly run out the contents. Then squirt some water from above into *b*, allow to stand for a moment, and rinse thoroughly with water.

The strongest fuming oil of vitriol cannot be run directly into water without loss. Such oil of vitriol is weighed out in small glass bulbs, as described above; both ends are sealed up, the bulb is placed in a bottle containing a considerable quantity of water, the stopper put in, the bulb broken by shaking the bottle, and after waiting a little the solution titrated.

Solid products of this class must be melted by moderate heating; they then remain long enough in the liquid state to complete the weighing and running out without being heated again. But products which are not far removed from real SO_3 in composition would give out too much vapour in this operation. Such products are weighed out in a stoppered bottle, and mixed in this with a known and exactly analysed quantity of monohydrate, at a temperature of 30° to 40° C. This ought to produce a mixture containing about 70 per cent. SO_3 which will remain liquid at ordinary temperatures.

If only 0.5 to 1 g. of acid has been weighed off, titrate directly.

This is more accurate than diluting and titrating only part of the liquid, but the latter method cannot be avoided when a larger quantity of acid has been weighed.

The acidimetric determination, of course, indicates the total percentage of acid. From this we must deduct in the first instance any SO_3 present. This is estimated in the usual way by decinormal iodine, and for each c.c. of this 0.05 c.c. normal sodium carbonate solution is deducted (since with methyl orange the colour changes when SO_2 has passed into NaHSO_3). If we call the c.c. of normal sodium carbonate used = n , those of decinormal iodine used for the same quantity of oil of vitriol = m , the acidity due to $\text{H}_2\text{SO}_4 + \text{SO}_3$ is = $(n - 0.05 m) 0.04003 \text{ SO}_3$. To the SO_3 thus found add the SO_2 (calculated = $0.003203 m$), and assume the residue to be water.* By multiplying this H_2O by 4.443, we obtain the quantity of SO_3 combined with it to form H_2SO_4 , and by deducting this from the total SO_3 acidity, that of the free SO_3 .

III. SALTCAKE AND HYDROCHLORIC ACID.

A.—Salt (Common Salt, Rock-Salt).

1. *Moisture*.—Ignite 5 g. of salt in a covered platinum crucible (to prevent loss by spirting); heat first quite gradually, then for some minutes, up to a low red heat. If the sample is too damp or if several samples are to be tested at the same time, weigh off the 5 g. samples in flat-bottomed Erlenmeyer flasks, with funnels on, heat a number of these on a sand-bath for three or four hours to 140° or 150° (without funnel), and allow them to cool with the funnel in, which saves the use of a desiccator. Afterwards the small remainder of chemically combined water may be removed by heating on a wire-gauze, but this is mostly unnecessary.

2. *Insoluble matter*.—Dissolve 5 g., filter the insoluble matter, wash, dry, and ignite.

3. *Chlorine*.—Weigh off 5.85 g. of the moist salt, dissolve it, and dilute to 500 c.c.; take out 25 c.c. by means of a pipette, add so much of a solution of neutral potassium chromate that the liquid is distinctly yellow, and titrate with decinormal silver solution (*cf.* Appendix). Add the silver solution from a 50 c.c. burette, till the precipitate, even after agitation, shows a distinct but faint pink colour. 0.2 c.c. is deducted from the number of cubic centimetres of silver solution used, as being required for producing the colour. The remainder, multiplied by 2, gives the

* In case any weighable quantity of solid impurities is present, this must be of course equally deducted.

percentage of NaCl in the salt. In lieu of potassium chromate, sodium arsenate may be employed as indicator. This is even more sensitive, and *no* deduction from the silver solution used should be made in this case.

4. *Lime*.—Dissolve 5 g. of the salt in water, if necessary with the aid of a little HCl. When analysing impure rock-salt the treatment with dilute HCl must be continued for some time, in order to dissolve all CaSO₄. It is also necessary to filter off any clay, etc., but non-argillaceous salt ought to dissolve completely, excepting any grains of sand and the like. In the clear solution precipitate the lime with ammonia and ammonium oxalate, allow to stand for twelve hours, filter the precipitate through a fine filter paper in a well-shaped funnel (*cf.* p. 110), wash, dry, and ignite it in a platinum crucible till it is completely converted into CaO. This is done by first gently heating till the calcium oxalate is decomposed, and then igniting at nearly a white heat for twenty minutes, either over a gas blow-pipe or, more conveniently, in a Hempel's gas-oven or over a Muencke burner. One part CaO is equal to 2.4271 CaSO₄, and is calculated as such.

5. *Sulphates*.—Dissolve 10 g. of the salt in tepid water, with addition of a little hydrochloric acid. Dilute to 1 litre, filter through a dry pleated filter, and precipitate 250 c.c. (=2.5 g. salt) by barium chloride (*cf.* p. 110). The sulphate is usually calculated as CaSO₄.

6. *Magnesium chloride* may be titrated directly by drying the salt, extracting it with absolute alcohol, filtering, evaporating off the alcohol from the filtrate (which contains nothing but MgCl₂), and titrating with silver nitrate.

B.—Saltcake (Sulphate of Soda).

(*N.B.*—Nos. 1 and 2 are sufficient for daily examinations of the produce of works; the others are employed for saltcake when bought and sold.)

1. *Free Acid*.—Dissolve 20 g. saltcake, dilute to 250 c.c., take out 50 c.c. with a pipette, add methyl orange, and titrate with standard sodium carbonate to the point of neutralisation. Each cubic centimetre of the standard alkali is equal to 1 per cent. SO₃. The total acidity is calculated as SO₃, including HCl and NaHSO₄. (If litmus were employed as indicator, the presence of salts of iron and alumina would cause trouble in the titration; with methyl orange this is not the case.)

2. *Sodium Chloride*.—Take another 50 c.c. of the solution made for the test No. 1, add the same quantity of standard alkali as used for this test, so that the acid is exactly neutralised, then a

little neutral potassium chromate, and titrate with decinormal silver solution, as in A, 3. Each cubic centimetre of silver solution (after deducting 0·2 from the whole) is equal to 0·146 per cent. NaCl. Or else employ a solution containing 2·905 g. AgNO₃ per litre and indicating 0·001 g. NaCl per cubic centimetre. This would, in the present case, indicate 0·025 per cent. NaCl per cubic centimetre.

3. *Iron*.—Dissolve 10 g. of sulphate in water, reduce the iron salts to the ferrous state by a little sulphuric acid and zinc, and titrate with potassium permanganate (*cf.* page 142).

4. Residue, insoluble in water, is estimated as usual, if present.

5. *Lime*.—Dissolve 10 g. in water, if necessary with a little HCl; add NH₄Cl and NH₃, precipitate with ammonium oxalate, ignite, and weigh as CaO (*cf.* A, 4). If any appreciable quantity of Fe₂O₃ has been found, this must be deducted.

6. *Magnesia* is precipitated in the filtrate from No. 5 by ammonium phosphate; allow to stand for twenty-four hours; filter, wash with dilute ammonia, dry, ignite, and weigh the magnesium pyrophosphate, of which 1 part = 0·3624 MgO.

7. *Alumina*.—The solution of the saltcake is precipitated with ammonia (free from CO₂). The precipitate is ignited and weighed. Deducting the weight of Fe₂O₃ found in No. 3, the remainder is = Al₂O₃.

8. *Sodium Sulphate (direct estimation)*.—Dissolve 1 g. of the saltcake; precipitate any lime together with ferric oxide, etc., as in No. 5; filter; evaporate the filtrate to dryness after adding a few drops of pure sulphuric acid; ignite; repeat this after adding a small piece of ammonium carbonate, and weigh. Deduct from this weight (1) the NaCl found in test No. 2, calculated for Na₂SO₄ (1·0000 NaCl = 1·2150 Na₂SO₄, or each cubic centimetre of decinormal silver solution employed in test No. 2 = 0·001774 g. Na₂SO₄); (2) the MgO found in test No. 6, calculated as MgSO₄ (1·000 MgO = 2·9836 MgSO₄). The remainder is equal to the sodium sulphate actually present in 1 g. saltcake.

C.—Chimney-Testing.

Act of Parliament.—By the Alkali Works Regulation Act of 1906, it is enacted that "Every alkali work shall be carried on in such a manner as to secure the condensation to the satisfaction of the chief inspector, (a) of the muriatic acid gas evolved in such work to the extent of 95 per centum, and to such an extent that in each cubic foot of air, smoke, or chimney gases escaping from the works into the atmosphere, there is not contained more than *one-fifth part of a grain* [= 0·457 g. per cubic centimetre] of muriatic acid; (b) of the acid gases of sulphur and nitrogen which are evolved in the process of the manufacture of sul-

phuric acid in that work to such an extent that the total acidity of such gases in each cubic foot of residual gases after completion of the process, and *before* admixture with air, smoke, or other gases does not exceed what is equivalent to *four grains* of sulphuric anhydride; (c) in the residual gases from the concentration or distillation of sulphuric acid, the total acidity of gases in each cubic foot must not exceed the equivalent of $1\frac{1}{2}$ grain of sulphuric anhydride."

Hydrochloric Acid in Chimney Gases.—In order to ascertain the HCl in chimney gases, an aspirator is used known as Fletcher's flexible aspirator, or bellows. This aspirator is supposed to draw at one aspiration one-tenth of a cubic foot. It is not safe to trust to this supposed capacity, and moreover the capacity of a new aspirator varies for some time. To ascertain the real capacity, fill a very large beaker or other cylindrical vessel with water, and invert it under water. Completely fill the aspirator with air, and expel this air into the inverted beaker. Mark the point to which the beaker is filled when the water inside the beaker is level with that outside. Measure the capacity of the beaker to that mark, say it contains V cubic centimetres of water. Then the number of aspirations which must be made with this aspirator in order to draw 1 cubic foot of air is:—

$$N = \frac{28290}{V}$$

or if the capacity of the beaker is measured in grains:—

$$N = \frac{436485}{V}$$

N will usually be a mixed number, but the nearest integral number is substituted, and it will be safest to substitute the next higher integral number. Thus, if N be found 9.3, it will be safest to consider 10 as the number of aspirations necessary to draw 1 cubic foot. The aspirator must be air-tight. The gas is withdrawn from the chimney through a glass tube, which should be sufficiently long to reach a considerable distance into the chimney, say 6 feet. The glass tube should be of at least $\frac{1}{2}$ in. diameter, otherwise the aspiration is tedious. In flues where the temperature is too high for glass, a platinum tube must be employed. The bellows and tube are washed with distilled water until the washings give no reaction with silver nitrate. 100 or 200 cubic centimetres of distilled water, free from chloride, are then charged into the bellows, and after each aspiration the gas is well washed by shaking the contents of the aspirator violently. When the number N of aspirations has been made, some water is forced into the glass tube, and allowed to flow back into the bellows to wash out any acid which may have condensed in the tube. The

liquid is then transferred into a porcelain dish (or into a beaker standing on a porcelain slab). If the liquid is so highly charged with soot that it would be impossible to recognise the change of colour, it must be filtered through a filter previously washed free from chlorides. The liquid is then oxidised with potassium permanganate, and any excess of this reagent removed with a trace of ferrous sulphate, neutralised with pure sodium carbonate, coloured with potassium chromate, and titrated with decinormal silver solution. (See p. 145 A, 3, and Appendix.) Some use a centinormal silver solution. Call the number of cubic centimetres consumed = x , then the hydrochloric acid, in grains per cubic foot of gas, will be :—

$$G = 0.05633x \text{ grains.}$$

In order to calculate the percentage escape, the velocity of the gas in the chimney must be ascertained and reduced to 60° F. No notice is usually taken of the barometric pressure, since the measurement by the bellows is otherwise inaccurate. In addition, the diameter of the chimney and the number of tons of salt decomposed during twenty-four hours in the furnaces connected with the chimney must be known.

If G = number of grains of HCl per cubic foot,

If V = velocity at 60° F. in feet per second,

If D = diameter of chimney at testing-hole in feet,

If T = tons of salt decomposed per twenty-four hours assumed to contain 98 per cent. NaCl,

the percentage escape will be :—

$$0.7458 \times \frac{GVD^2}{T}$$

D.—Testing of the Gases in the Hargreaves' Process.

(a) *Total acidity*, as described p. 117.

(b) *Sulphur dioxide*, as p. 116.

(c) *Hydrogen chloride* is estimated in the sample taken for (a), as described p. 148. By deducting (b) and (c) from (a), the amount of SO_3 is found.

E.—Hydrochloric Acid.

1. SPECIFIC GRAVITY OF PURE HYDROCHLORIC ACID AT 15° C. COMPARED WITH WATER AT 4°, AND REDUCED TO VACUUM. (Lunge and Marchlewski.)

Degrees Twaddell.	Specific Gravity at 15° 4° in vacuo.	100 parts by weight correspond to parts by weight of			1 litre contains g. of HCl.	1 cubic foot contains lbs. of HCl.
		HCl.	Acid of spec. gravity 1·1425 = 23·5° Tw.	Acid of spec. gravity 1·152 = 30·4° Tw.		
0	1·000	0·16	0·57	0·58	1·6	0·10
1	1·005	1·15	4·08	8·84	12·	0·75
2	1·010	2·14	7·60	7·14	22·	1·87
3	1·015	3·12	11·80	10·41	32·	1·99
4	1·020	4·18	14·67	18·79	42·	2·62
5	1·025	5·15	18·80	17·19	58·	3·80
6	1·030	6·15	21·85	20·58	64·	3·99
7	1·035	7·15	25·40	23·87	74·	4·61
8	1·040	8·16	28·99	27·24	85·	5·80
9	1·045	9·16	32·55	30·58	96·	5·98
10	1·050	10·17	36·14	33·95	107	6·67
11	1·055	11·18	39·73	37·33	118	7·85
12	1·060	12·19	43·32	40·70	129	8·04
13	1·065	13·19	46·87	44·04	141	8·79
14	1·070	14·17	50·35	47·31	152	9·48
15	1·075	15·16	53·87	50·62	163	10·16
16	1·080	16·15	57·39	53·92	174	10·85
17	1·085	17·13	60·87	57·19	186	11·59
18	1·090	18·11	64·35	60·47	197	12·28
19	1·095	19·06	67·73	63·64	209	13·08
20	1·100	20·01	71·11	66·81	220	13·71
21	1·105	20·97	74·52	70·01	232	14·46
22	1·110	21·92	77·89	73·19	243	15·15
23	1·115	22·86	81·23	76·32	255	15·90
24	1·120	23·82	84·64	79·53	267	16·65
25	1·125	24·78	88·06	82·74	278	17·38
26	1·130	25·75	91·50	85·97	291	18·14
27	1·135	26·70	94·88	89·15	303	18·89
28	1·140	27·66	98·29	92·35	315	19·64
29	1·145	28·61	101·67	95·52	328	20·45
30	1·150	29·57	105·08	98·73	340	21·20
31	1·155	30·55	108·53	102·00	353	22·01
32	1·160	31·52	112·01	105·24	366	22·82
33	1·165	32·49	115·46	108·48	379	23·63
34	1·170	33·46	118·91	111·71	392	24·44
35	1·175	34·42	122·32	114·92	404	25·19
36	1·180	35·39	125·76	118·16	418	26·06
37	1·185	36·31	129·08	121·23	430	26·81
38	1·190	37·23	132·30	124·30	443	27·63
39	1·195	38·16	135·61	127·41	456	28·43
40	1·200	39·11	138·98	130·58	469	29·24

2. INFLUENCE OF TEMPERATURE ON THE SPECIFIC GRAVITY OF HYDROCHLORIC ACID.

0°.	5°.	10°.	15°.	20°.	25°.	30°.	35°.	40°.	45°.	50°.
1·168	1·165	1·163	1·160	1·157	1·154	1·152	1·149	1·147	1·144	1·142
1·158	1·155	1·153	1·150	1·147	1·145	1·142	1·139	1·137	1·134	1·132
1·148	1·145	1·143	1·140	1·137	1·134	1·132	1·129	1·127	1·125	1·123
1·138	1·135	1·133	1·130	1·127	1·125	1·122	1·119	1·117	1·114	1·112
1·128	1·125	1·123	1·120	1·117	1·115	1·112	1·110	1·108	1·106	1·106
1·118	1·115	1·113	1·110	1·107	1·105	1·103	1·101	1·099	1·097	1·094
1·108	1·105	1·103	1·100	1·097	1·095	1·092	1·090	1·088	1·086	1·084
1·098	1·095	1·093	1·090	1·087	1·085	1·082	1·080	1·077	1·075	1·073
1·088	1·085	1·083	1·080	1·077	1·075	1·073	1·070	1·068	1·066	1·064
1·078	1·075	1·073	1·070	1·068	1·066	1·063	1·061	1·059	1·057	1·055
1·068	1·065	1·063	1·060	1·058	1·055	1·053	1·050	1·048	1·046	1·044
1·058	1·055	1·053	1·050	1·048	1·045	1·043	1·040	1·038	1·035	1·033
1·048	1·045	1·043	1·040	1·037	1·035	1·032	1·030	1·027	1·025	1·022
1·038	1·035	1·033	1·030	1·027	1·024	1·022	1·019	1·017	1·014	1·012
1·028	1·025	1·023	1·020	1·017	1·014	1·012	1·009	1·007	1·004	1·002
1·018	1·015	1·013	1·010	1·007	1·004	1·002	0·999	0·997	0·994	0·992
55°.	60°.	65°.	70°.	75°.	80°.	85°.	90°.	95°.	100°.	
1·140	1·138	1·136	1·133	1·131	1·129	1·127	1·125	1·123	1·121	
1·130	1·128	1·126	1·123	1·121	1·119	1·116	1·114	1·112	1·110	
1·120	1·118	1·116	1·113	1·111	1·108	1·106	1·104	1·102	1·099	
1·109	1·107	1·104	1·102	1·100	1·097	1·095	1·093	1·090	1·088	
1·101	1·099	1·096	1·094	1·091	1·089	1·086	1·084	1·081	1·079	
1·098	1·090	1·088	1·085	1·083	1·080	1·078	1·075	1·073	1·070	
1·082	1·080	1·078	1·076	1·073	1·071	1·069	1·066	1·064	1·061	
1·071	1·069	1·067	1·065	1·063	1·061	1·059	1·057	1·055	1·053	
1·062	1·060	1·058	1·056	1·054	1·053	1·051	1·049	1·047	1·045	
1·053	1·051	1·049	1·048	1·046	1·044	1·043	1·041	1·039	1·037	
1·042	1·040	1·038	1·036	1·034	1·033	1·031	1·029	1·027	1·025	
1·031	1·029	1·027	1·025	1·023	1·021	1·019	1·017	1·115	1·013	
1·020	1·018	1·016	1·014	1·011	1·009	1·007	1·005	1·003	1·001	
1·010	1·008	1·006	1·003	1·001	0·999	0·997	0·995	0·993	0·991	
1·000	0·998	0·995	0·993	0·991	0·989	0·987	0·985	0·983	0·981	
0·990	0·988	0·985	0·983	0·981	0·979	0·977	0·975	0·973	0·971	

3. ANALYSIS OF HYDROCHLORIC ACID.

(a) *Estimation of HCl.*—Measure off, by means of an accurate pipette, 10 c.c. of the acid, the specific gravity of which should be known, dilute to 200 c.c., take out 10 c.c. Or else employ a glass-tap pipette, as described p. 144, for fuming sulphuric acid; in this case its contents are run into water and employed directly for

titration. Add sodium carbonate, free from chloride, till the reaction is neutral or faintly alkaline. This point will be hit quickly, and without the loss of many drops for testing, if the percentage of the acid is ascertained from its specific gravity by the table (p. 150) and the corresponding quantity of sodium carbonate solution is run in from a burette. Now add a little neutral potassium chromate, and titrate with decinormal silver solution till a faint pink colour is produced (*cf.* p. 145). Deduct 0.2 c.c. from the silver solution employed; the remainder, multiplied by 72.92 and divided by the specific gravity of the acid, indicates its percentage of HCl. This test would fail in the presence of metallic chlorides, which are, however, hardly ever present in appreciable quantity in ordinary hydrochloric acid. The free HCl can also be ascertained by estimating the total acidity and deducting therefrom that due to sulphuric acid, making allowance for any sodium sulphate present.

(b) *Estimation of Sulphuric Acid.*—Neutralise the acid almost, but not quite, with sodium carbonate free from sulphate, and precipitate the sulphuric acid by barium chloride, as on p. 110. If the acid be partially saturated with NH_3 , or not saturated at all, the result is too low. Each part of BaSO_4 is equal to 0.34293 SO_3 .

(c) *Estimation of Iron.*—Reduce this to ferrous iron by digesting the acid for a short time with a rod of zinc free from iron, wash the rod, dilute the whole with water, add some manganous chloride or sulphate (in order to counteract the action of HCl on permanganate), and titrate with a twentieth normal solution of potassium permanganate, each cubic centimetre of which indicates 0.002795 g. Fe. In case of SO_2 being present, this must first be oxidised to sulphuric acid, before reducing the ferric salt and titrating.

(d) *Free Chlorine.*—Introduce a sample of the acid into a flask, remove the air from the empty space by CO_2 ; shake the acid with a strip of clean metallic copper. The latter will be converted into chloride by the free chlorine, and the copper thus dissolved can be detected by potassium ferrocyanide, etc. This will show the smallest traces of chlorine. For ordinary purposes it is sufficient to heat the acid gently and hold a strip of KI starch paper in the vapour; this will at once turn blue in the presence of free Cl.

(e) *Sulphur Dioxide.*—Oxidise with permanganate, or iodine, or H_2O_2 to sulphuric acid, estimate the total H_2SO_4 now present as in No. 2, and deduct the quantity there found, the remainder = SO_2 .

(f) *Arsenic.*—Reduce all to trichloride by passing in SO_2 for some time, and precipitate by H_2S as As_2S_3 . Wash the precipitate, dissolve it on the filter in ammonia, evaporate the solution in a glass or porcelain dish, dry at 100° , and weigh. One part As_2S_3 = 0.60931 As = 0.80429 As_2O_3 .

IV. BLEACHING POWDER AND CHLORATE OF POTASH MANUFACTURE.

A.—Natural Manganese Ore.

1. *Manganese Dioxide*.—Weigh 1.0875 g. of manganese ore, ground as fine as possible, and dried for some time at 100° C.; put it into the flask (Fig. 12) closed by a rubber (Bunsen) valve or, preferably, into a flask provided with a Contat-Göckel bulb (Fig. 13), which has been half-filled with a concentrated solution of sodium carbonate; put into the flask 75 c.c. (in three portions with a 25 c.c. pipette) of a solution containing



FIG. 12.

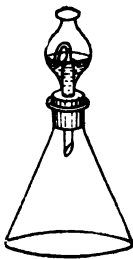


FIG. 13.

100 g. pure crystallised ferrous sulphate and 100 c.c. pure concentrated sulphuric acid, diluted to 1 litre, and standardised on the same day by means of the same 25 c.c. pipette, with decinormal potassium permanganate. Close the flask with its cork or valve, and heat till the manganese is completely decomposed, leaving a light-coloured residue. On cooling, the valve must act properly, which will be seen by the collapsing of the rubber tube, Fig. 12, or by the running in of sodium carbonate solution, Fig. 13. After complete cooling add 200 c.c. of water, and titrate with potassium permanganate to a faint pink coloration. Deduct the quantity of permanganate required from that corresponding to the 75 c.c. of iron solution; the remainder indicates for each cubic centimetre 0.02175 g., equal to 2 per cent. MnO_2 .

2. *Carbon Dioxide* is estimated gravimetrically by expelling it with dilute sulphuric or nitric acid and absorbing it with soda-lime, by means of the apparatus and process described (p. 112, No. 6). Or more quickly by Lunge and Rittener's gas-volumetric process, see p. 169.

3. *Estimation of the Hydrochloric Acid required for Decomposing the Ore.*—Dissolve 1 g. of manganese ore in a flask provided with a reflux condenser in 10 c.c. of ordinary strong hydrochloric acid the titre of which is known, employing heat as far as necessary. Allow the solution to cool, add standard alkali till reddish-brown flakes of ferric hydroxide appear, which do not redissolve on agitation. Calculate the standard alkali corresponding to the acid employed for dissolving the ore, and deduct the quantity thus found from the 10 c.c. first employed.

B.—Recovered Manganese Mud and Weldon Liquors.

1. *MnO₂ in Weldon Mud.*—Standardise an acid iron solution (100 g. pure crystallised ferrous sulphate + 100 c.c. pure concentrated sulphuric acid in 1 litre) with seminormal potassium permanganate (*cf.* Appendix), by diluting 25 c.c. of the former with 100 c.c. or 200 c.c. of cold water, and adding the permanganate from a stopcock burette, till, on agitating, the pink colour is not discharged immediately, but remains at least for half a minute. Subsequent decolorisation is not taken into account. This test should be made once each day. Call the cubic centimetres of permanganate employed x . Now, put another 25 c.c. of the iron solution into a beaker. Take 10 c.c. of manganese mud out of the well-shaken bottle (mere stirring does not ensure a proper mixture) containing it; wash the pipette outside, run its contents into the beaker containing the iron solution, and wash the mud remaining inside into the same beaker. When all has dissolved, on agitating, add 100 c.c. of water, and titrate with potassium permanganate. The number of cubic centimetres now used equals y . The quantity of MnO₂ in grams per litre of mud equals $2.175(x - y)$.

2. *Total Manganese of the Mud, expressed in Grams of theoretically possible MnO₂ per Litre.*—Take 10 c.c. of the mud, with the same precautions as in test No. 1. Boil with strong hydrochloric acid till all chlorine is driven off; saturate the excess of acid by ground marble or precipitated calcium carbonate; add a concentrated filtered solution of bleaching powder; boil a few minutes till the colour turns a decided pink, and the excess of bleaching powder can be smelt, and again destroy the pink colour by adding alcohol drop by drop. All manganese is now present as MnO₂; filter and wash. The filtrate should not produce any brown colour with a bleaching-powder solution, which would show the presence of Mn in solution. Continue the washing till starch and KI do not give any reaction. Transfer the filter with the precipitate into 25 c.c. of the acid iron solution employed in test No. 1. If all MnO₂ is not dissolved, add another 25 c.c. of

iron solution; dilute with 100 c.c. of water, and titrate with permanganate. Calculation as in No. 1.

3. *Estimation of the "Base," i.e., the Monoxides, etc., of the Mud which combine with HCl without yielding Free Chlorine.*—Dilute 25 c.c., or with a very rich base 50 c.c., of normal oxalic acid (63 g. crystallised oxalic acid in 1 litre) to 100 c.c.; heat to 60° to 80° C., add 10 c.c. manganese mud by means of a pipette, with the precautions stated in No. 1, and agitate till the colour of the precipitate is no longer yellowish but pure white, which ought to take place very soon at the above temperature. Dilute to 202 c.c. (2 c.c. correspond to the volume of the precipitate, and are marked on the neck of the 200 c.c. flask); pour through a dry filter, and titrate 100 c.c. of the filtrate with standard alkali, employing phenolphthalein as indicator. (Methyl orange is not applicable for oxalic acid.) Call the number of cubic centimetres of standard alkali z . The oxalic acid serves (1) for reducing the MnO_2 with formation of MnO and CO_2 ; (2) for saturating the MnO thus formed; (3) for saturating the monoxides originally present, *i.e.*, the base. The oxalic acid not thus used is equal to $2z$. The acid used for reducing MnO_2 is equal to that used for neutralising the MnO formed, and both amounts together are equal to the value $x-y$ obtained by the MnO_2 test, since the oxalic acid is normal and the permanganate half normal. The amount of oxalic acid consumed by the bases of the mud is found by deducting from the total acid used that required for the MnO_2 ($x-y$), and that which was not neutralised at all by the mud— $2z$, therefore in all $x-y-2z$. The "base" is equal to the ratio of this value to that found in test No. 1, *viz.*, $\frac{x-y}{2}$

It is, therefore, if 25 c.c. of oxalic acid had been employed, equal to :

$$\frac{50 - 2x - 4z + 2y}{x - y} = \left(\frac{50 - 4z}{x - y} \right) - 2$$

or, if 50 c.c. had been employed, equal to :—

$$\left(\frac{100 - 4z}{x - y} \right) - 2$$

C.—Limestone.

1. *Insoluble Matter.*—Dissolve 1 g. in hydrochloric acid, filter the residue, wash, dry, and ignite. In the presence of appreciable quantities of organic matter weigh the filter after drying at 100°, and ignite afterwards. The difference is taken as organic matter.

2. *Lime.*—Dissolve 1 g. in 25 c.c. normal hydrochloric acid

and titrate with normal alkali. Deduct the volume of the latter used from 25 and multiply the remainder with 2.8 to find the percentage of CaO, or with 5 to find that of CaCO₃. (*N.B.*—Here MgO is calculated as CaO. This is admissible for most limestones employed in alkali and bleaching powder making, because they contain but little MgO; otherwise the MgO or MgCO₃ found as in No. 3 must be deducted.)

3. *Magnesia* need only be estimated in limestone used for manganese recovery. Dissolve 2 g. of limestone in HCl, precipitate the CaO with NH₃ and ammonium oxalate, and precipitate the magnesia in the filtrate by sodium phosphate (*cf.* p. 147).

4. *Iron* is usually estimated only in limestone used for bleaching powder making. Dissolve 2 g. HCl, reduce by zinc, dilute, add some manganese solution free from iron, and titrate with permanganate (*cf.* p. 142).

D.—Quicklime.

1. *Free CaO*.—Weigh 100 g. of an average sample carefully taken, slake it completely, put the milk into a half-litre flask, fill up to the mark, shake well, take 100 c.c. out, run it into a half-litre flask, fill up, mix well, and employ 25 c.c. of the contents, equal to 1 g. quicklime, for the test. Titrate with normal oxalic acid and phenolphthalein as indicator, adding the acid *very slowly* and shaking well after each addition. The colour is changed when all free lime has been saturated and before the CaCO₃ is attacked. One c.c. normal HCl = 0.02805 g. CaO.

2. *Carbon Dioxide*.—Titrate CaO and CaCO₃ together by dissolving in an excess of standard hydrochloric acid and titrating back with standard alkali. By deducting the CaO estimated as in No. 1 the quantity of CaCO₃ is obtained. For very accurate estimations the CO₂ is expelled by HCl, absorbed in soda-lime, and weighed as described; or it is estimated by volume in Lunge and Rittener's apparatus (p. 169).

E.—Slaked Lime.

1. *Water*.—Weigh about 1 g. in a stoppered glass tube, and heat it gradually in a platinum crucible, at last to a strong red heat (*cf.* p. 146); allow to cool in the exsiccator, and weigh. The loss of weight is equal to H₂O + CO₂.

2. *Carbon Dioxide* is estimated as above in D, 2.

3. *Estimation of the percentage of Caustic Lime in Milk of Lime by means of the specific gravity* (Blattner).—Thin milk of lime is poured into the cylinder and the reading of the hydrometer is taken quickly, before the lime subsides. For thick milk of lime employ a somewhat wide cylinder, put the hydrometer in without

using any force and turn the cylinder slowly round, so that it receives a slight shaking, until the hydrometer ceases to sink. The following table is valid for 15° C.

TABLE SHOWING AMOUNT OF LIME IN MILK OF LIME.
(Calculated from Blattner.)

Degrees Twaddell.	Grms. CaO per litre.	Lbs. CaO per cubic foot.	Degrees Twaddell.	Grms. CaO per litre.	Lbs. CaO per cubic foot.
2	11·7	0·7	28	177	11·1
4	24·4	1·5	30	190	11·9
6	37·1	2·3	32	203	12·7
8	49·8	3·1	34	216	13·5
10	62·5	3·9	36	229	14·3
12	75·2	4·7	38	242	15·1
14	87·9	5·5	40	255	15·9
16	100	6·3	42	268	16·7
18	113	7·1	44	281	17·6
20	126	7·9	46	294	18·4
22	138	8·7	48	307	19·2
24	152	9·5	50	321	20·0
26	164	10·3			

F.—Bleaching Powder.

1. *Available Chlorine.*—Weigh 7·090 g. of the sample, previously well mixed; grind it with a little water in a porcelain mortar (the lip of which has been greased a little underneath) till a completely homogeneous thin paste has been obtained; dilute with more water, wash the whole into a litre flask, fill up to the mark, and take for each test 50 c.c.=0·3545 g. bleaching powder, having shaken up the flask immediately before. Run into the above, with continuous agitation, an alkaline decinormal arsenite solution, containing 4·95 g. As_2O_3 per litre (*cf.* Appendix) till the expected point is not very far off. Then place a drop of the mixture on to a piece of filter paper, moistened with a starch solution containing potassium iodide. If there is very much chlorine left, a brown spot will be produced; if less chlorine, the spot will be blue. According to the depth of this colour more or less arsenite solution is run in, and the above test is repeated till the paper is coloured hardly perceptibly, or not at all. Each cubic centimetre of the arsenite solution indicates 1 per cent. available chlorine. (For sampling of bleach, *cf.* Appendix.)

Another very accurate method, requiring no standard solution,

consists in decomposing the bleaching powder by hydrogen peroxide in a nitrometer or gas-volumeter (Lunge, *S.C.I.*, 1890, 22).

2. *Comparison of the Percentage of Bleaching Powder with the French (Gay-Lussac) Degrees.*—The latter are understood to mean the number of litres of chlorine gas at 0° C. and 760 mm. pressure, which could be given off by 1 kilogram of bleaching powder. The oxygen given off in the hydrogen peroxide method (*cf.* last paragraph) shows this directly.

French Degrees.	Per cent. Chlorine.	French Degrees.	Per cent. Chlorine.	French Degrees.	Per cent. Chlorine.	French Degrees.	Per cent. Chlorine.
63	20·02	80	25·42	97	30·82	113	35·91
64	20·34	81	25·74	98	31·14	114	36·22
65	20·65	82	26·06	99	31·46	115	36·54
66	20·97	83	26·37	100	31·78	116	36·86
67	21·29	84	26·69	101	32·09	117	37·18
68	21·61	85	27·01	102	32·41	118	37·50
69	21·93	86	27·33	103	32·73	119	37·81
70	22·24	87	27·65	104	33·05	120	38·13
71	22·56	88	27·96	105	33·36	121	38·45
72	22·88	89	28·28	106	33·68	122	38·77
73	23·20	90	28·60	107	34·00	123	39·08
74	23·51	91	28·92	108	34·32	124	39·40
75	23·83	92	29·23	109	34·64	125	39·72
76	24·15	93	29·55	110	34·95	126	40·04
77	24·47	94	29·87	111	35·27	127	40·36
78	24·79	95	30·19	112	35·59	128	40·67
79	25·10	96	30·51				

3. *Carbon Dioxide in Bleaching Powder or Bleach Liquors by Lunge and Rittener's Process.*—The same apparatus is employed as that described later on for sodium carbonate solutions (p. 169), and the operation is carried out in the same way, but no aluminium must be used in this case for expelling the gases, but 2 or 3 c.c. of a 3 per cent. solution of hydrogen peroxide which during the final boiling gives out oxygen gas.

Employ only so much of the substance that not more than 50 or 60 c.c. of gas (CO₂ and Cl₂) is formed; read off the volume of the gases = *c* in the Bunté burette, charged with concentrated sodium chloride solution, after allowing twenty minutes for cooling, and after putting the level-bottle in the proper position. Introduce into the burette funnel an excess of decinormal arsenic solution = *d* c.c.; run this slowly into the burette, so that it forms a layer above the salt solution; wash the funnel two or three times with a few c.c. of water; shut off the connection with the level-bottle,

shake for two minutes; run into the burette so much of a 30 per cent. solution of sodium hydroxide that, on shaking, no more will run in; read off the volume of gas = b . The figure $c - b$, or, after reduction to 0° and 760 mm. $c_1 - b_1$, indicates the absorbed c.c. $\text{CO}_2 + \text{Cl}_2$. Now run the contents of the burette into a flask, wash the burette with water, add to the whole an excess of NaHCO_3 , and titrate with decinormal iodine; the c.c. used = e . Since 20,000 c.c. $\frac{n}{10}$ arsenic solution indicate 22,030 c.c. Cl_2 , we have had in the burette,

$$\frac{22030}{20000} \times (d - e) \text{ c.c. chlorine.}$$

and together with this,

$$(c_1 - b_1) - \frac{22030}{20000} (d - e) \text{ c.c. CO}_2.$$

4. *Testing the Atmosphere of the Chambers for Chlorine before opening them.*—In England a maximum of 5 grains chlorine per cubic foot (=11.5 g. per cubic metre) is prescribed before the chamber may be opened. This is ascertained by the apparatus, Fig. 14. A is a rubber pressure ball holding about 100 c.c., B a hole in its mouthpiece, D a glass tube reaching nearly to the bottom of the glass jar E; its lower end is contracted so that only a thin needle can pass through. E is charged with 26 c.c. of a solution, so prepared that ten deliveries of the bulb indicate $2\frac{1}{2}$ grains (or five deliveries 5 grains) chlorine per cubic foot. It is prepared by dissolving 0.3485 arsenious acid in sodium carbonate solution, neutralising with sulphuric acid, adding 25 g. potassium iodide, 5 g. precipitated calcium carbonate, 6 to 10 drops liquor ammoniæ, and diluting the whole to 1 litre. To the 26 c.c. of this solution add a little starch solution, introduce the outer end of D into the bleaching-powder chamber 2 feet above the bottom, compress A and close the hole B by a finger, whereupon the pressure on A is relieved. By the expansion of the rubber ball A chamber air is aspirated into the liquid contained in E. Note the number of times the ball A must be employed as described, before the liquid is coloured by the separation of iodine. According to the prescribed limit, this number should be at least 5.

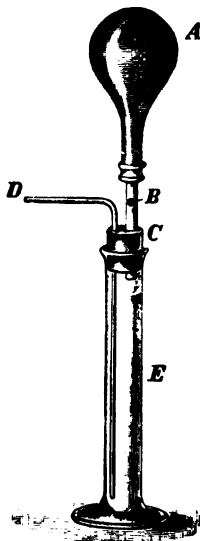


FIG. 14.

G.—Deacon Process.

1. *Proportion of HCl and Cl in the Gases.*—Aspirate 5 litres of gas, issuing from the decomposer, placing the apparatus as near to the outlet of the decomposer as possible, and absorb the hydrochloric acid and chlorine in a solution of caustic soda of 15° Tw., of which about 250 c.c. are distributed into two or three absorbing bottles. The time of absorption ought to agree with the time occupied by the charge in the saltcake pan. Unite the contents of the several bottles and dilute to 500 c.c.

(a) Take 100 c.c. of this solution, and add it gradually to 25 c.c. of an iron solution (prepared and standardised as directed on page 154) in a flask as shown in Fig. 13, p. 153, and heat to boiling. Allow to cool, dilute with 200 c.c. of water, and titrate with seminormal permanganate solution. Say it required y c.c. Suppose that when standardising the iron solution 25 c.c. of iron solution required x c.c.

(b) Take 10 c.c. of the solution to be tested, add some solution of sulphurous acid, acidify with dilute sulphuric acid; if it does not smell of sulphurous acid, add a little more. Heat to boiling. When cool, add, if necessary, a few drops of permanganate to oxidise any sulphurous acid in excess. Neutralise with pure carbonate of soda, dilute with water, and after adding a few drops potassium chromate, titrate with decinormal silver solution. Suppose it requires z c.c. of silver solution. Then

$$\frac{50x - y}{z}$$

is the percentage of hydrochloric acid decomposed, and

$$\frac{43.53 + \frac{x - y}{8}}{z}$$

equals the amount of air present for every volume of hydrochloric acid. If any other volume, l , of gas instead of 5 litres be employed, the constant 43.53 becomes

$$\frac{1.624n}{50 \times 0.003645}$$

assuming that the other directions are strictly followed, and that 1 litre of hydrochloric acid weighs 1.624 g. at 15° C. at 760 mm. pressure.

2. *Carbon Dioxide.*—Pass 20 litres of the gas, from which the HCl has been removed by water, into an ammoniacal solution of barium chloride, heat this finally, filter the BaCO₃ and estimate

this by igniting, or by converting it into BaSO_4 , of which 1 g. = 0.1885 g. CO_2 . Cf. also below, *sub H*.

3. *Steam*.—Pass the gas through a weighed tube, containing pumice moistened with strong sulphuric acid, and before reweighing remove the other gases by a current of air.

H.—Electrolytic Chlorine.

Examination for Carbon Dioxide.—Chlorine gas produced by means of gas carbon electrodes may contain up to 12 per cent. carbon dioxide. This CO_2 is estimated by Ferchland's process, as modified in Lunge's laboratory.

A dry Bunte burette, the content of which (from tap to tap = v) is exactly known, is filled with the chlorine by passing this through for some time, the gas passing in from below, so as to rise regularly below the lighter air. When filled with the chlorine gas under atmospheric pressure, the burette is fixed in a clamp in a vertical position, and a level tube is attached by means of a strong rubber tube, filled with mercury to the bottom tap, which has a single bore. The rubber tube must be entirely filled with mercury, so that no air can get into the burette, and it is secured against slipping off by iron wire. When the bottom tap of the burette is opened, mercury enters into the burette and absorbs the chlorine, at first pretty quickly, but later on its surface is covered by a pellicle, which precludes further action. Then the bottom tap is closed, and by agitating the burette the complete absorption of the chlorine is effected. The sides of the burette are thereby covered with a non-transparent layer, and a mixture of mercurous chloride and mercury floats on the top of the mercury, which prevents reading off the volume. When the absorption of the chlorine is finished, open the bottom tap, put the level of the mercury approximately equal in the burette and the level tube, and allow ten or fifteen minutes for the equalisation of the temperature. Now put 1 c.c. saturated solution of sodium chloride into the top beaker, and allow this to enter the burette by lowering the level tube. This causes the pulverulent mixture on the top of the mercury to subside, and an easily readable surface to be formed. Then adjust the levels for atmospheric pressure, as described in the case of the nitrometer (p. 137) and read the volume of gas = a . Now introduce a little concentrated solution of potassium hydroxide through the funnel into the burette, absorb the CO_2 by shaking, re-establish atmospheric pressure, and read the new volume of gas = b . The formula $\frac{(a - b) 100}{v}$ shows the percentage of CO_2 in the crude chlorine gas.

No correction for vapour tension of water need be made in this case, if concentrated solutions have been used.

I.—Chlorate of Potash.

1. *Chlorate Liquors* contain calcium chlorate and chloride, but these are calculated as potassium salts for the sake of convenience.

(a) *Chlorate* is estimated both in order to check the work and to calculate the necessary addition of KCl. Measure 2 c.c. of liquor in an accurate pipette, run it into the flask (Fig. 13, p. 153), add a little hot water and one drop of alcohol, boil (without the valve) till all smell of chlorine and the pink colour have disappeared, allow to cool, add 25 c.c. of the strongly acid ferrous sulphate solution (cf. p. 154, and requiring *a* c.c. of seminormal permanganate), close the flask with its valve, and boil for ten minutes. After cooling, titrate with seminormal permanganate. The number of cubic centimetres required to produce a faint pink = *b*. The liquor then contains calcium chlorate equivalent to $5.105(a - b)$ g. KClO_3 per litre, and it will theoretically require an amount of $3.106(a - b)$ g. of pure KCl per litre.

(b) *Chloride* is estimated in order to check the work, and is therefore calculated as KCl, although present as CaCl_2 . Treat 1 c.c. of liquor as above, to destroy the free chlorine and pink colour, allow to cool, add a little neutral potassium chromate, and titrate with decinormal silver nitrate (as described p. 145). Each cubic centimetre of the latter indicates chloride equivalent to 7.46 g. KCl per litre.

2. *Commercial Chlorate of Potash* is only tested for any chlorides calculated as KCl. As their quantity is very small, it is advisable to dissolve 50 g. of the salt in water absolutely free from chlorine, and to test with decinormal silver nitrate, as in 1 (b). Each cubic centimetre of this solution = 0.00746 g. KCl = 0.015 per cent. KCl.

K.—Bleach Liquors.

These are tested like Bleaching Powder, p. 157.
Electrolytic Bleach Liquor, see p. 191.

**PRESSURE AND SPECIFIC GRAVITY OF LIQUID
CHLORINE. (Knietzsch.)**

Temperature.	Pressure.	Specific Gravity.	Mean coefficient of expansion.
-88°	37.5 mm. Hg.	...	} 0.001409
-85	45.0 "	...	
-80	62.5 "	1.6602	
-75	88.0 "	1.6490	
-70	118 "	1.6382	
-65	159 "	1.6273	
-60	210 "	1.6167	
-55	275 "	1.6055	
-50	350 "	1.5945	
-45	445 "	1.5830	
-40	560 "	1.5720	
-35	705 "	1.5589	
-33.6	760 "	1.5575	
-30	1.20 atm.	1.5485	
-25	1.50 "	1.5358	
-20	1.84 "	1.5230	
-15	2.23 "	1.5100	
-10	2.63 "	1.4965	
- 5	3.14 "	1.4830	
± 0	3.66 "	1.4690	
+ 5	4.25 "	1.4548	} 0.001978
+10	4.95 "	1.4405	
+15	5.75 "	1.4273	} 0.002030
+20	6.62 "	1.4118	
+25	7.63 "	1.3984	} 0.002190
+30	8.75 "	1.3815	
+35	9.95 "	1.3683	} 0.002260
+40	11.50 "	1.3510	
50	14.70 "	1.3170	} 0.002690
60	18.60 "	1.2830	
70	23.00 "	1.2430	} 0.003460
80	28.40 "	1.2000	
90	34.50 "		
100	41.70 "		
110	50.80 "		
120	60.40 "		
130	71.60 "		
146	93.50 "	Critical Point	

V. SODA ASH MANUFACTURE BY THE LEBLANC PROCESS.

A.—Raw Materials.

1. SALTCAKE.—(Cf. p. 146).
2. LIMESTONE or CHALK, for mixing.
 - (a) *Insoluble*.—(Cf. p. 155).
 - (b) *Lime* (+ MgO).—(P. 156).
 - (c) *Magnesia* (only in limestones containing much magnesia).—(P. 156).
3. MIXING COAL (slack).
 - (a) *Moisture*.—(P. 95).
 - (b) *Fixed Carbon*.—(P. 95).
 - (c) *Ash* (p. 95).—In the case of unknown descriptions of coal it is not sufficient to estimate the total percentage of ash, but the latter should be analysed, and silica, alumina, and ferric oxide estimated according to the methods for the analysis of silicates.
 - (d) *Sulphur*.—Mix 0.5 g. to 1 g. of finely ground coal with one and a half times the weight of an intimate mixture of two parts well-calcined magnesia and one part anhydrous sodium carbonate. This is done by means of a glass rod in a platinum crucible, which is heated without cover, and in a slanting position, so that only its lower half attains red heat, preferably in the perforated asbestos board (Fig. 1, p. 96). The combustion should be assisted by frequent stirring with a platinum wire, and should not last longer than an hour, the grey colour of the mixture passing into yellow, reddish, or brown. Pour hot water over the mass, add bromine-water till the liquid is faintly yellow; boil, decant through a filter, and wash with hot water. Acidulate the filtrate with HCl, boil till all bromine is removed and the liquor has been decolorised, and precipitate with barium chloride (as described p. 96). If the magnesia or sodium carbonate employed contains sulphates, these must be estimated and taken into account. If the gas contains much sulphur, it is best to employ a spirit lamp, but the perforated asbestos board, as recommended above, will nearly always suffice to keep away the products of combustion of the gas from the contents of the crucible, and thus admit of employing ordinary illuminating gas and a Bunsen burner.
 - (e) *Nitrogen* is estimated by igniting with soda-lime and absorbing the ammonia formed in standard sulphuric acid, according to the method employed in organic analysis.

B.—Black-Ash.

Digest 50 g. of the finely powdered average sample with 480 c.c. of water at 45° C., which have been previously freed from CO₂,

and O by boiling and cooling down in a corked bottle. This will produce 500 c.c. of liquid. Shake at once and afterwards frequently, at least during two hours. The following tests are made partly with the muddy mixture, partly with the clear portion; the former ones must be made to begin with.

1. TESTS MADE WITH THE MUDDY MIXTURE.—Each time before taking out a sample, the flask is thoroughly shaken up, and before the deposit settles again a sample is taken by means of a 5 c.c. pipette, with a short and somewhat wide outlet (to prevent obstruction by the mud). The mud outwardly adhering is washed off, the contents of the pipette are run out into a beaker, and the mud adhering to the inside of the pipette is washed into the same beaker.

(a) *Free Lime* (or its equivalent of sodium hydroxide) is estimated by adding to 5 c.c. of the mixture an excess of barium chloride solution, as well as a drop of phenolphthalein solution, and titrating with $\frac{1}{2}$ normal oxalic acid, till the red colour has just vanished. Each c.c. of the acid = 0.00561 g. CaO.

(b) *Total Lime*.—5 c.c. of the muddy mixture are put into a flask, a few c.c. of concentrated hydrochloric acid are added, and the whole is boiled till all the gases have been expelled. Cool down a little, add a drop of methyl orange solution, and neutralise exactly with sodium carbonate, *i.e.*, till the red colour has just gone. Then add 30 c.c. of $\frac{1}{2}$ normal sodium carbonate solution, measured exactly, and heat to boiling, to precipitate all the lime as CaCO_3 (together with any ferric oxide, alumina and magnesia, the quantity of which is too insignificant to be regarded for this test). Wash the whole into a 200 c.c. flask, fill up to the mark, take 100 c.c. of the clear liquid, and titrate back with $\frac{1}{2}$ normal hydrochloric acid. Deduct the c.c. used $\times 2$ from 30; the difference $\times 0.00561$ = total lime, or $\times 0.01001$ = calcium carbonate.

(*N.B.*—These tests cannot be expected to give very accurate results, owing to the almost insurmountable difficulty of obtaining a real average sample of black-ash ball. This, however, applies to all tests made with black-ash.)

2. TESTS MADE WITH THE CLEAR PORTION.—After having made all the tests described under 1, allow the mixture to settle down in the well-corked flask, and take samples of the supernatant, clear liquid for the following tests:—

(a) *Available Alkali and Sodium Carbonate*.—10 c.c. (= 1 g. black-ash) is titrated cold with hydrochloric acid and methyl orange. This indicates the total available alkali, *i.e.*, Na_2CO_3 , NaOH, and Na_2S . (The small quantity of alumina and silica present causes no appreciable error.) By deducting the quantities found in tests Nos. 2 and 3 the quantity of *sodium carbonate* is found, *viz.*, 0.05305 g. for each cubic centimetre of normal HCl. It is, however, expressed, like all other sodium compounds, in

terms of Na_2O , by multiplying each cubic centimetre of normal acid used by 0.03105.

(b) *Caustic Soda* is estimated by adding to 20 c.c. of solution, contained in a 100 c.c. flask, an excess of barium chloride (10 c.c. of a 10 per cent. solution of $\text{BaCl}_2 \cdot 2\text{H}_2\text{O}$, will always more than suffice for this), adding boiling water up to the mark, shaking up, and corking the flask. After a few minutes the precipitate settles. Take out 50 c.c. of the clear portion, without filtering,* and titrate with normal hydrochloric acid. When employing methyl orange as indicator, the liquid must be cooled first and the titration must be made slowly, with constant shaking. Each cubic centimetre of the standard acid indicates 0.04006 g. of NaOH in 1 g. of black-ash = 0.03105 g. Na_2O , but sodium sulphide is also included.

(c) *Sodium Sulphide*.—Dilute 10 c.c. of solution to about 200 c.c., employing water freed from oxygen by boiling, acidulate with acetic acid, and titrate quickly with iodine solution, using starch as an indicator. When employing a decinormal iodine solution (12.697 g. I per litre), each cubic centimetre indicates 0.003908 g. Na_2S (= 0.003105 g. Na_2O). A solution containing 3.249 g. I per litre would indicate 0.001 g. Na_2S per cubic centimetre. In the former case the number of cubic centimetres of decinormal solution divided by 10 can be deducted at once from the acid employed in test No. 1, whereby the sulphide is eliminated from the alkali test. Other sulphur compounds (except sulphate) need not be taken account of in fresh black-ash.

(d) *Sodium Chloride*.—Neutralise 10 c.c. of the liquor as accurately as possible with nitric acid, preferably by adding exactly as many cubic centimetres of standard nitric acid (63.02 g. HNO_3 per litre) as had been employed in test No. 1. Boil till all H_2S has been expelled, filter from any sulphur precipitated, add a little neutral potassium chromate, and titrate with silver solution (as described p. 145). Each cubic centimetre of decinormal silver solution indicates 0.00585 g. NaCl . A solution containing 2.905 g. AgNO_3 per litre corresponds to 0.001 g. NaCl per cubic centimetre.

(e) *Sodium Sulphate*.—Acidulate 10 c.c. with a very slight excess of HCl , boil, add barium chloride, filter, wash, and ignite the precipitated BaSO_4 . Since the quantity is very small, it can be washed with hot water on the filter itself, which is then placed in the moist state in a platinum crucible and ignited. Each part of BaSO_4 = 0.6089 Na_2SO_4 .

(f) Prepare an average sample of all batches by pouring a certain quantity of the liquor belonging to each batch into a common vessel; carbonate this by passing CO_2 through it, filter, evaporate the filtrate to dryness, and estimate Na_2CO_3 , Na_2SO_4 , and NaCl in the residue.

* The filter paper absorbs an appreciable portion of barium salt.

C.—Tank Waste (Vat Waste).

Take a large, really representative, average sample, which should be kept protected from air, and of which 50 g. should be weighed out *quickly* and in the *moist* state. Drying in contact with air would considerably change its composition. Moist tank waste may be assumed, without any great error, to contain 40 per cent. of water. Digest the above 50 g. waste with 490 c.c. water of 40° C., which will yield 500 c.c. of liquid.

1. *Available Soda* (Na_2CO_3 , or Na_2S).—Take 100 c.c. of the liquor, pass into it a current of well-washed carbon dioxide, heat the liquid to boiling, bring up the volume again to 100 c.c., pour through a dry filter, and titrate 50 c.c. of the clear portion with decinormal hydrochloric acid, of which each c.c. will indicate 0.003105 g. Na_2O , or, in this case, 0.0621 per cent. Na_2O on the moist waste.

2. *Total Soda (inclusive of Insoluble Sodium Salts)*.—Heat 17.71 g.* tank waste in a porcelain or iron dish with sulphuric acid of specific gravity 1.5, till all has been decomposed and converted into a stiff paste, evaporate to dryness, heat till all free sulphuric acid has been driven off, add hot water, scrape out the mass, and put it into a 250 c.c. cylinder. Neutralise any free acid left, and precipitate any magnesia present by adding pure milk of lime (obtained from ordinary slaked lime by pouring off the first water, which may contain some alkali), fill up to the mark, allow to settle, take out 50 c.c. of the clear liquor, add 10 c.c. of saturated baryta water, pour the mixture through a dry filter, take 50 c.c. of the filtrate, precipitate all baryta by passing through the liquid CO_2 and boiling, filter, and titrate the filtrate with decinormal hydrochloric acid. Each cubic centimetre of this will indicate 0.1 per cent. of Na_2O in the waste, taking into account its bulk.

3. *Total and Oxidisable Sulphur*.—Boil 2 g. of the waste with hydrochloric acid, filter, wash with dilute HCl , neutralise the filtrate almost completely by adding sodium carbonate, precipitate with barium chloride, filter, wash, and ignite the barium sulphate. From this the sulphur present as sulphate is calculated (*a*). Another sample of 2 g. waste is oxidised by a strong bleaching-powder solution and hydrochloric acid, or by a solution of bromine in strong hydrochloric acid. When a strong smell of chlorine persists, all S is oxidised to sulphuric acid. Filter and estimate the SO_4H_2 in the filtrate. This indicates the total sulphur (*b*). The difference $b - a$ is the oxidisable sulphur, *i.e.*, the theoretically recoverable maximum of sulphur in the waste.

* This amount is correct, not 18.6 g., as calculation would seem to show, because an allowance must be made for the bulk of the insoluble residue in the measuring vessels.

D.—Tank Liquor (Vat Liquor).

Vat liquor is tested while hot, or else it is kept at about 40° C., to prevent crystallisation. Take out only small samples (2 to 5 c.c.) with an accurate pipette. This greatly facilitates the work.

1. *Sodium Carbonate*.—Titrate 2 c.c. with standard hydrochloric acid. When employing methyl orange as indicator, first add some cold water. From the volume required deduct that found in test No. 2 and one-tenth of that in test No. 3.

2. *Sodium Hydroxide* (estimated as on p. 166).

3. *Sodium Sulphide* is estimated by decinormal iodine solution (as on p. 166). The error caused by other sulphur compounds is hardly appreciable, and for practical purposes of no consequence. In any case this test must be made in order to correct test No. 1.

4. *Sodium Sulphate* (as on p. 166).

5. *Total Sulphur*.—Oxidise the liquor with bleaching powder and hydrochloric acid (as described C. 3, p. 167), and precipitate with barium chloride.

6. *Sodium Chloride* (as on p. 166).

7. *Sodium Ferrocyanide*.—Acidulate 20 c.c. of liquor (or more) with HCl, and add *strong* bleaching-powder solution from a burette, constantly agitating. From time to time mix a drop of the mixture on a white slab with a drop of dilute ferric chloride solution, free from ferrous chloride. When no more Prussian blue is formed, but the mixture of both drops turns brown, all is oxidised, hence also all ferrocyanide is turned into ferricyanide. A drop of bleach solution in excess does no harm, but if too much excess has been used, or if too much liquor has been lost by taking out test drops, a fresh sample is taken out, which can then be oxidised by running the requisite quantity of bleach liquor from the burette without losing much by making the drop-tests. This method gives quicker and more accurate results than adding an excess of bleach and driving out the chlorine by heating, in which case some ferricyanide may be decomposed. The oxidised liquor is titrated with decinormal copper solution, containing 3.18 g. Cu or 12.488 g. crystallised cupric sulphate per litre, which precipitates yellow $\text{Cu}_3\text{Fe}_3\text{Cy}_{12}$. From time to time test a drop of the liquid by bringing it together on a porcelain slab with a drop of a *dilute* ferrous sulphate solution. So long as a blue colour is produced by the action of FeSO_4 on Na_3FeCy_6 more copper solution is added, till the test on the slab does not turn blue or grey, but reddish. Now no more Na_3FeCy_6 is present, and the FeSO_4 on the slab reduces the yellow copper ferricyanide to red ferrocyanide. The first sensible reddening must be taken as the final reaction, although it vanishes after a short time. According to theory, each cubic centimetre of the copper solution ought to indicate 0.01013 g. Na_4FeCy_6 ; but direct experiments (*Chem. Ind.*, 1882, p. 79) have shown this not to be

the case. Too little copper solution is employed, and each cubic centimetre of this must therefore be regarded as equal to 0.0123 g. Na_3FeCy_6 , or, still better, the copper solution must be standardised by pure potassium ferrocyanide.

8. *Silica, Alumina, and Ferric Oxide (Parnell).*—Supersaturate 100 c.c. of liquor with HCl, boil, add a large quantity of ammonium chloride and ammonia in excess, and boil till all smell of NH_3 has ceased. The precipitate settles easily, and can be well washed. On washing with hot water it turns intensely blue (owing to the formation of Prussian blue?); on igniting it leaves SiO_2 , Al_2O_3 , and Fe_2O_3 .

9. A large sample of the liquor is carbonated by passing CO_2 through it; it is then filtered, evaporated to dryness, and the residue tested for available alkali, Na_2SO_4 and NaCl.

III.—Carbonated Liquor.

This is tested like tank liquor (No. D); also for bicarbonate. This is done with sufficient accuracy for practical purposes as follows. Titrate 10 c.c. of liquor, without diluting it, in the cold

with normal hydrochloric acid, employing phenolphthalein as indicator, until this is decolorised. The temperature should not be much above 0° . The c.c. of $\frac{n}{1}$ HCl used

= a . Now add a drop of methyl orange and more acid, until the colour changes; the c.c. $\frac{n}{1}$ HCl used for this = b . Then $b - a$ indicates the bicarbonate, $2a$ the soda present as Na_2CO_3 , $a + b$ the total soda. For other methods, see "Bicarbonate," p. 184.

The most accurate and at the same time the quickest method for estimating carbon dioxide, both in small and in large quantities, is that of Lunge and Rittener (*Z. angew. Chem.*, 1906, p. 1849). Their apparatus is shown in Fig. 15. The small flask B, holding about 30 c.c., is provided with a tap funnel C and a long capillary D, which is connected with the lateral capillary of the two-way tap E of the gas-burette A. D should be cut off at the lower surface of the rubber stopper of B. Introduce so much substance (solid or liquid) into B that it cannot yield more than 80

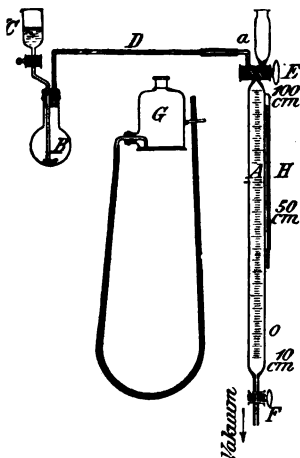


FIG. 15.

c.c. CO_2 ; also 15 c.c. of the finest aluminium wire, rolled up in a spiral. Then close B and connect D with tap E of burette A. This is an ordinary Bunte burette; as usual, it is divided in c.c., beginning below the tap E with 100, going downwards to B, then again to -10 c.c., leaving a few c.c. of undivided space down to the tap F. A level-bottle, G, can be connected with F in the ordinary manner; it contains a saturated solution of sodium chloride. At the beginning of the operation F is not connected with G, but with a water-pump which is turned on for two or three minutes, in order to evacuate the apparatus B-D-A. F is then closed and the capillary below this tap connected with the rubber tube of the level-bottle G. By cautiously opening F, a little of the salt solution is allowed to pass from G through F, till it appears just above this tap in the capillary space of A. This is done in order to check any leak at F.

If a solution is to be tested which is not previously contained in flask B, it is poured into funnel C, and by cautiously opening the tap it enters into B. Rinse C twice or thrice with a little water, and then introduce through C enough hydrochloric acid to decompose the carbonate and dissolve the aluminium wire. If B contains initially a solid substance or a solution, the acid is of course run in directly through C. In any case this is done drop by drop, to avoid a violent reaction. When it slackens, heat B gently, until the aluminium is dissolved, and then bring the solution to the boil, until drops of water condense in E. Now close E and allow water to enter through C, to completely fill the flask B and the capillary C. If a few small bubbles of gas should remain in C, they are transferred to A by cautiously opening E for a few moments. Next detach the capillary D from E, and wait twenty to twenty-five minutes, so that the gas in A is cooled down to the temperature of the outer air. Read the thermometer H, attached to the upper part of A by means of rubber rings, note also the barometer, cautiously open tap E, until the liquid in G and A stands at the same level, close F, and read the volume of gas in A, preferably by means of a Goeckel reading-screen.

Now run a solution of caustic soda (1 : 2 water) through E into A, without taking notice of any precipitation of calcium carbonate, which will take place in A, if a solution of impure common salt has been used in the level-bottle G. Close E, shake A, in order to promote the absorption of CO_2 , adjust the liquid in G and A to the same level, read off the volume in A, introduce more caustic soda solution until this causes no further contraction of the volume of gas.

The difference between the first reading a and that taken after absorption of the $\text{CO}_2 = b$ shows the volume of the CO_2 originally present, which is reduced to 0° and 760 mm. in the usual way. Of course regard must be had to the fact that the tension of a saturated NaCl solution is less than that of pure water; for ordinary temperatures it may be put = 80 per cent. of the tension

of pure water (Table 24, p. 55), so that, *e.g.*, at 15° C. it will be 12 mm. instead of 15 mm.

If you call the volumes of gas, reduced to the normal state, a_1 and b_1 and the weight (or volume) of substance employed n , its percentage of CO_2 is :—

$$\frac{0.19766(a^1 - b^1)}{n}$$

Instead of absorbing the CO_2 in the burette A, as described, it might be transferred, by raising G, into a Hempel's or Drehschmidt's absorption-pipette, attached to *a*. This pipette is filled with caustic soda solution. After the CO_2 has been absorbed, the remaining gas is retransferred to A, by raising G. E is then closed, the liquid adjusted to the same level in A and G, and the volume of the gas read and reduced to normal conditions as above.

F.—Mother Liquor.

This is tested like uncarbonated tank liquor, p. 168. But in this case it is necessary to estimate sulphide, sulphate, sulphite, and thiosulphate in the presence of one another. The most convenient method for this purpose is that of Lunge and Smith (*Chem. Ind.*, 1883, p. 301), which is as follows :—

(a) *Sulphate* is estimated by displacing the air in the flask by CO_2 (to prevent oxidation by air), heating, acidulating, and precipitating with BaCl_2 .

(b) *Other Compounds of Sulphur*.—In a second sample determine the consumption of decinormal iodine solution, after diluting with water free from air and acidulating with acetic acid.

(c) To a sample, four times the amount of (b), add zinc acetate or cadmium carbonate, in order to remove the Na_2S , dilute it to a known volume, allow to settle, and take a quarter of the clear liquid for each of the following tests :—

(1) The consumption of decinormal iodine = M.

(2) To another quarter add, without acidulating it, a large excess of permanganate solution of the value W (see below), the solution to be tested being run into the permanganate solution ; then an acid solution of ferrous sulphate, of known value against KMnO_4 , is added in excess, and the excess is titrated back by permanganate. The total permanganate solution used, less that corresponding to the ferrous sulphate, is called N.

(The value W signifies the quantity of permanganate solution used in accordance with the equation :—



which is found by calculation, or else experimentally by titration of pure sodium thiosulphate.)

If we call the sulphur of thiosulphate S, that of sulphate *s*, we have :—

$$S = \frac{1}{2}(8WN - 0.0064M)$$

$$s = 2WN - 2S.$$

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By deducting M from the result of the original iodine titration (b) you find the amount of Na_2S .

Another method for the same purpose, by Richardson and Ackroyd, has been published in *Journ. Soc. Chem. Ind.*, 1896, p. 172.

G.—Tables.

1. SPECIFIC GRAVITIES OF SOLUTIONS OF SODIUM CARBONATE AT 15° C.

Specific gravity.	Degrees Twaddell.	Degrees Baumé.	Per cent. by weight.		1 cubic metre contains kilog.	
			Na_2CO_3 .	Na_2CO_3 , 10 aq.	Na_2CO_3 .	Na_2CO_3 , 10 aq.
1·000	0	0	0·00	0·00	0·00	0·00
1·005	1	0·7	0·45	1·21	4·52	12·16
1·010	2	1·4	0·91	2·46	9·19	24·85
1·015	3	2·1	1·39	3·75	14·11	38·06
1·020	4	2·7	1·90	5·13	19·38	52·33
1·025	5	3·4	2·35	6·34	24·09	64·99
1·030	6	4·1	2·82	7·61	29·05	78·38
1·035	7	4·7	3·27	8·82	33·84	91·29
1·040	8	5·4	3·74	10·09	38·90	104·94
1·045	9	6·0	4·21	11·36	43·99	118·71
1·050	10	6·7	4·70	12·68	49·35	133·14
1·055	11	7·4	5·17	13·95	54·54	147·17
1·060	12	8·0	5·65	15·24	59·89	161·54
1·065	13	8·7	6·15	16·59	65·50	176·68
1·070	14	9·4	6·63	17·89	70·94	191·42
1·075	15	10·0	7·08	19·10	76·11	205·33
1·080	16	10·6	7·56	20·40	81·65	220·32
1·085	17	11·2	8·03	21·67	87·13	235·12
1·090	18	11·9	8·48	22·88	92·43	249·39
1·095	19	12·4	8·90	24·01	97·46	262·91
1·100	20	13·0	9·31	25·12	102·41	276·32
1·105	21	13·6	9·80	26·44	108·29	292·16
1·110	22	14·2	10·27	27·71	114·00	307·58
1·115	23	14·9	10·75	29·00	119·86	323·35
1·120	24	15·4	11·22	30·27	125·66	339·02
1·125	25	16·0	11·67	31·49	131·29	354·26
1·130	26	16·5	12·17	32·83	137·52	370·98
1·135	27	17·0	12·64	34·10	143·46	387·04
1·140	28	17·7	13·08	35·29	149·11	402·31
1·145	29	18·3	13·50	36·42	154·58	417·01
1·150	30	18·8	13·94	37·61	160·31	432·52
1·155	31	19·3	14·34	38·69	165·63	446·87

2. SPECIFIC GRAVITIES OF CONCENTRATED SOLUTIONS
OF SODIUM CARBONATE AT 30° C.*

Specific gravity at 30°.	Degrees Twaddell.	Degrees Baumé.	Per cent. by weight.		1 cubic metre contains kilog.	
			Na ₂ CO ₃ .	Na ₂ CO ₃ , 10 aq.	Na ₂ CO ₃ .	Na ₂ CO ₃ , 10 aq.
1.310	62	34.2	28.08	75.76	367.85	992.46
1.305	61	33.7	27.66	74.63	360.96	973.92
1.300	60	33.3	27.25	73.52	354.25	955.76
1.295	59	32.8	26.84	72.41	347.58	937.71
1.290	58	32.4	26.42	71.28	340.82	919.51
1.285	57	32.0	26.00	70.15	334.10	901.43
1.280	56	31.5	25.60	69.07	327.68	884.10
1.275	55	31.1	25.18	67.94	321.05	866.24
1.270	54	30.6	24.74	66.75	314.20	847.73
1.265	53	30.2	24.28	65.51	307.14	828.70
1.260	52	29.7	23.85	64.35	300.51	810.81
1.255	51	29.3	23.43	63.21	294.05	793.29
1.250	50	28.8	23.03	62.14	287.88	776.75
1.245	49	28.4	22.63	61.06	281.74	760.20
1.240	48	27.9	22.22	59.95	275.53	743.38
1.235	47	27.4	21.80	58.82	269.23	726.43
1.230	46	26.9	21.37	57.66	262.85	709.22
1.225	45	26.4	20.96	56.55	256.76	692.73
1.220	44	26.0	20.55	55.44	250.71	676.87
1.215	43	25.5	20.12	54.28	244.46	659.50
1.210	42	25.0	19.67	53.07	238.01	642.15
1.205	41	24.5	19.26	51.96	232.08	626.12
1.200	40	24.0	18.83	50.80	225.96	609.60
1.195	39	23.5	18.42	49.70	220.42	594.22
1.190	38	23.0	18.00	48.56	214.20	577.84
1.185	37	22.5	17.55	47.35	207.97	561.10
1.180	36	22.0	17.09	46.11	201.66	544.10
1.175	35	21.4	16.62	44.84	195.29	526.87
1.170	34	20.9	16.16	43.60	189.07	510.12
1.165	33	20.3	15.70	42.36	182.91	493.49
1.160	32	19.8	15.25	41.14	176.90	477.22
1.155	31	19.3	14.84	40.04	171.40	462.46
1.150	30	18.8	14.42	38.91	165.83	447.47
1.145	29	18.3	14.02	37.83	160.53	433.15
1.140	28	17.7	13.61	36.72	155.15	418.61

* This temperature has been specially chosen, because the higher concentrations of sodium carbonate cannot exist in solution at lower temperatures.

3. INFLUENCE OF TEMPERATURE ON THE SPECIFIC

0° C.	5°.	10°.	15°.	20°.	25°.	30°.	35°.	40°.	45°.	50°.
...	1·285	1·282	1·279	1·276	1·273
...	1·274	1·271	1·267	1·265	1·262
...	1·263	1·260	1·257	1·254	1·251
...	1·252	1·250	1·247	1·244	1·240
...	1·241	1·239	1·236	1·233	1·230
...	1·240	1·238	1·236	1·234	1·232	1·230	1·227	1·224
...	1·230	1·228	1·225	1·223	1·221	1·219	1·216	1·213
...	1·220	1·218	1·215	1·213	1·210	1·208	1·205	1·201
...	1·210	1·208	1·206	1·204	1·201	1·199	1·196	1·192
...	1·200	1·198	1·196	1·194	1·192	1·189	1·186	1·183
1·198	1·195	1·193	1·190	1·188	1·186	1·184	1·182	1·179	1·176	1·173
1·188	1·185	1·183	1·180	1·178	1·176	1·174	1·172	1·169	1·166	1·163
1·177	1·174	1·172	1·170	1·168	1·166	1·164	1·162	1·160	1·157	1·154
1·166	1·164	1·162	1·160	1·158	1·156	1·154	1·152	1·150	1·148	1·145
1·156	1·154	1·152	1·150	1·148	1·146	1·144	1·142	1·139	1·136	1·134
1·146	1·144	1·142	1·140	1·138	1·136	1·134	1·132	1·129	1·126	1·123
1·136	1·134	1·132	1·130	1·128	1·126	1·124	1·122	1·120	1·117	1·114
1·126	1·124	1·122	1·120	1·118	1·116	1·114	1·112	1·110	1·107	1·104
1·116	1·114	1·112	1·110	1·108	1·106	1·104	1·102	1·100	1·098	1·095
1·106	1·104	1·102	1·100	1·098	1·096	1·094	1·092	1·090	1·088	1·085
1·096	1·094	1·092	1·090	1·088	1·086	1·084	1·082	1·080	1·078	1·075
1·086	1·084	1·082	1·080	1·078	1·076	1·074	1·072	1·070	1·068	1·065
1·075	1·073	1·071	1·070	1·069	1·067	1·065	1·063	1·061	1·059	1·056
1·064	1·063	1·061	1·060	1·059	1·057	1·056	1·054	1·052	1·050	1·047
1·053	1·052	1·051	1·050	1·049	1·048	1·046	1·044	1·042	1·040	1·037
1·043	1·042	1·041	1·040	1·039	1·038	1·036	1·034	1·032	1·030	1·027
1·033	1·032	1·031	1·030	1·029	1·028	1·026	1·024	1·022	1·020	1·017
1·023	1·022	1·021	1·020	1·019	1·018	1·016	1·014	1·012	1·010	1·007
1·013	1·012	1·011	1·010	1·009	1·008	1·006	1·004	1·002	1·000	0·997

GRAVITIES OF SOLUTIONS OF SODIUM CARBONATE.

55°.	60°.	65°.	70°.	75°.	80°.	85°.	90°.	95°.	100°.
1·270	1·267	1·264	1·260	1·256	1·252	1·247	1·243	1·238	1·234
1·259	1·256	1·253	1·249	1·244	1·240	1·236	1·232	1·228	1·224
1·248	1·245	1·241	1·237	1·233	1·229	1·226	1·222	1·218	1·215
1·237	1·234	1·230	1·227	1·224	1·220	1·217	1·213	1·210	1·206
1·226	1·223	1·220	1·216	1·213	1·210	1·207	1·204	1·200	1·197
1·220	1·217	1·213	1·210	1·206	1·203	1·199	1·195	1·191	1·188
1·209	1·206	1·202	1·199	1·195	1·192	1·188	1·184	1·181	1·178
1·198	1·194	1·191	1·188	1·184	1·181	1·178	1·174	1·171	1·168
1·189	1·185	1·182	1·178	1·175	1·172	1·168	1·165	1·162	1·159
1·179	1·176	1·172	1·168	1·165	1·162	1·158	1·155	1·152	1·149
1·169	1·666	1·163	1·159	1·156	1·153	1·149	1·146	1·143	1·140
1·160	1·156	1·153	1·150	1·147	1·144	1·140	1·137	1·134	1·131
1·151	1·147	1·144	1·141	1·138	1·135	1·131	1·128	1·125	1·122
1·142	1·139	1·136	1·133	1·130	1·126	1·123	1·120	1·117	1·114
1·131	1·128	1·125	1·122	1·119	1·116	1·113	1·110	1·107	1·104
1·120	1·118	1·115	1·112	1·109	1·106	1·103	1·100	1·097	1·094
1·111	1·108	1·105	1·102	1·099	1·096	1·093	1·090	1·087	1·084
1·101	1·098	1·095	1·092	1·089	1·086	1·083	1·080	1·077	1·074
1·092	1·089	1·086	1·083	1·080	1·077	1·074	1·071	1·068	1·065
1·082	1·079	1·076	1·073	1·070	1·067	1·064	1·061	1·058	1·055
1·072	1·070	1·067	1·064	1·061	1·058	1·055	1·052	1·049	1·046
1·062	1·060	1·057	1·054	1·052	1·049	1·046	1·043	1·040	1·038
1·053	1·051	1·048	1·045	1·043	1·040	1·037	1·034	1·032	1·029
1·044	1·041	1·038	1·036	1·032	1·030	1·028	1·025	1·023	1·020
1·034	1·032	1·029	1·027	1·024	1·021	1·019	1·016	1·014	1·011
1·024	1·022	1·019	1·017	1·015	1·012	1·010	1·007	1·005	1·003
1·014	1·012	1·009	1·007	1·005	1·002	1·000	0·997	0·995	0·993
1·004	1·002	0·999	0·997	0·995	0·992	0·990	0·987	0·985	0·983
0·994	0·992	0·989	0·987	0·985	0·982	0·980	0·977	0·975	0·973

H.—Analysis of Commercial Soda Ash.

When merely the *available alkali* (alkalimetric degree) has to be ascertained, it is convenient to weigh out 15.5 g., to dissolve in a 500 c.c. flask, and to take for each test 50 c.c. (in Germany, without filtering; in England, sometimes with, sometimes without). In this case each cubic centimetre of standard acid indicates 0.03105 g. Na_2O , or just 2 per cent. of available alkali (Na_2O). The standard acid is normal hydrochloric acid, containing 36.46 g. HCl per litre, and standardised both with pure sodium carbonate and with silver nitrate. (*Cf. Appendix.*) The indicator is either litmus (in which case the solution has to be boiled for some time) or more conveniently methyl orange (which is used with cold solutions).

If the percentage of alkali is to be calculated in terms of Na_2CO_3 , as is usual in Germany and other countries, 2.6525 g. is weighed out, dissolved, and titrated (without filtering) with normal hydrochloric acid, each c.c. of which indicates 2 per cent. Na_2CO_3 in this case. In Germany the samples are ignited before weighing, and the percentage is always stated for soda ash in this dry state.

For a *complete* analysis of commercial soda ash 50 g. are dissolved in warm water.

1. *The Insoluble Residue* is filtered and washed, the filtrate and washings are diluted up to 1 litre, and the following tests are made with this solution.

2. *Sodium Carbonate* is found by titrating 20 c.c. (equal to 1 g. of soda ash) with normal HCl, deducting the amount of No. 3. That of No. 4 is always too small to consider in this case.

3. *Sodium Hydroxide* is estimated by barium chloride, according to p. 166.

4. *Sodium Sulphide*.—100 c.c. (equal to 5 g. of ash) are titrated with ammoniacal silver nitrate (*cf. Appendix*), containing 13.810 g. Ag per litre, and indicating 0.005 g. Na_2S per cubic centimetre. Heat the soda liquor to boiling, add ammonia, and run in the silver solution from a burette divided in $\frac{1}{10}$ c.c., till no further black precipitate of Ag_2S is produced. In order to observe this more accurately the liquid is filtered towards the end of the operation, and the titration is continued if necessary. This filtration is repeated several times. Each cubic centimetre of silver solution indicates 0.1 per cent. of Na_2S in the alkali.

5. *Sodium Sulphite*.—Acidulate 100 c.c. (equal to 5 g. soda ash) with acetic acid, add starch solution, and titrate with iodine till a blue colour appears. A decinormal iodine solution corre-

sponds to 0'006308 g. Na_2SO_3 per cubic centimetre (in this case 0'126 per cent.). The solution mentioned on p. 166, of 3'249 g. iodine per litre, corresponds to 0'001613 g. Na_2SO_3 (in this case 0'0323 per cent.). From this should be deducted the amount corresponding to test No. 4; 1 c.c. of the silver solution can be regarded as equal to 1'3 c.c. of the decinormal, or equal to 5'0 c.c. of the weaker iodine solution.

6. *Sodium Sulphate*.—Acidulate 20 c.c. of the solution (equal to 1 g. soda ash) with hydrochloric acid, precipitate with barium chloride, as on p. 110, and weigh the BaSO_4 , of which 1'000 part is equal to 0'6089 part Na_2SO_4 .

7. *Sodium Chloride*.—Neutralise 20 c.c. (equal to 1 g. soda ash) exactly with nitric acid, preferably by adding exactly as many cubic centimetres normal nitric acid from a burette as had been used in test No. 1; then add neutral potassium chromate, and titrate with decinormal silver nitrate as described on p. 145. Each cubic centimetre of this corresponds to 0'00585 g. NaCl .

8. *Iron*.—Neutralise 100 c.c. (equal to 5 g. soda ash) with sulphuric acid free from iron, reduce with zinc free from iron (p. 142), and titrate with $\frac{1}{10}$ normal potassium permanganate, of which each cubic centimetre corresponds to 0'002795 g. Fe , or in this case 0'056 per cent. Fe .

9. *Sodium Silicate* is not present in appreciable quantities in ordinary soda ash, but always in the ash recovered from the liquor used in the manufacture of wood "cellulose." It is estimated by acidulating 20 c.c. (equal to 1 g. soda ash) with HCl , filtering the SiO_2 , drying, and igniting. 1 g. $\text{SiO}_2 = 2'028$ g. Na_2SiO_3 .

10. *Table for Comparing French, German, and English Commercial Alkalimetric Degrees*.—The French or Descroizilles degrees mean the quantity of real sulphuric acid, SO_4H_2 , neutralised by 100 parts of soda ash. The German degrees express the available alkali in terms of sodium carbonate, Na_2CO_3 . In England some works invoice in real per cent. of soda, Na_2O , as found in the first column of the following tables. The Newcastle test is based on the equivalent 32 for Na_2O , or 59'26 degrees for pure Na_2CO_3 , and invoices fractions of degrees.

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FRENCH, GERMAN, AND ENGLISH COMMERCIAL
ALKALIMETRICAL DEGREES.

Real Soda. Na ₂ O.	German degrees. Na ₂ CO ₃ .	New-castle degrees.	French degrees.	Real Soda. Na ₂ O.	German degrees. Na ₂ CO ₃ .	New-castle degrees.	French degrees.
0·5	0·85	0·51	0·79	18	30·78	18·23	28·45
1	1·71	1·01	1·58	18·5	31·63	18·74	29·24
1·5	2·56	1·52	2·37	19	32·49	19·25	30·03
2	3·42	2·03	3·16	19·5	33·34	19·76	30·82
2·5	4·27	2·54	3·95	20	34·20	20·26	31·61
3	5·13	3·04	4·74	20·5	35·05	20·77	32·40
3·5	5·98	3·55	5·53	21	35·91	21·27	33·19
4	6·84	4·05	6·32	21·5	36·76	21·78	33·98
4·5	7·69	4·56	7·11	22	37·62	22·29	34·77
5	8·55	5·06	7·90	22·5	38·47	22·80	35·56
5·5	9·40	5·57	8·69	23	39·33	23·30	36·35
6	10·26	6·08	9·48	23·5	40·18	23·81	37·14
6·5	11·11	6·59	10·27	24	41·04	24·31	37·93
7	11·97	7·09	11·06	24·5	41·89	24·82	38·72
7·5	12·82	7·60	11·85	25	42·75	25·32	39·51
8	13·68	8·10	12·64	25·5	43·60	25·83	40·30
8·5	14·53	8·61	13·43	26	44·46	26·34	41·09
9	15·39	9·12	14·22	26·5	45·31	26·85	41·88
9·5	16·24	9·63	15·01	27	46·17	27·35	42·67
10	17·10	10·13	15·81	27·5	47·02	27·86	43·46
10·5	17·95	10·64	16·60	28	47·88	28·36	44·25
11	18·81	11·14	17·39	28·5	48·73	28·87	45·04
11·5	19·66	11·65	18·18	29	49·59	29·38	45·83
12	20·52	12·17	18·97	29·5	50·44	29·89	46·62
12·5	21·37	12·68	19·76	30	51·29	30·39	47·42
13	22·23	13·17	20·55	30·5	52·14	30·90	48·21
13·5	23·08	13·68	21·34	31	53·00	31·41	49·00
14	23·94	14·18	22·13	31·5	53·85	31·91	49·79
14·5	24·79	14·69	22·92	32	54·71	32·42	50·58
15	25·65	15·19	23·71	32·5	55·56	32·92	51·37
15·5	26·50	15·70	24·50	33	56·42	33·43	52·16
16	27·36	16·21	25·29	33·5	57·27	33·94	52·95
16·5	28·21	16·73	26·08	34	58·13	34·44	53·74
17	29·07	17·22	26·87	34·5	58·98	34·95	54·53
17·5	29·92	17·73	27·66	35	59·84	35·46	55·32

FRENCH, GERMAN, AND ENGLISH COMMERCIAL ALKALIMETRIICAL DEGREES—Continued.

Real Soda. Na ₂ O.	German degrees. Na ₂ CO ₃ .	New-castle degrees.	French degrees.	Real Soda. Na ₂ O.	German degrees. Na ₂ CO ₃ .	New-castle degrees.	French degrees.
35.5	60.69	35.96	56.11	53	90.61	53.70	83.77
36	61.55	36.47	56.90	53.5	91.47	54.20	84.56
36.5	62.40	36.98	57.69	54	92.32	54.71	85.35
37	63.26	37.48	58.48	54.5	93.18	55.22	86.14
37.5	64.11	37.98	59.27	55	94.03	55.72	86.93
38	64.97	38.50	60.06	55.5	94.89	56.23	87.72
38.5	65.82	39.00	60.85	56	95.74	56.74	88.52
39	66.68	39.51	61.64	56.5	96.60	57.24	89.31
39.5	67.53	40.02	62.43	57	97.45	57.75	90.10
40	68.39	40.52	63.22	57.5	98.31	58.26	90.89
40.5	69.24	41.03	64.01	58	99.16	58.76	91.68
41	70.10	41.54	64.81	58.5	100.02	59.27	92.47
41.5	70.95	42.04	65.60	59	100.87	59.77	93.26
42	71.81	42.55	66.39	59.5	101.73	60.28	94.05
42.5	72.66	43.06	67.18	60	102.58	60.79	94.84
43	73.52	43.57	67.97	60.5	103.44	61.30	95.63
43.5	74.37	44.07	68.76	61	104.30	61.80	96.42
44	75.23	44.58	69.55	61.5	105.15	62.31	97.21
44.5	76.08	45.08	70.34	62	106.01	62.82	98.00
45	76.94	45.69	71.13	62.5	106.86	63.32	98.79
45.5	77.80	46.10	71.92	63	107.72	63.83	99.58
46	78.66	46.60	72.71	63.5	108.57	64.33	100.37
46.5	79.51	47.11	73.50	64	109.43	64.84	101.16
47	80.37	47.62	74.29	64.5	110.28	65.35	101.95
47.5	81.22	48.12	75.08	65	111.14	65.85	102.74
48	82.07	48.63	75.87	65.5	111.99	66.36	103.53
48.5	82.93	49.14	76.66	66	112.85	66.87	104.32
49	83.78	49.64	77.45	66.5	113.70	67.37	105.11
49.5	84.64	50.15	78.24	67	114.56	67.88	105.90
50	85.48	50.66	79.03	67.5	115.41	68.39	106.69
50.5	86.34	51.16	79.82	68	116.27	68.89	107.48
51	87.19	51.67	80.61	68.5	117.12	69.40	108.27
51.5	88.05	52.18	81.40	69	117.98	69.91	109.06
52	88.90	52.68	82.19	69.5	118.83	70.41	109.85
52.5	89.76	53.19	82.98	70	119.69	70.92	110.64

FRENCH, GERMAN, AND ENGLISH COMMERCIAL ALKALIMETRIICAL DEGREES—*Continued.*

Real Soda. Na ₂ O.	German degrees. Na ₂ CO ₃ .	New-castle degrees.	French degrees.	Real Soda. Na ₂ O.	German degrees. Na ₂ CO ₃ .	New-castle degrees.	French degrees.
70·5	120·53	71·43	111·43	75·5	129·08	76·49	119·34
71	121·39	71·93	112·23	76	129·94	77·00	120·13
71·5	122·24	72·44	113·02	76·5	130·79	77·51	120·92
72	123·10	72·95	113·81	77	131·65	78·01	121·71
72·5	123·95	73·45	114·60	77·5	132·50	78·52	122·50
73	124·81	73·96	115·39				
73·5	125·66	74·47	116·18				
74	126·52	74·97	116·97				
74·5	127·37	75·48	117·76				
75	128·23	75·99	118·55				

I.—Sulphur Recovery (Chance Process).

1. *Estimation of Sulphur as Sulphides in Vat Waste.*—The apparatus consists of a small flask fitted with a stopcock funnel and outlet tube connected with two Mohr's potash bulbs, the first one being empty, the second containing a strong solution of caustic potash. (In lieu of Mohr's bulbs a tube of the shape shown in Fig. 8, p. 120 can be employed with great advantage.) It is preferable to connect the last potash bulb to an aspirator or Bunsen pump, to produce a slight vacuum. About 2 g. of vat waste are put into the flask, and a sufficient quantity of water is added. Then hydrochloric acid, diluted with its volume of water, is run in from the funnel gradually. After the decomposition has ceased, the solution is boiled, until the whole of the gases are displaced by steam, most of the steam condensing in the first empty potash bulbs. When enough steam has been produced to bring the first bulb of the second set, filled with potash solution, up to boiling, the tap of the funnel is opened, and the apparatus allowed to cool down. The potash solution is then transferred to a $\frac{1}{4}$ or $\frac{1}{2}$ litre flask, made up to the mark, an aliquot part taken, diluted with a large quantity of previously boiled water (free from air), neutralised with acetic acid, and titrated with decinormal iodine, each c.c. of which indicates 0·001603 g. S.

2. *Sulphur as Sulphide in Carbonated Mud.*—About 6 g. are taken for analysis; otherwise the test is conducted just like the preceding one.

3. *Sulphide-sulphur + Carbonic Acid in Vat Waste.*—This test

(which is only exceptionally made) is carried out in a small flask, fitted with stopcock funnel, connected with a U-tube containing sodium sulphate to absorb any traces of HCl passing over, and a sufficient number of chloride of calcium tubes to thoroughly dry the gases. To the last of these are connected two weighed potash bulbs containing a strong solution of caustic potash, followed by weighed CaCl_2 tubes. The whole apparatus being connected, 2 g. of vat waste are put into the flask, and some water added. A current of nitrogen is then passed through the apparatus to displace the air. [The nitrogen for this purpose is conveniently made by passing lime-kiln gases through a solution of caustic soda, then through a red-hot tube containing bright copper clippings to absorb any oxygen, and finally through solutions of caustic potash and barium hydroxide.] The vat waste is then decomposed by hydrochloric acid, and the contents of the flask boiled. Afterwards a current of nitrogen is passed through the apparatus for a considerable time to displace the H_2S and CO_2 in the flask and drying tubes. The potash bulbs and the last drying tubes are reweighed, the increase showing the amount of $\text{H}_2\text{S} + \text{CO}_2$ in the vat waste employed. The potash solution is then transferred to a measuring flask, and the H_2S estimated as described in 1. Deducting the amount from the increase of weight of the absorbing apparatus, we find the amount of CO_2 present.

4. *Sulphur as Sulphide in Solutions of Calcium or Sodium Sulphhydrates and Sulphides.*—10 c.c. are diluted to 250, and of this liquid a convenient portion is taken out, largely diluted with air-free water, acidulated with acetic acid, and titrated with iodine, as in test 1. If thiosulphates are present, they are estimated as in 5, and deducted. If polysulphides are present, the sulphur which would be precipitated by an acid is not estimated by this method, but only that which would be liberated as H_2S by an acid.

5. *Soda, Lime, and Thiosulphate in Sulphur Liquors.*—In one sample of the liquor, say 5 c.c., estimate the total alkalinity, *i.e.* $\text{Na}_2\text{O} + \text{CaO}$, by standard hydrochloric acid and methyl orange. Take another sample, say 50 c.c., pass pure CO_2 in till lead paper shows the absence of all sulphides, boil to decompose calcium bicarbonate, dilute with water to 500 c.c., allow the precipitate to settle, take 50 c.c. of the clear liquor and titrate again, the alkalinity this time being due to Na_2O only. CaO is found from the difference between the two titrations.

Another sample of the carbonated liquor is titrated with decinormal iodine for thiosulphate. Each c.c. of iodine solution indicates 0.006412 g. S as thiosulphate.

6. *Lime-kiln Gases.*— CO_2 is estimated by an Orsat apparatus, or a Honigmann burette, or any other similar apparatus. When using an Orsat apparatus, the test for oxygen can be made as on p. 98.

7. *Gas from Gas-holder.*

(a) *Hydrogen Sulphide + Carbon Dioxide* are estimated by an Orsat apparatus or a Honigmann burette, etc.

(b) *Hydrogen Sulphide Only.*—A wide-mouthed bottle of known capacity, holding about 500 c.c., is fitted with a rubber cork and two tubes, one nearly reaching to the bottom, the other ending just below the cork, both of them with stopcocks outside. Gas is passed through for some time, till it has entirely displaced the air in the bottle. Then 20 or 25 c.c. of standard potash solution is run in from a pipette, through one of the stopcocks, the bottle is well shaken, until the whole of the H_2S and CO_2 are absorbed, the contents of the bottle are poured into a measuring flask, the bottle is rinsed out completely, and the total liquid made up to the mark.

An aliquot portion is taken out, largely diluted with previously boiled water, acidified with acetic acid, and the H_2S estimated by iodine. In this case a solution of iodine is employed containing 11.43 g. I per litre, each c.c. of which indicates 1 c.c. of gaseous H_2S at 0° C. and 760 mm. pressure. For somewhat exact estimations, the temperature, pressure, and vapour tension have to be taken into account; but it is unnecessary to observe the thermometer and barometer, and to make any complicated calculations, if a Lunge's gas-volumeter be used (p. 139). In this case the level-tube, C, of the instrument is placed so that the mercury stands at the same height in C as in the reduction tube B; the height of mercury in the latter is read off, which gives the volume occupied by 100 c.c. of dry air of 0° and 760 mm. under the prevailing atmospheric conditions; the number of c.c. of iodine solution, multiplied by 100, is divided by this figure, and thus the correction of the normal volume effected.

8. *Exit Gases from the Claus Kilns.*—These contain SO_2 and H_2S . Both these gases, on being passed through iodine solution, produce 2HI for each atom of S; but whilst H_2S does not further increase the acidity of the solution, SO_2 produces its equivalent of H_2SO_4 . Hence SO_2 and H_2S are measured together by the amount of iodine converted into HI, and SO_2 by the acidity present after the HI has been saturated with caustic soda. Since the current of gases carries away some iodine from the decinormal solution, the gases must be passed through caustic soda, or, better, through sodium thiosulphate, to intercept this iodine. The manipulation is hence as follows: Aspirate one or more litres of the gases through 50 c.c. of decinormal iodine solution, contained in a bulb apparatus (Fig. 6, p. 104), or other efficient absorbing tubes, followed by another apparatus containing 50 c.c. of decinormal thiosulphate solution. Empty the contents of both apparatus into a beaker, and titrate with decinormal iodine and starch solution, till a blue colour appears. The number of c.c. of iodine solution used, if multiplied by 0.0016

g., indicates the total sulphur present as SO_2 and H_2S . Now add a drop of thiosulphate to discharge the blue colour, then a drop of methyl orange, and decinormal caustic soda from a burette, till the pink colour of the liquid is discharged. The number of c.c. of caustic soda used, less those of iodine used in the preceding test, multiplied by 0.0016, indicates the sulphur present as SO_2 .

VI. MANUFACTURE OF SODA BY THE AMMONIA PROCESS.

A.—Raw Materials.

1. *Rock Salt*, compare p. 145.

2. *Brine*.—The following determinations are made:—

(a) *Specific Gravity*, by the hydrometer.

(b) *Chlorine*, expressed as NaCl . Dilute 10 c.c. to 1 litre and titrate 10 c.c. of the diluted solution as on p. 145.

(c) *Sulphates*.—Dilute 50 c.c. brine to 150 or 200 c.c., add a little hydrochloric acid, and precipitate with barium chloride as on p. 110.

(d) *Ferric Oxide and Alumina*.—To 500 c.c. brine add a little nitric acid, heat to 80° , precipitate with an excess of ammonia, digest for half an hour at 80° , filter, and wash well. As a check, redissolve the precipitate in hydrochloric acid and reprecipitate it by ammonia.

In the filtrate *lime* and *magnesia* may be estimated as on p. 146.

(e) *Bicarbonates of Iron, Lime, and Magnesia*.—Destroy the bicarbonates as such by prolonged boiling of 500 c.c., replacing the water driven off, filter the precipitate formed, wash it, dissolve it in hydrochloric acid, and in the solution estimate the iron by precipitation with NH_3 , and lime and magnesia in the ordinary way.

3. *Concentrated Gas Liquor or Sulphate of Ammonia*, cf. Chapter XI., pp. 215 and 217.

4. *Limestone*, cf. p. 155.

5. *Quick Lime*, cf. p. 156.

6. *Coals or Coke*, cf. p. 95.

B.—Tests made during the Process of Manufacture.

1. *Ammoniacal Brine* from the receivers.

(a) *Sodium Chloride*.—Acidulate with nitric acid and estimate the NaCl by AgNO_3 gravimetrically, or volumetrically in the neutral or faintly alkaline solution as on p. 145.

(b) *Ammonia, free and combined*.—Dilute 10 c.c. to 100 c.c. and boil in a distilling flask until all the free ammonia and ammonium carbonate has been expelled; absorb this in a measured volume of normal sulphuric acid and titrate back. To the solution remaining in the flask add caustic soda solution, distil again, and absorb this "combined" ammonia also in sulphuric acid. Cf. Chapter XI., p. 215.

2. *Carbonators*.—Free and combined NH_3 are estimated as in No. 1 (b).

3. *Mother Liquor*.—Estimate:—

(a) NH_3 , free and combined, as above.

(b) Undecomposed NaCl , by evaporating 10 c.c. in a platinum dish, heating till all NH_4Cl is expelled, and weighing.

4. *Crude Bicarbonate*.—Estimate:—

(a) *The Alkalimetric Degree*, as on p. 165.

(b) CO_2 , as on p. 169.

(c) Moisture, by igniting and allowing for the CO_2 present as bicarbonate and found in (b).

5. *Distillation of Ammonia*.—

(a) NH_3 , free and combined, in the mother liquor as in No. 1 (b).

(b) Milk of lime as on p. 157.

(c) Excess of lime in the stills. Boil 100 c.c. until all NH_3 has been expelled, add a little ammonium sulphate and boil again. The NH_3 now set free, which corresponds to the excess of lime, is absorbed in standard sulphuric acid and titrated.

6. *Lime-Kiln Gases*.—Estimate the CO_2 as on p. 97.

C.—Commercial Products.

1. *Soda ash*, as on p. 176.

2. *Commercial Bicarbonate* is tested like the crude, No. 1, or very accurately by heating in an air-bath to 270° and receiving the gas in a Lunge's gas-volumeter, p. 139 (compare Lunge, *Z. angew. Chem.*, 1897, p. 522).

VII. CAUSTIC SODA.

A.—Caustic Liquor.

(a) Test for *available alkali and sodium carbonate* (as described p. 165). An exact estimation of CO_2 , which is rarely necessary in this case, could be made by expelling it with dilute sulphuric acid, and absorbing it in soda lime, or, preferably, by Lunge and Rittener's method, p. 169.

(b) SPECIFIC GRAVITIES OF SOLUTIONS OF SODIUM HYDROXIDE AT 15° C.

Specific Gravity.	Degrees Twaddell.	Degrees Baumé.	Per cent. Na ₂ O.	Per cent. NaOH.	1 cb.m. contains kg.	
					Na ₂ O.	NaOH.
1·000	0	0	0	0·00	0	0
1·005	1	0·7	0·33	0·43	3·31	4·32
1·010	2	1·4	0·67	0·86	6·77	8·69
1·015	3	2·1	0·99	1·28	10·05	12·99
1·020	4	2·7	1·31	1·69	13·36	17·24
1·025	5	3·4	1·65	2·13	16·91	21·83
1·030	6	4·1	2·02	2·60	20·81	26·78
1·035	7	4·7	2·37	3·06	24·53	31·67
1·040	8	5·4	2·71	3·50	28·18	36·40
1·045	9	6·0	3·02	3·90	31·56	40·76
1·050	10	6·7	3·36	4·34	35·28	45·57
1·055	11	7·4	3·69	4·76	38·98	50·22
1·060	12	8·0	4·08	5·20	42·72	55·12
1·065	13	8·7	4·39	5·67	46·75	60·39
1·070	14	9·4	4·75	6·13	50·83	65·59
1·075	15	10·0	5·10	6·58	54·83	70·74
1·080	16	10·6	5·46	7·05	58·97	76·14
1·085	17	11·2	5·81	7·50	63·04	81·38
1·090	18	11·9	6·16	7·95	67·14	86·66
1·095	19	12·4	6·50	8·39	71·18	91·87
1·100	20	13·0	6·81	8·78	74·91	96·58
1·105	21	13·6	7·15	9·23	79·01	101·99
1·110	22	14·2	7·50	9·67	83·25	107·34
1·115	23	14·9	7·84	10·12	87·42	112·84
1·120	24	15·4	8·18	10·56	91·62	118·27
1·125	25	16·0	8·57	11·06	96·41	124·43
1·130	26	16·5	8·95	11·55	101·14	130·52
1·135	27	17·0	9·32	12·02	105·78	136·43
1·140	28	17·7	9·68	12·49	110·35	142·39
1·145	29	18·3	10·03	12·94	114·84	148·16
1·150	30	18·8	10·34	13·34	118·91	153·41
1·155	31	19·3	10·67	13·76	123·24	158·93
1·160	32	19·8	11·00	14·19	127·60	164·60
1·165	33	20·3	11·33	14·62	131·99	170·32
1·170	34	20·9	11·67	15·06	136·54	176·20
1·175	35	21·4	12·04	15·53	141·47	182·48
1·180	36	22·0	12·40	16·00	146·32	188·80
1·185	37	22·5	12·75	16·45	151·09	194·93
1·190	38	23·0	13·11	16·91	156·01	201·23
1·195	39	23·5	13·46	17·36	160·85	207·45
1·200	40	24·0	13·80	17·81	165·60	213·72
1·205	41	24·5	14·15	18·26	170·51	220·03

(b) SPECIFIC GRAVITIES OF SOLUTIONS OF SODIUM HYDROXIDE AT 15° C.—*Continued.*

Specific Gravity.	Degrees Twaddell.	Degrees Baumé.	Per cent. Na ₂ O.	Per cent. NaOH.	1 cb.m. contains kg.	
					Na ₂ O.	NaOH.
1·210	42	25·0	14·50	18·71	175·45	226·39
1·215	43	25·5	14·87	19·18	180·67	233·04
1·220	44	26·0	15·23	19·65	185·81	239·73
1·225	45	26·4	15·59	20·12	190·98	246·47
1·230	46	26·9	15·97	20·60	196·43	253·38
1·235	47	27·4	16·30	21·03	201·31	259·72
1·240	48	27·9	16·64	21·47	206·34	266·23
1·245	49	28·4	16·97	21·90	211·28	272·66
1·250	50	28·8	17·31	22·33	216·38	279·13
1·255	51	29·3	17·65	22·77	221·51	285·76
1·260	52	29·7	18·01	23·23	226·93	292·70
1·265	53	30·2	18·35	23·68	232·13	299·55
1·270	54	30·6	18·70	24·13	237·62	306·45
1·275	55	31·1	19·05	24·58	242·89	313·40
1·280	56	31·5	19·41	25·04	248·45	320·51
1·285	57	32·0	19·77	25·50	254·04	327·68
1·290	58	32·4	20·12	25·96	259·55	334·88
1·295	59	32·8	20·47	26·41	265·09	342·01
1·300	60	33·3	20·81	26·85	270·53	349·05
1·305	61	33·7	21·20	27·35	276·66	356·92
1·310	62	34·2	21·59	27·85	282·83	364·33
1·315	63	34·6	21·97	28·34	288·91	372·67
1·320	64	35·0	22·35	28·83	295·02	380·56
1·325	65	35·4	22·73	29·32	301·17	388·40
1·330	66	35·8	23·10	29·80	307·23	396·34
1·335	67	36·2	23·47	30·28	313·32	404·24
1·340	68	36·6	23·83	30·74	319·32	411·92
1·345	69	37·0	24·18	31·20	325·22	419·64
1·350	70	37·4	24·61	31·75	332·24	428·63
1·355	71	37·8	25·02	32·28	339·02	437·39
1·360	72	38·2	25·42	32·79	345·71	445·94
1·365	73	38·6	25·78	33·26	351·90	454·00
1·370	74	39·0	26·14	33·73	358·12	462·10
1·375	75	39·4	26·52	34·22	364·65	470·53
1·380	76	39·8	26·90	34·71	371·22	479·00
1·385	77	40·1	27·28	35·20	377·83	487·52
1·390	78	40·5	27·66	35·68	384·47	496·95
1·395	79	40·8	28·02	36·15	390·88	504·29
1·400	80	41·2	28·42	36·67	397·88	513·38
1·405	81	41·6	28·81	37·17	404·78	522·24
1·410	82	42·0	29·18	37·65	411·44	530·87
1·415	83	42·3	29·58	38·16	418·56	539·96

(b) SPECIFIC GRAVITIES OF SOLUTIONS OF SODIUM HYDROXIDE AT 15° C.—Continued.

Specific Gravity.	Degrees Twaddell.	Degrees Baumé.	Per cent. Na ₂ O.	Per cent. NaOH.	1 cb.m. contains kg.	
					Na ₂ O.	NaOH.
1.420	84	42.7	29.97	38.67	425.57	549.11
1.425	85	43.1	30.36	39.17	432.63	558.17
1.430	86	43.4	30.75	39.67	439.72	567.28
1.435	87	43.8	31.14	40.18	446.86	576.58
1.440	88	44.1	31.53	40.68	454.03	585.79
1.445	89	44.4	31.93	41.20	461.39	595.34
1.450	90	44.8	32.32	41.70	468.64	604.65
1.455	91	45.1	32.72	42.22	476.07	614.30
1.460	92	45.4	33.14	42.75	483.84	624.15
1.465	93	45.8	33.54	43.27	491.36	633.91
1.470	94	46.1	33.95	43.80	499.07	643.86
1.475	95	46.4	34.36	44.33	506.81	653.87
1.480	96	46.8	34.76	44.85	514.45	663.78
1.485	97	47.1	35.17	45.37	522.27	673.74
1.490	98	47.4	35.57	45.89	529.99	683.76
1.495	99	47.8	35.98	46.42	537.90	693.98
1.500	100	48.1	36.38	46.94	545.70	704.10
1.505	101	48.4	36.79	47.47	553.69	714.42
1.510	102	48.7	37.20	48.00	561.72	724.80
1.515	103	49.0	37.61	48.53	569.79	735.23
1.520	104	49.4	38.02	49.05	577.90	745.56
1.525	105	49.7	38.42	49.58	585.91	756.10
1.530	106	50.0	38.83	50.10	594.10	766.53

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(c) INFLUENCE OF TEMPERATURE ON THE SPECIFIC

0° C.	5°.	10°.	15°.	20°.	25°.	30°.	35°.	40°.	45°.	50°.
1·867	1·864	1·862	1·860	1·857	1·855	1·853	1·850	1·848	1·845	1·842
1·857	1·854	1·852	1·850	1·847	1·845	1·843	1·840	1·837	1·835	1·832
1·847	1·844	1·842	1·840	1·838	1·835	1·833	1·830	1·827	1·825	1·822
1·838	1·835	1·832	1·830	1·828	1·825	1·823	1·820	1·817	1·815	1·812
1·828	1·825	1·822	1·820	1·818	1·815	1·813	1·810	1·807	1·805	1·802
1·818	1·815	1·813	1·810	1·808	1·805	1·803	1·800	1·297	1·294	1·292
1·808	1·805	1·803	1·800	1·297	1·294	1·292	1·289	1·287	1·284	1·282
1·298	1·295	1·293	1·290	1·287	1·284	1·282	1·279	1·277	1·274	1·272
1·288	1·285	1·283	1·280	1·277	1·274	1·272	1·269	1·267	1·264	1·262
1·278	1·275	1·273	1·270	1·267	1·265	1·262	1·260	1·258	1·255	1·252
1·268	1·265	1·263	1·260	1·257	1·255	1·252	1·250	1·248	1·245	1·242
1·257	1·255	1·252	1·250	1·247	1·245	1·242	1·240	1·238	1·235	1·232
1·247	1·245	1·242	1·240	1·237	1·235	1·232	1·230	1·228	1·225	1·222
1·237	1·235	1·232	1·230	1·227	1·224	1·222	1·220	1·218	1·215	1·212
1·227	1·225	1·222	1·220	1·217	1·214	1·212	1·210	1·208	1·205	1·202
1·217	1·215	1·212	1·210	1·207	1·204	1·203	1·200	1·198	1·196	1·192
1·207	1·205	1·202	1·200	1·197	1·195	1·193	1·190	1·188	1·186	1·184
1·197	1·195	1·192	1·190	1·187	1·185	1·183	1·180	1·178	1·176	1·174
1·187	1·185	1·182	1·180	1·177	1·175	1·173	1·170	1·168	1·166	1·164
1·176	1·174	1·172	1·170	1·167	1·165	1·163	1·161	1·158	1·156	1·154
1·166	1·164	1·162	1·160	1·157	1·155	1·153	1·151	1·148	1·146	1·144
1·156	1·154	1·152	1·150	1·148	1·146	1·144	1·142	1·140	1·137	1·135
1·146	1·144	1·142	1·140	1·138	1·136	1·134	1·132	1·130	1·127	1·125
1·136	1·134	1·132	1·130	1·128	1·126	1·124	1·122	1·120	1·118	1·116
1·126	1·124	1·122	1·120	1·118	1·116	1·114	1·112	1·110	1·108	1·106
1·116	1·114	1·112	1·110	1·108	1·106	1·104	1·102	1·100	1·099	1·097
1·105	1·103	1·102	1·100	1·098	1·096	1·095	1·093	1·092	1·090	1·087
1·094	1·093	1·091	1·090	1·088	1·087	1·086	1·084	1·082	1·080	1·078
1·084	1·083	1·081	1·080	1·078	1·077	1·076	1·074	1·072	1·070	1·068
1·074	1·073	1·071	1·070	1·068	1·067	1·066	1·064	1·062	1·060	1·058
1·064	1·063	1·061	1·060	1·058	1·057	1·056	1·054	1·052	1·050	1·048
1·054	1·053	1·051	1·050	1·048	1·047	1·046	1·044	1·042	1·040	1·038
1·044	1·043	1·041	1·040	1·038	1·037	1·036	1·034	1·032	1·030	1·028
1·034	1·033	1·031	1·030	1·028	1·027	1·026	1·024	1·022	1·020	1·018
1·024	1·023	1·021	1·020	1·018	1·017	1·016	1·014	1·012	1·010	1·008
1·014	1·013	1·011	1·010	1·008	1·007	1·006	1·004	1·002	1·000	0·998

GRAVITIES OF SOLUTIONS OF CAUSTIC SODA.

55°.	60°.	65°.	70°.	75°.	80°.	85°.	90°.	95°.	100°.
1·839	1·836	1·838	1·831	1·828	1·826	1·823	1·821	1·818	1·816
1·830	1·827	1·824	1·822	1·819	1·816	1·814	1·811	1·808	1·806
1·820	1·817	1·814	1·812	1·809	1·806	1·804	1·801	1·298	1·296
1·810	1·807	1·804	1·802	1·299	1·296	1·294	1·291	1·288	1·286
1·800	1·297	1·294	1·292	1·289	1·286	1·283	1·280	1·277	1·274
1·289	1·286	1·284	1·281	1·278	1·275	1·272	1·269	1·266	1·263
1·279	1·276	1·274	1·271	1·268	1·265	1·262	1·259	1·256	1·253
1·269	1·266	1·264	1·261	1·258	1·255	1·252	1·249	1·245	1·242
1·259	1·256	1·254	1·251	1·248	1·245	1·242	1·239	1·235	1·232
1·250	1·247	1·245	1·242	1·239	1·236	1·233	1·231	1·228	1·225
1·240	1·237	1·235	1·232	1·229	1·226	1·223	1·221	1·218	1·215
1·231	1·228	1·226	1·223	1·220	1·218	1·215	1·213	1·209	1·207
1·221	1·218	1·216	1·213	1·210	1·208	1·205	1·203	1·200	1·197
1·210	1·208	1·206	1·203	1·200	1·198	1·195	1·192	1·190	1·187
1·200	1·198	1·195	1·192	1·190	1·188	1·185	1·182	1·180	1·177
1·191	1·189	1·186	1·184	1·181	1·179	1·176	1·173	1·171	1·168
1·182	1·180	1·177	1·175	1·172	1·169	1·166	1·163	1·161	1·158
1·172	1·169	1·166	1·164	1·161	1·158	1·155	1·153	1·150	1·147
1·162	1·159	1·156	1·153	1·151	1·148	1·145	1·143	1·140	1·137
1·152	1·149	1·146	1·143	1·140	1·138	1·135	1·132	1·130	1·127
1·142	1·139	1·136	1·133	1·130	1·128	1·125	1·122	1·120	1·117
1·132	1·130	1·127	1·124	1·121	1·118	1·116	1·113	1·110	1·107
1·122	1·120	1·117	1·114	1·111	1·108	1·106	1·103	1·100	1·097
1·113	1·110	1·107	1·104	1·101	1·099	1·096	1·093	1·090	1·087
1·103	1·100	1·097	1·094	1·092	1·089	1·086	1·083	1·080	1·077
1·094	1·091	1·089	1·086	1·083	1·080	1·077	1·074	1·071	1·068
1·084	1·082	1·079	1·076	1·073	1·070	1·067	1·064	1·061	1·058
1·075	1·073	1·070	1·067	1·064	1·061	1·058	1·055	1·052	1·048
1·066	1·063	1·060	1·057	1·054	1·051	1·048	1·045	1·043	1·040
1·056	1·053	1·050	1·047	1·044	1·042	1·039	1·036	1·033	1·030
1·046	1·043	1·040	1·037	1·034	1·032	1·029	1·026	1·023	1·020
1·036	1·033	1·030	1·027	1·024	1·021	1·019	1·016	1·013	1·010
1·026	1·023	1·020	1·017	1·014	1·011	1·009	1·006	1·003	1·000
1·016	1·013	1·010	1·007	1·004	1·001	0·999	0·996	0·993	0·990
1·006	1·003	1·000	0·997	0·994	0·991	0·989	0·986	0·983	0·980
0·996	0·993	0·990	0·987	0·984	0·981	0·979	0·976	0·973	0·970

B.—Lime Mud.

(a) *Sodium as Carbonate and Hydroxide.*—Evaporate to dryness with addition of ammonium carbonate (in order to decompose the insoluble sodium compounds), repeat this, digest with hot water, filter, wash, and test the filtrate for alkali. The soda may have been originally present as NaOH or as Na_2CO_3 . It is expressed in terms of Na_2O (0.03105 g. per cubic centimetre of normal acid).

(b) *Caustic Lime.*—Titrate as described (p. 156) with normal hydrochloric acid and phenolphthalein. This indicates NaOH as well, for which half of the amount found in test (a) may be assumed without any serious error.

(c) *Calcium Carbonate.*—Titrate with normal hydrochloric acid and methyl orange, deduct from the cubic centimetres required those required in tests (a) and (b).

C.—Fished Salts.

Dissolve 50 g. in 1 litre of water, and take 50 c.c. of the solution for each test.

(a) *Available Alkali* is tested for with normal hydrochloric acid.

(b) *Sodium Chloride.*—Neutralise with nitric acid, preferably running normal acid out of a burette, and proceed in other respects as described on p. 166.

(c) *Sodium Sulphate.*—Add a slight excess of hydrochloric acid, precipitate with barium chloride, and weigh the BaSO_4 (p. 110).

(d) *Sodium Sulphite, Thiosulphate, etc.*—Add an excess of bleaching-powder solution, then hydrochloric acid, till the reaction is acid, and a smell of chlorine is produced (p. 167); precipitate with BaCl_2 , weigh the BaSO_4 , and deduct the amount found in test (c). The remainder is calculated as " Na_2SO_4 from oxidisable sulphur compounds."

D.—Caustic Bottoms.

Dissolve 10 g. in water, and filter. The washed residue is dried and ignited, and yields:—

(a) *Insoluble Matter.*—If necessary, the contained iron is estimated by dissolving in concentrated hydrochloric acid, reducing with zinc, adding manganous sulphate, and titrating with permanganate as on p. 113.

(b) *Available Alkali* is estimated in the aqueous solutions by normal hydrochloric acid, using litmus or lacmoid as indicator. (Methyl orange is not available in this case, owing to the presence of alumina.)

(c) *Sodium Carbonate* is estimated as in commercial soda ash (p. 176).

E.—Commercial Caustic Soda.

The sample must be very carefully taken. (Cf. Appendix.) The single pieces must be freed from the outer crust by scraping it off, before weighing. Dissolve 50 g. of the prepared sample in 1 litre of water, and take aliquot portions for each of the following tests with a pipette.

(a) *Available Alkali* is tested in at least 20 c.c. (equal to 1 g.) with normal HCl. If the caustic soda contains more than traces of alumina, methyl orange cannot be used as indicator, but litmus or lacmoid should be employed. In the case of strong caustic this is unnecessary.

(b) *Sodium Carbonate* is estimated by expelling the CO_2 with dilute sulphuric acid, and absorbing it in soda lime (the pumice saturated with cupric sulphate is left out here), or by Lunge and Rittener's process, p. 169. The quantity of CO_2 being so small, any estimation by difference yields unsatisfactory results. Very approximate results can, however, be obtained by titrating first with phenolphthalein till the pink colour is discharged (when all Na_2CO_3 will have been changed into NaHCO_3), noting the amount of standard acid used, adding methyl orange and more standard acid till the pink colour appears. The acid used in the second test $\times 2$ indicates Na_2CO_3 .

(c) *The Table for Comparing English, French, and German Degrees* is given on pp. 178 to 180.

VIII. ELECTROLYTIC ALKALI LIQUORS.

These are analysed just like bleach liquor, p. 162.

1. *Hypochlorites* are titrated as on p. 157.

2. *Free Hypochlorous Acid*.—Estimate the bleaching chlorine as in No. 1, then chloride, chlorate, and other acids on the one hand, and all bases on the other; the acidity in excess represents free HOCl.

3. *Chlorate* may be estimated as on p. 162, but since there is but little chlorate in presence of much hypochlorite, it is prefer-

able to use the direct method of Fresenius, as follows:—To the solution add an excess of neutral lead acetate solution; this produces a precipitate which gradually turns brown, and which contains a quantity of PbO_2 , corresponding to the chlorate. Allow to stand for eight or ten hours, until there is no more smell of chlorine, filter, wash, evaporate the filtrate to a small volume, precipitate lead and lime by means of a little sodium carbonate, and estimate the chlorate in the filtrate according to p. 162.

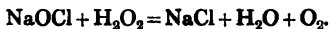
In mixtures of chlorate and hypochlorite, containing large quantities of the latter, Ditz and Knöpfelmacher estimate the chlorate iodometrically, by decomposing it at the ordinary temperature with concentrated hydrochloric acid and potassium bromide. Put the substance, together with a sufficient excess of KBr , into a small flask provided with a hollow glass stopper with dropping funnel and lateral absorbing vessel for the retention of bromine vapours. The latter is charged with 10 c.c. of a 5 per cent. solution of KI . Pour 50 c.c. concentrated hydrochloric acid through the dropping funnel into the flask, allow it to act for an hour, pour in 300 c.c. water, then 20 c.c. of the solution of KI , shake well, transfer the contents of the absorbing vessel to the flask, and titrate the iodine which has been set free by thiosulphate. The quantity of chlorate + hypochlorite is thus ascertained. When there is very much of the latter present, it should be removed beforehand.

4. *Chloride*.—Employ the solution from No. 1, in which all hypochlorite has been converted into chloride, with formation of sodium arsenate, which is an excellent indicator for the titration of the total chlorides by silver nitrate, p. 146, making *no* deduction for any excess of silver nitrate required to produce the colour. From the quantity of chloride thus found, deduct that which corresponds to the hypochlorite.

5. *Carbon Dioxide*.—Destroy the hypochlorite by boiling with liquor ammoniæ, free from CO_2 , expel the CO_2 by a strong acid, and estimate it as on p. 169.

6. *Bases*.—Convert these into sulphates, by evaporation with sulphuric acid, and estimate them in the residue by the ordinary methods.

7. *Free Alkali*.—Add to the solution a little of Merck's chemically pure hydrogen peroxide, which reacts as follows with the hypochlorite:—



$NaOH$ and Na_2CO_3 remain unchanged in solution, and are titrated as on p. 165.

In regard to the estimation of carbon dioxide in electrolytic chlorine gas, see p. 161.

IX. NITRIC ACID MANUFACTURE.**A.—Commercial Nitrate of Soda.**

According to the custom of the trade, which has held for many years, no direct estimation of the nitrate is made in the commercial nitrate of soda exported from Chili. The rule is, to estimate moisture, sodium chloride, sodium sulphate, and insoluble substances. The sum of these impurities is called the "refraction," and everything else is assumed to be real nitrate of soda. But as Chili saltpetre sometimes contains potassium nitrate (in which the percentage of NO_3 is less than that of NaNO_3), errors up to 1 per cent. NaNO_3 or even more may be caused by this indirect method of testing. Therefore, besides the above estimations, it ought to be insisted upon to estimate the potassium present and to calculate the results accordingly, or even better, to estimate the nitric-nitrogen directly.

The *sampling* ought to be done very carefully, since especially the amount of moisture may vary considerably in different parts of a cargo, and the reduction of the large sample to a smaller bulk ought to yield a really representative average sample.

1. *Moisture*.—Heat 10 g. or more of a good average sample in a small glass or porcelain dish to 130° for four or five hours, till the weight is constant.

2. *Insoluble*.—Dissolve 10 g. in water, filter, wash, and ignite. If there is a very appreciable quantity of organic matter present, first dry at 100°C . and weigh the filter with the precipitate before igniting it. The solution is used for the tests Nos. 4 to 6.

3. *Sodium Nitrate*.—In order to obtain a really representative sample, take about 20 g. of the carefully taken, large, average sample, dry this at 110° , grind it very finely, mix it thoroughly, and use it for the estimation of nitrate, etc. For the nitrate test, weigh out about 0.35 g. (that is, a quantity which will yield between 100 and 120 c.c. NO at the ordinary temperature and barometric pressure) in a narrow weighing-tube. Pour its contents as completely as possible into the decomposition vessel D of the gas-volumeter, Fig. 9, p. 139, so that the substance gets as much as possible to the bottom of the beaker of D. Weigh the weighing-tube again, with the small quantity of nitrate still adhering to it, so as to ascertain the weight of nitrate taken = a , in D. The three-way cock must be closed. Now run in 0.5 c.c. water, wait until the nitrate has been entirely or nearly all dissolved, draw the solution with any small crystals into the inside

of D, by lowering the level-tube E and cautiously opening the tap, rinse the beaker with $\frac{1}{2}$ or at most 1 c.c. water, and then allow 15 c.c. of pure concentrated sulphuric acid to enter in the same way. (It is important not to employ more than 1.5 c.c. water in all to 15 c.c. of strong acid, for if the acid is too much diluted, a froth of basic mercuric sulphate is formed which prevents an exact reading of the volume. On the other hand, the addition of a little water to the strong acid prevents the solution of an appreciable quantity of NO in the liquid.)

The reaction is finished by vigorous shaking of the acid solution with the mercury (as in the ordinary nitrometer, p. 136). During this period the level-tube should be roughly put into position, to avoid any considerable differences of pressure and possible leakages through the tap. When the agitating has been finished, wait half an hour for cooling. Then connect tube *c* of vessel D (Fig. 9, p. 139) with tube *e* of the measuring tube A, so that glass touches glass, as described p. 140, and transfer all the gas to A, by raising E and lowering C, but not allowing any acid to get into A. Then shut both taps, and by adjusting the tubes A, B, C in the manner described, p. 140, compress the gas volume to that corresponding to 0° and 760 mm. pressure.

Of course it is also possible to employ, in lieu of the gas-volumeter, an ordinary nitrometer, that is to leave out the "reduction-tube" B. In this case the volume of NO is read off under the prevailing atmospheric pressure, by adjusting the level-tube accordingly; the volume of NO is then reduced to 0° and 760 mm. by reading the thermometer and barometer, and employing the Tables 20, I. and II., pp. 38 *et seq.* The reduced volume of NO we call *x*. Each c.c. of it corresponds to 0.0037986 g. NaNO₃ (compare the table, p. 138); the whole, divided by the weight of the nitrate employed *a* and multiplied by 100, indicates the percentage of real nitrate; that is:—

$$\frac{0.37986x}{a}$$

(*N.B.*—The nitrometer should be tested whether it really contains exactly 100 c.c. to the mark 100, by inverting it, filling in mercury to the mark 100, running it off, and weighing. It should weigh 1360 g. reduced to 0°, or 1356 g. at 15° C. If there is an error, this must be allowed for in each reading.)

4. *Sodium Sulphate* is estimated in the solution No. 2 by precipitation with BaCl₂ and weighing the BaSO₄. (*Cf.* pp. 110 and 146.)

5. *Sodium Chloride* is titrated with silver nitrate. (*Cf.* p. 145.)

6. *Iodine* is detected by reducing the iodic acid with zinc, heating the solution with concentrated sulphuric acid, which liberates the iodine, diluting and agitating with carbon disulphide, which

takes up the iodine, and is thereby coloured pink. The faintest traces of iodate are found by dissolving 5 g. in 100 c.c. of boiled water, adding a little nitric acid, a few drops of a solution of potassium iodide in boiled water, and a drop of starch solution. In the presence of as little as 0.01 mg. I in 1 g. of nitre, a blue colour will appear. A check test must, however, be made with the potassium iodide employed for this test, as this often contains some iodate.

7. *Potassium*.—Evaporate a special sample several times with strong hydrochloric acid until all the nitrate is decomposed, and estimate the K as in the analysis of potassium chloride, p. 203. Calculate it as KNO_3 , 100 parts of which is equivalent with 84.08 of NaNO_3 .

8. *Perchlorate* (Gilbert).—Treat 20 g. of the dried substance with 2 or 3 c.c. concentrated hydrochloric acid in a flat, platinum crucible; add about 1 g. manganese dioxide, free from chlorine, dry by heating over a small flame; bring to fusion, put on the lid and keep the crucible at a red heat during one-quarter hour. Dissolve the melt in hot water and dilute the solution to 250 c.c. Take out 50 c.c. (= 4 g. nitre), acidulate with nitric acid and add a 1 per cent. solution of KMnO_4 until the red colour persists for a full minute. Then add ferric potassium sulphate (iron-alum), and titrate the chloride by means of silver nitrate (Volhard's method). From the Cl thus found, deduct that which was originally present (No. 5), and calculate the remainder as perchlorate. 1 part NaCl corresponds to 2.094 NaClO_3 .

B.—Nitro-Oake.

1. *Free Acid* is titrated with standard alkali (p. 146). When considerable quantities of ferric oxide or alumina are present, no indicator is employed, but normal alkali is added till the first flakes of a precipitate indicate the end of the reaction.

2. *Nitric Acid* should be estimated in the gas-volumeter (p. 139), or in the nitrometer (p. 136); the method employed is exactly the same as described, viz., dissolving in the beaker in very little water, and decomposing with a large excess of sulphuric acid.

3. *Ferric Oxide and Alumina* (as pp. 142 and 147).

C.—Nitric Acid.

1. SPECIFIC GRAVITY OF NITRIC ACID AT 15° C., COMPARED WITH WATER OF 4° C. (IN VACUO).

(Lunge and Rey.)

Degrees Twad- dell.	Percentage by weight.		Grams per litre.	
	N ₂ O ₅ .	HNO ₃ .	N ₂ O ₅ .	HNO ₃ .
0	0·08	0·10	1	1
1	0·35	1·00	8	10
2	1·62	1·90	16	19
3	2·89	2·80	24	28
4	3·17	3·70	33	38
5	3·94	4·60	40	47
6	4·71	5·50	49	57
7	5·47	6·38	57	66
8	6·22	7·26	64	75
9	6·97	8·13	73	85
10	7·71	8·99	81	94
11	8·43	9·84	89	104
12	9·15	10·68	97	113
13	9·87	11·51	105	123
14	10·57	12·33	113	132
15	11·27	13·15	121	141
16	11·96	13·95	129	151
17	12·64	14·74	137	160
18	13·31	15·33	145	169
19	13·99	16·32	153	179
20	14·67	17·11	161	188
21	15·34	17·89	170	198
22	16·00	18·67	177	207
23	16·67	19·45	186	217
24	17·34	20·23	195	227
25	18·00	21·00	202	236
26	18·66	21·77	211	246
27	19·32	22·54	219	256
28	19·98	23·31	228	266
29	20·64	24·08	237	276
30	21·29	24·84	245	286
31	21·94	25·60	254	296
32	22·60	26·36	262	306
33	23·25	27·12	271	316
34	23·90	27·88	279	326

SPECIFIC GRAVITY OF NITRIC ACID AT 15° C., COMPARED WITH WATER OF 4° C. (IN VACUO)—Continued.

Degrees Twad. dell.	Percentage by weight.		Grams per litre.	
	N ₂ O ₅ .	HNO ₃ .	N ₂ O ₅ .	HNO ₃ .
35	24·54	28·68	288	386
36	25·18	29·88	297	347
37	25·83	30·13	306	357
38	26·47	30·88	315	367
39	27·10	31·62	324	378
40	27·74	32·36	333	388
41	28·36	33·09	342	399
42	28·99	33·82	351	409
43	29·61	34·55	360	420
44	30·24	35·28	369	430
45	30·88	36·03	378	441
46	31·53	36·78	387	452
47	32·17	37·53	397	463
48	32·82	38·29	407	475
49	33·47	39·05	417	486
50	34·13	39·82	427	498
51	34·78	40·58	437	509
52	35·44	41·34	447	521
53	36·09	42·10	457	533
54	36·75	42·87	467	544
55	37·41	43·64	477	556
56	38·07	44·41	487	568
57	38·73	45·18	498	581
58	39·39	45·95	508	593
59	40·05	46·72	519	605
60	40·71	47·49	529	617
61	41·37	48·26	540	630
62	42·06	49·07	551	643
63	42·76	49·89	562	656
64	43·47	50·71	573	669
65	44·17	51·53	585	683
66	44·89	52·37	597	697
67	45·62	53·22	609	710
68	46·35	54·07	621	725
69	47·08	54·93	633	739

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SPECIFIC GRAVITY OF NITRIC ACID AT 15° C., COMPARED WITH WATER OF 4° C. (IN VACUO)—*Continued.*

Degrees Twaddell.	Percentage by weight.		Grams per litre.	
	N ₂ O ₅ .	HNO ₃ .	N ₂ O ₅ .	HNO ₃ .
70	47·82	55·79	645	753
71	48·57	56·66	658	768
72	49·85	57·57	671	783
73	50·13	58·48	684	798
74	50·91	59·39	698	814
75	51·69	60·30	711	829
76	52·52	61·27	725	846
77	53·35	62·24	739	862
78	54·20	63·23	753	879
79	55·07	64·25	768	896
80	55·97	65·30	783	914
81	56·92	66·40	800	933
82	57·86	67·50	816	952
83	58·83	68·63	832	971
84	59·83	69·80	849	991
85	60·84	70·98	867	1011
86	61·86	72·17	885	1032
87	62·91	73·39	903	1053
88	64·01	74·68	921	1075
89	65·13	75·98	941	1098
90	66·24	77·28	961	1121
91	67·38	78·60	981	1144
92	68·56	79·98	1001	1168
93	69·79	81·42	1023	1193
94	71·06	82·90	1045	1219
95	72·39	84·45	1068	1246
96	73·76	86·05	1092	1274
97	75·18	87·70	1116	1302
98	76·80	89·60	1144	1335
99	78·52	91·60	1174	1369
100	80·65	94·09	1210	1411
101	82·63	96·39	1244	1451
102	84·09	98·10	1270	1481
103	84·92	99·07	1287	1501
104	85·44	99·67	1299	1515

2. INFLUENCE OF TEMPERATURE ON THE SPECIFIC GRAVITY OF NITRIC ACID.

0° C.	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°
1.424	1.414	1.407	1.400	1.392	1.385	1.378	1.371	1.368	1.356	1.349
1.418	1.404	1.397	1.390	1.382	1.375	1.367	1.361	1.354	1.347	1.340
1.402	1.394	1.387	1.380	1.372	1.365	1.357	1.351	1.344	1.339	1.332
1.391	1.383	1.377	1.370	1.363	1.356	1.349	1.342	1.335	1.330	1.323
1.380	1.373	1.367	1.360	1.353	1.346	1.340	1.333	1.326	1.320	1.314
1.369	1.362	1.356	1.350	1.343	1.337	1.330	1.323	1.317	1.312	1.305
1.359	1.352	1.346	1.340	1.333	1.327	1.320	1.314	1.306	1.303	1.297
1.348	1.342	1.336	1.330	1.324	1.318	1.311	1.305	1.299	1.294	1.288
1.338	1.332	1.326	1.320	1.314	1.308	1.302	1.296	1.290	1.285	1.280
1.327	1.321	1.316	1.310	1.304	1.299	1.293	1.287	1.281	1.276	1.271
1.317	1.311	1.306	1.300	1.294	1.289	1.283	1.278	1.273	1.268	1.263
1.307	1.301	1.296	1.290	1.284	1.279	1.273	1.268	1.263	1.258	1.253
1.297	1.291	1.286	1.280	1.274	1.269	1.263	1.258	1.253	1.248	1.243
1.287	1.281	1.276	1.270	1.265	1.259	1.254	1.248	1.243	1.238	1.234
1.277	1.271	1.266	1.260	1.255	1.249	1.244	1.238	1.233	1.228	1.224
1.266	1.260	1.255	1.250	1.245	1.240	1.235	1.229	1.224	1.219	1.215
1.256	1.250	1.245	1.240	1.235	1.230	1.225	1.220	1.215	1.210	1.205
1.245	1.240	1.235	1.230	1.225	1.220	1.215	1.210	1.206	1.201	1.196
1.235	1.230	1.225	1.220	1.215	1.210	1.205	1.200	1.196	1.191	1.186
1.224	1.219	1.214	1.210	1.205	1.200	1.196	1.191	1.187	1.182	1.177
1.213	1.208	1.204	1.200	1.195	1.190	1.186	1.181	1.177	1.172	1.167
1.202	1.198	1.194	1.190	1.185	1.181	1.177	1.172	1.168	1.163	1.158
1.192	1.188	1.184	1.180	1.177	1.171	1.167	1.163	1.158	1.154	1.150
1.182	1.178	1.174	1.170	1.166	1.162	1.158	1.154	1.149	1.145	1.141
1.172	1.168	1.164	1.160	1.156	1.152	1.148	1.144	1.140	1.136	1.132
1.161	1.158	1.154	1.150	1.146	1.142	1.139	1.135	1.130	1.127	1.123
1.151	1.147	1.144	1.140	1.136	1.132	1.129	1.125	1.121	1.118	1.114
1.139	1.136	1.133	1.130	1.126	1.123	1.119	1.116	1.112	1.109	1.105
1.129	1.126	1.123	1.120	1.116	1.113	1.110	1.106	1.103	1.100	1.096
1.118	1.115	1.112	1.110	1.107	1.104	1.101	1.097	1.094	1.091	1.087
1.108	1.100	1.102	1.100	1.097	1.094	1.091	1.088	1.085	1.082	1.079
1.098	1.095	1.092	1.090	1.087	1.084	1.081	1.078	1.075	1.073	1.070
1.088	1.085	1.082	1.080	1.077	1.074	1.071	1.068	1.065	1.063	1.060
1.077	1.075	1.072	1.070	1.067	1.064	1.061	1.058	1.056	1.054	1.051
1.067	1.064	1.062	1.060	1.057	1.055	1.052	1.050	1.048	1.045	1.043
1.057	1.054	1.052	1.050	1.047	1.045	1.043	1.040	1.038	1.035	1.033
1.047	1.044	1.042	1.040	1.037	1.035	1.033	1.030	1.028	1.025	1.023
1.037	1.034	1.032	1.030	1.027	1.025	1.023	1.020	1.018	1.015	1.013
1.027	1.024	1.022	1.020	1.017	1.015	1.013	1.010	1.008	1.005	1.003
1.017	1.014	1.012	1.010	1.007	1.005	1.003	1.000	0.998	0.995	0.993

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INFLUENCE OF TEMPERATURE ON THE SPECIFIC GRAVITY OF NITRIC ACID—*Continued.*

55°	60°	65°	70°	75°	80°	85°	90°	95°	100°
1·842	1·835	1·829	1·823	1·816	1·810	1·808	1·296	1·290	1·283
1·833	1·827	1·820	1·814	1·808	1·802	1·294	1·288	1·282	1·276
1·825	1·819	1·812	1·806	1·800	1·292	1·286	1·280	1·274	1·267
1·816	1·810	1·804	1·298	1·292	1·286	1·279	1·274	1·267	1·260
1·808	1·802	1·296	1·290	1·284	1·278	1·272	1·266	1·260	1·254
1·800	1·294	1·288	1·282	1·276	1·270	1·265	1·259	1·253	1·247
1·291	1·286	1·280	1·274	1·268	1·263	1·257	1·252	1·246	1·240
1·282	1·278	1·272	1·266	1·261	1·255	1·250	1·245	1·240	1·234
1·274	1·269	1·264	1·258	1·253	1·248	1·243	1·238	1·233	1·228
1·266	1·261	1·256	1·251	1·246	1·240	1·235	1·230	1·225	1·220
1·258	1·253	1·248	1·243	1·238	1·232	1·227	1·222	1·217	1·212
1·248	1·244	1·239	1·234	1·229	1·223	1·218	1·213	1·208	1·203
1·238	1·234	1·229	1·224	1·219	1·214	1·209	1·204	1·199	1·194
1·229	1·225	1·220	1·215	1·210	1·205	1·199	1·195	1·190	1·185
1·219	1·215	1·210	1·206	1·200	1·195	1·190	1·185	1·180	1·175
1·210	1·206	1·201	1·196	1·191	1·186	1·181	1·176	1·171	1·167
1·200	1·196	1·191	1·186	1·181	1·177	1·172	1·167	1·162	1·158
1·191	1·187	1·182	1·177	1·172	1·168	1·163	1·158	1·153	1·149
1·182	1·177	1·172	1·167	1·163	1·158	1·153	1·148	1·144	1·139
1·173	1·168	1·163	1·160	1·154	1·149	1·144	1·140	1·135	1·130
1·163	1·158	1·154	1·150	1·145	1·140	1·136	1·131	1·126	1·122
1·154	1·150	1·146	1·141	1·136	1·132	1·128	1·123	1·119	1·115
1·145	1·141	1·137	1·133	1·128	1·124	1·120	1·116	1·112	1·107
1·137	1·132	1·128	1·124	1·120	1·116	1·112	1·108	1·105	1·100
1·128	1·124	1·120	1·116	1·112	1·108	1·105	1·101	1·097	1·094
1·119	1·115	1·112	1·108	1·104	1·100	1·097	1·093	1·090	1·086
1·110	1·107	1·103	1·100	1·096	1·093	1·090	1·086	1·082	1·079
1·102	1·099	1·094	1·091	1·088	1·084	1·081	1·078	1·075	1·071
1·093	1·090	1·086	1·083	1·080	1·076	1·073	1·070	1·067	1·064
1·084	1·081	1·078	1·075	1·072	1·068	1·065	1·063	1·060	1·056
1·076	1·073	1·070	1·067	1·064	1·061	1·058	1·055	1·052	1·049
1·067	1·064	1·061	1·058	1·055	1·052	1·050	1·048	1·045	1·042
1·058	1·055	1·052	1·050	1·047	1·044	1·042	1·040	1·038	1·036
1·049	1·046	1·044	1·042	1·039	1·037	1·034	1·031	1·029	1·027
1·040	1·038	1·036	1·034	1·031	1·029	1·026	1·023	1·021	1·018
1·030	1·028	1·026	1·024	1·021	1·019	1·015	1·014	1·012	1·009
1·020	1·018	1·016	1·014	1·011	1·009	1·007	1·004	1·002	1·000
1·010	1·008	1·006	1·004	1·001	0·999	0·997	0·994	0·993	0·990
1·001	0·999	0·997	0·995	0·992	0·990	0·988	0·985	0·983	0·981
0·991	0·989	0·987	0·985	0·982	0·980	0·978	0·975	0·973	0·971

3. *Total Acidity*.—Titrate a diluted sample with standard caustic soda solution. Methyl orange can be quite well used as indicator, if the titration is performed as described, p. 135, although it would be destroyed by prolonged contact with nitrous acid. Strong fuming acid is weighed in a bulb-tap pipette, Fig. 11, p. 144; from this the acid is slowly run to the bottom of a flask, containing ice-cold water, and the titration is performed quickly, to prevent a decomposition of the nitrous acid. Less concentrated nitric acids may be measured by pipettes or burettes, in lieu of weighing.

4. *Chlorine*.—Saturate with sodium carbonate, free from chloride, till the reaction is neutral or faintly alkaline, and titrate with silver nitrate according to p. 145.

5. *Sulphuric Acid*.—Saturate almost completely with sodium carbonate and precipitate with barium chloride as on p. 110. If the acid on evaporating leaves any appreciable fixed residue, this usually consists of sodium sulphate.

6. *Nitrous Acid* or *Nitrogen Tetroxide* are estimated by running the acid from a burette into a measured volume of warm, dilute potassium permanganate (*cf.* p. 135). The result is usually expressed in terms of nitrogen peroxide, N_2O_4 . Each c.c. $\frac{1}{2}$ normal permanganate = 0.023005 g. N_2O_4 . Hence, if m c.c. acid have been used and n c.c. permanganate required, the amount of N_2O_4 is:—

$$\frac{0.023005 n}{m} \text{ g.}$$

The quantity of N_2O_4 is often so considerable that the specific gravity tables give a very deceptive result as to the real percentage of HNO_3 , and an actual determination should be made.

7. *Fixed Residue*, consisting chiefly of sodium sulphate, with a little ferric oxide, etc., is estimated by evaporating to dryness in a place protected from dust, igniting, and weighing.

8. *Iron*.—Precipitate with excess of ammonia, filter, weigh, and ignite the Fe_2O_3 .

9. *Iodine* is detected by digesting for a short time with pure zinc, which reduces iodic acid and generates some nitrous acid; the latter sets the iodine of the HI free, and this can then be recognised by shaking up with carbon disulphide, which thereby assumes a pink colour.

N.B.—Tests Nos. 8 and 9 are only made with nitric acid sold as chemically pure.

D.—Mixtures of Sulphuric Acid and Nitric Acid.

Such mixtures are sold for the manufacture of explosives and other nitrating purposes. They are analysed by the methods described by Lunge and Berl, *Z. angew. Chem.*, 1905, p. 1681; *Chem. Zeit.*, 1907, p. 485.

1. *Total Acidity*.—Weigh about 1 g. in a bulb-tap pipette, Fig. 11, p. 144, and titrate with normal caustic soda solution. When employing methyl orange as indicator, either add it only towards the end of the titration (or else renew it as destroyed), or else add an excess of soda, then the indicator, and titrate back with normal hydrochloric acid (compare p. 135).

2. *Nitrous Acid* is estimated as on p. 135, by running the mixed acid into a measured quantity of $\frac{1}{2}$ normal permanganate. It may be calculated as HNO_2 , or N_2O_3 , or even as N_2O_4 . In the latter case each c.c. of the $\frac{1}{2}$ normal permanganate indicates 0.023005 g. N_2O_4 . If we call the c.c. of permanganate used x , the c.c. of mixed acid required for decolorising it y , and s the specific gravity of the latter, the N_2O_4 is $= \frac{23x}{y}$ g. per litre, or $\frac{2.3x}{ys}$ per cent. by weight of N_2O_4 in the mixed acid.

3. *Total Nitrogen Acids* are estimated by the nitrometer, p. 136. From the NO given off deduct that corresponding to the nitrous acid found in No. 2, and calculate the remainder as HNO_3 .

4. *Sulphuric Acid* is found by deducting the nitrogen acids, found in No. 3, from the total acidity found in No. 1.

If for 1 g. mixed acid we have used a c.c. $\frac{1}{2}$ normal soda solution and found b c.c. NO (reduced to 0° and 760 mm.), and c , c.c. of $\frac{1}{2}$ normal permanganate to be required, the percentage of the individual components is found by one of the following formulæ, according as to whether we assume N_2O_4 or N_2O_3 to be present:—

$$\begin{aligned} \text{H}_2\text{SO}_4 &= 0.9808 a - 0.219 b \\ \text{HNO}_3 &= 0.28144 b - 3.149 c \\ \text{N}_2\text{O}_4 &= 2.30 c \\ \text{H}_2\text{O} &= 100 - (\text{H}_2\text{SO}_4 + \text{HNO}_3 \\ &\quad + \text{N}_2\text{O}_4) \end{aligned}$$

$$\begin{aligned} \text{H}_2\text{SO}_4 &= 0.9808 a - 0.219 b \\ \text{HNO}_3 &= 0.28144 b - 1.5745 c \\ \text{N}_2\text{O}_3 &= 0.9508 c \\ \text{H}_2\text{O} &= 100 - (\text{H}_2\text{SO}_4 + \text{HNO}_3 \\ &\quad + \text{N}_2\text{O}_3). \end{aligned}$$

X. POTASSIUM SALTS.

A.—Crude Salts (Carnallite, Kainite, etc.).

1. *Moisture*.—Heat 10 g. to 150° for some time, and allow to cool in a desiccator.

2. *Percentage of Potassium* : *—

(a) *In the Absence of more than 0.5 per cent. Potassium Sulphate*.—Obtain a well-mixed sample; dissolve 7.640 g. in a half-litre flask, fill up to the mark, and filter. Place 20 c.c. of the filtrate (=0.3056 of the crude salt) in a porcelain dish; add 5 c.c. of a solution of platinum chloride containing 10 g. Pt in 100 c.c. Evaporate on the water-bath to a syrupy condition, with frequent agitation, so that most of the HCl is driven off and the mass appears dry after cooling. When cool, crush it with a flattened glass rod, add 20 c.c. strong alcohol (at least 94 per cent.), mix well through and pour the liquid portion through a filter which has been previously dried at 120° to 130° till the weight is constant, then weighed and moistened with alcohol. The filter should not be filled up to the top. Pour fresh alcohol on the residue, and heat it on the water-bath nearly to boiling. Wash the solid portion on to the filter, remove most of the liquid by suction, press it between layers of filter paper and dry it till the weight is constant at 120° to 130° (this will usually require only twenty minutes). Each milligram of the potassium-platinum chloride corresponds to 0.1 per cent. KCl in the quantity of substance employed.

(b) *In the Presence of more than 0.5 per cent. Potassium Sulphate*.—Dissolve 30.56 g. of the crude salt in a $\frac{1}{2}$ -litre flask in 300 c.c. water + 13 c.c. strong hydrochloric acid by boiling, allow to cool, and fill the flask up to the mark. Put 50 c.c. of the clear solution into a 200 c.c. flask, heat to boiling, and precipitate the sulphate with the exactly necessary quantity of barium chloride, by adding the principal portion of the reagent quickly, the remainder in single drops, always waiting till the liquid shows a clear layer and throwing into this a minute crystal of barium chloride, until this ceases to produce a cloud. If too

* These are the methods given by Tietjens in *Tech. Meth.*, vol. i., p. 520, as worked out and practised at all the Stassfurt works. This applies also to the figures employed for the calculation of the results which are not based on the real atomic weight of platinum (=194.80) and on the formula K_2PtCl_6 , but are empirical data, based on many years' experience. The difference is mainly caused by the fact that the precipitate is not pure K_2PtCl_6 , but contains some chemically combined water which is not given up even after prolonged drying.

much BaCl_2 should have been accidentally added, it must be removed by a drop or two of dilute sulphuric acid. After cooling, fill up to the mark and take 20 c.c. of the clear solution = 0.3056 g. salt, which is then treated with platinum chloride as described in No. 1. One mg. of the precipitate corresponds to 0.1 per cent. KCl, if the K is to be calculated as such.

For the analysis of salts consisting essentially of K_2SO_4 , like kainite, dissolve 35.71 g., in which case each mg. of the platinum precipitate indicates 0.1 per cent. K_2SO_4 . When testing rich sulphate (90 to 97 per cent. K_2SO_4) it is necessary to add to the percentage thus found a correction of +0.3 per cent., but this should not be made in the case of potasso-magnesium sulphates.

3. Percentage of Sodium Chloride :—

(a) *In High-Grade Salts.*—If there is little or no sulphate present, the NaCl is calculated from the difference between the KCl found directly by gravimetric analysis and the total chlorides as found by titration with silver solution, p. 145. Where there is an appreciable proportion of sulphate present, the percentage of (combined) SO_3 must be estimated, as well as that of potassium and chlorine. The barium sulphate obtained is calculated to KCl (1 part $\text{BaSO}_4 = 0.7469 \text{K}_2\text{SO}_4 = 0.6391 \text{KCl}$); this amount is deducted from the total quantity of K, calculated as KCl; the remaining KCl, which was present as such and must be quoted as such in the analysis, is deducted from that which is found when calculating all the Cl as KCl. The now remaining nominal amount of KCl is calculated as NaCl, 100 parts KCl being equivalent to 78.52 NaCl. The SO_3 found is calculated as K_2SO_4 .

(b) *In Low-Grade Salts* it is not usual to estimate the NaCl. If it is to be done, a complete analysis is required. KCl is estimated as above, in addition: Ca (p. 146), Mg (pp. 147 and 205), SO_3 (p. 110), insoluble matter, and moisture. SO_3 is calculated as CaSO_4 ; if there is not enough Ca present for all the SO_3 , the remainder is calculated as MgSO_4 , and after that as K_2SO_4 . If more Mg is present than is required to saturate the SO_3 at disposal, the remaining Mg is calculated as MgCl_2 . Any excess of Cl over that required to form KCl and MgCl_2 is calculated as NaCl.

4. *Magnesium Chloride.*—In order to distinguish the carnallite salts (which gave up the MgCl_2 to alcohol) from the non-carnallitic salts (which do not do this), shake 10 g. of the crude salt for ten minutes in a $\frac{1}{2}$ -litre flask with 100 c.c. 96 per cent. alcohol and titrate 10 c.c. of the filtrate with $\frac{1}{10}$ normal silver solution. Such salts as contain upwards of 6 per cent. Cl soluble in alcohol are regarded as belonging to the carnallite group.

5. *Total Magnesium*.—Boil 10 g. of finely ground, crude salt with 300 c.c. of water in a $\frac{1}{2}$ -litre flask for an hour; after cooling add 50 c.c. twice-normal sodium hydroxide solution, in the case of much lime being present also 20 c.c. of a 10 per cent. solution of neutral potassium oxalate, fill the flask up to the mark, filter after a quarter of an hour, and titrate 50 c.c. of the filtrate with normal hydrochloric acid. Each c.c. of the twice-normal alkali used up is = 0.04036 g. $MgCl_2$. To the percentage of MgO 0.2 per cent. should be added (*Precht. Z. anal. Chem.*, 1879, p. 438).

B.—Commercial Potassium Chloride.

Weigh out 7.640 g. and proceed exactly as described under A, 2 (a), p. 203. The calculation is also made in the same manner.

Potassium chloride made from vinasses contains much sulphate and a little carbonate which is estimated alkalimetrically.

C.—Potassium Sulphate.

Proceed just as in the case of sodium sulphate, p. 146. The potassium must sometimes be estimated, which is done as on p. 203 for A, 2 (b).

D.—Leblanc Process for the Manufacture of Potassium Carbonate.

Both the raw materials and the intermediate products are tested like those for the soda process, p. 164 *et seq.*

E.—Beet Ashes.

For this material, which seldom occurs in the English trade, special methods have been worked out by Heyer (*Chemiker-Zeitung*, 1891, p. 1489 *et seq.*), and by Alberti and Hempel (*ibid.*, p. 1623).

F.—Commercial Carbonate of Potash.

1. *Available Alkali* is titrated with normal hydrochloric acid, as on p. 176.

2. *Total Potassium* is estimated according to p. 203, A (b), so that all sulphate is converted into chloride. Of course, initially,

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more hydrochloric must be employed in order to decompose the carbonate.

3. *Chloride* is estimated by decinormal silver solution, p. 145. 1 c.c. of this = 0.00746 g. KCl.

4. *Sulphate* is estimated as BaSO_4 , p. 110. 1 g. BaSO_4 = 0.7469 K_2SO_4 .

5. *Insoluble matter*, as on p. 176.

6. *Silicate*.—Saturate the salt with hydrochloric acid, evaporate to dryness, moisten with HCl, evaporate again, dissolve in dilute HCl, filter, wash, and strongly ignite the SiO_2 . This test is only made exceptionally, and the potassium silicate is calculated together with the carbonate.

7. *Phosphate* is estimated by the magnesia method, and is treated like the silicate.

8. *Calculation of the Analyses*.—Calculate :—

(a) K_2CO_3 from the difference between the total potassium and that corresponding to the Cl and SO_3 found.

(b) Na_2CO_3 from the difference between the total available alkali and the K_2CO_3 as calculated in (a).

(c) KCl and

(d) K_2SO_4 as above.

(e) Water and

(f) Insoluble matter, if necessary also iron, by a special test.

1. SPECIFIC GRAVITIES OF SOLUTIONS OF POTASSIUM CARBONATE AT 15°.

Specific Gravity.	Degrees Twaddell.	Degrees Baumé.	Per cent. K_2CO_3 .	1 cb.m. contains kg. K_2CO_3 .
1·000	0	0	0	0
1·005	1	0·7	0·50	5·0
1·010	2	1·4	1·04	10·50
1·015	3	2·1	1·60	16·24
1·020	4	2·7	2·10	21·42
1·025	5	3·4	2·64	27·06
1·030	6	4·1	3·21	33·06
1·035	7	4·7	3·77	39·02
1·040	8	5·4	4·34	45·14
1·045	9	6·0	4·90	51·21
1·050	10	6·7	5·47	57·44
1·055	11	7·4	6·00	63·30
1·060	12	8·0	6·50	68·90
1·065	13	8·7	7·07	75·30
1·070	14	9·4	7·60	81·32
1·075	15	10·0	8·10	87·08
1·080	16	10·6	8·67	93·64
1·085	17	11·2	9·20	99·82
1·090	18	11·9	9·70	105·73
1·095	19	12·4	10·20	111·69
1·100	20	13·0	10·70	117·70
1·105	21	13·6	11·26	124·42
1·110	22	14·2	11·80	130·98
1·115	23	14·9	12·30	137·15
1·120	24	15·4	12·80	143·36
1·125	25	16·0	13·30	149·63
1·130	26	16·5	13·80	155·94
1·135	27	17·0	14·30	162·31
1·140	28	17·7	14·80	168·72
1·145	29	18·3	15·30	175·19
1·150	30	18·8	15·80	181·70
1·155	31	19·3	16·30	188·27
1·160	32	19·8	16·80	194·88
1·165	33	20·3	17·30	201·55
1·170	34	20·9	17·80	208·26
1·175	35	21·4	18·30	215·03
1·180	36	22·0	18·80	221·84
1·185	37	22·5	19·26	228·23

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SPECIFIC GRAVITIES OF SOLUTIONS OF POTASSIUM
CARBONATE AT 15°—*Continued.*

Specific Gravity.	Degrees Twaddell.	Degrees Baumé.	Per cent. K_2CO_3 .	l. cu. m. contains kg. K_2CO_3 .
1.190	38	23.0	19.70	234.43
1.195	39	23.5	20.20	241.89
1.200	40	24.0	20.70	248.40
1.205	41	24.5	21.15	254.86
1.210	42	25.0	21.60	261.36
1.215	43	25.5	22.05	267.91
1.220	44	26.0	22.50	274.50
1.225	45	26.4	22.96	281.26
1.230	46	26.9	23.41	287.94
1.235	47	27.4	23.90	295.17
1.240	48	27.9	24.40	302.56
1.245	49	28.4	24.86	309.51
1.250	50	28.8	25.32	316.50
1.255	51	29.3	25.80	323.79
1.260	52	29.7	26.30	331.38
1.265	53	30.2	26.77	338.64
1.270	54	30.6	27.17	345.06
1.275	55	31.1	27.60	351.90
1.280	56	31.5	28.05	359.04
1.285	57	32.0	28.50	366.23
1.290	58	32.4	28.96	373.58
1.295	59	32.8	29.42	380.99
1.300	60	33.3	29.97	389.61
1.305	61	33.7	30.43	397.11
1.310	62	34.2	30.86	404.27
1.315	63	34.6	31.24	410.81
1.320	64	35.0	31.60	417.12
1.325	65	35.4	32.06	424.80
1.330	66	35.8	32.52	432.52
1.335	67	36.2	32.96	440.02
1.340	68	36.6	33.38	447.29
1.345	69	37.0	33.80	454.61
1.350	70	37.4	34.22	461.97
1.355	71	37.8	34.64	469.37
1.360	72	38.2	35.06	476.82
1.365	73	38.6	35.48	484.30
1.370	74	39.0	35.90	491.83

SPECIFIC GRAVITIES OF SOLUTIONS OF POTASSIUM CARBONATE AT 15°—Continued.

Specific Gravity.	Degrees Twaddell.	Degrees Baumé.	Per cent. K_2CO_3 .	1 cb.m. contains kg. K_2CO_3 .
1.375	75	39.4	36.32	499.40
1.380	76	39.8	36.74	507.01
1.385	77	40.1	37.17	514.80
1.390	78	40.5	37.60	522.64
1.395	79	40.8	38.02	530.38
1.400	80	41.2	38.45	538.30
1.405	81	41.6	38.88	546.26
1.410	82	42.0	39.30	554.13
1.415	83	42.3	39.73	562.19
1.420	84	42.7	40.16	570.27
1.425	85	43.1	40.59	578.41
1.430	86	43.4	41.02	586.59
1.435	87	43.8	41.45	594.81
1.440	88	44.1	41.88	602.64
1.445	89	44.4	42.22	610.08
1.450	90	44.8	42.58	617.41
1.455	91	45.1	42.97	625.21
1.460	92	45.4	43.37	633.20
1.465	93	45.8	43.77	641.23
1.470	94	46.1	44.17	649.30
1.475	95	46.4	44.57	657.41
1.480	96	46.8	44.96	665.41
1.485	97	47.1	45.38	673.89
1.490	98	47.4	45.81	682.57
1.495	99	47.8	46.24	691.29
1.500	100	48.1	46.66	699.90
1.505	101	48.4	47.03	707.80
1.510	102	48.7	47.40	715.74
1.515	103	49.0	47.78	723.87
1.520	104	49.4	48.15	731.88
1.525	105	49.7	48.53	740.08
1.530	106	50.0	48.90	748.17
1.535	107	50.3	49.26	756.14
1.540	108	50.6	49.61	763.99
1.545	109	50.9	49.96	771.88
1.550	110	51.2	50.33	780.12
1.555	111	51.5	50.70	788.39
1.560	112	51.8	51.07	796.69
1.565	113	52.1	51.45	805.19

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2. INFLUENCE OF TEMPERATURE ON THE SPECIFIC

0° C.	5°.	10°.	15°.	20°.	25°.	30°.	35°.	40°.	45°.	50°.
1.588	1.586	1.583	1.580	1.577	1.574	1.571	1.568	1.566	1.563	1.559
1.577	1.575	1.573	1.570	1.568	1.565	1.563	1.560	1.557	1.554	1.551
1.567	1.565	1.563	1.560	1.558	1.555	1.553	1.550	1.548	1.545	1.543
1.557	1.554	1.552	1.550	1.548	1.546	1.544	1.541	1.538	1.536	1.533
1.547	1.544	1.542	1.540	1.538	1.536	1.534	1.531	1.528	1.526	1.523
1.536	1.534	1.532	1.530	1.528	1.526	1.524	1.521	1.518	1.515	1.512
1.526	1.524	1.522	1.520	1.518	1.516	1.514	1.511	1.508	1.506	1.502
1.516	1.514	1.512	1.510	1.508	1.506	1.503	1.500	1.498	1.496	1.492
1.506	1.504	1.502	1.500	1.498	1.496	1.493	1.490	1.488	1.486	1.482
1.496	1.494	1.492	1.490	1.488	1.486	1.484	1.481	1.478	1.475	1.472
1.486	1.484	1.482	1.480	1.478	1.476	1.474	1.471	1.468	1.465	1.462
1.476	1.474	1.472	1.470	1.468	1.466	1.464	1.461	1.458	1.455	1.452
1.466	1.464	1.462	1.460	1.458	1.456	1.454	1.451	1.448	1.445	1.442
1.456	1.454	1.452	1.450	1.448	1.446	1.444	1.441	1.438	1.435	1.432
1.446	1.444	1.442	1.440	1.438	1.436	1.434	1.431	1.428	1.425	1.422
1.436	1.434	1.432	1.430	1.428	1.426	1.423	1.420	1.418	1.414	1.411
1.426	1.424	1.422	1.420	1.418	1.416	1.413	1.410	1.408	1.404	1.401
1.416	1.414	1.412	1.410	1.408	1.406	1.404	1.401	1.398	1.395	1.392
1.406	1.404	1.402	1.400	1.398	1.396	1.394	1.391	1.388	1.385	1.382
1.396	1.394	1.392	1.390	1.388	1.386	1.384	1.381	1.378	1.375	1.373
1.386	1.384	1.382	1.380	1.378	1.376	1.374	1.371	1.368	1.366	1.363
1.376	1.374	1.372	1.370	1.368	1.366	1.364	1.361	1.358	1.355	1.353
1.366	1.364	1.362	1.360	1.358	1.356	1.354	1.351	1.348	1.346	1.343
1.356	1.354	1.352	1.350	1.348	1.346	1.344	1.341	1.338	1.336	1.333
1.346	1.344	1.342	1.340	1.338	1.336	1.334	1.331	1.328	1.326	1.323
1.336	1.334	1.332	1.330	1.328	1.326	1.324	1.321	1.318	1.316	1.313
1.326	1.324	1.322	1.320	1.318	1.316	1.314	1.311	1.308	1.306	1.303
1.316	1.314	1.312	1.310	1.308	1.306	1.303	1.300	1.298	1.296	1.292
1.306	1.304	1.302	1.300	1.298	1.296	1.293	1.290	1.288	1.285	1.282
1.296	1.294	1.292	1.290	1.288	1.286	1.283	1.280	1.278	1.275	1.273
1.286	1.284	1.282	1.280	1.278	1.276	1.273	1.270	1.268	1.265	1.263
1.276	1.274	1.272	1.270	1.268	1.265	1.263	1.260	1.257	1.255	1.252
1.266	1.264	1.262	1.260	1.258	1.255	1.253	1.250	1.247	1.245	1.242
1.256	1.254	1.252	1.250	1.248	1.246	1.243	1.240	1.238	1.235	1.232
1.246	1.244	1.242	1.240	1.238	1.236	1.233	1.230	1.228	1.225	1.222
1.236	1.234	1.232	1.230	1.228	1.226	1.224	1.221	1.219	1.217	1.214
1.226	1.224	1.222	1.220	1.218	1.216	1.214	1.211	1.209	1.207	1.204
1.216	1.214	1.212	1.210	1.208	1.206	1.204	1.202	1.199	1.197	1.194
1.206	1.204	1.202	1.200	1.198	1.196	1.194	1.192	1.189	1.187	1.184
1.196	1.194	1.192	1.190	1.188	1.186	1.184	1.182	1.179	1.177	1.174
1.186	1.184	1.182	1.180	1.178	1.176	1.174	1.172	1.170	1.167	1.164
1.176	1.174	1.172	1.170	1.168	1.166	1.164	1.162	1.160	1.157	1.155
1.166	1.163	1.161	1.160	1.158	1.156	1.154	1.152	1.150	1.147	1.145
1.156	1.153	1.151	1.150	1.148	1.146	1.144	1.142	1.140	1.137	1.135
1.144	1.143	1.141	1.140	1.138	1.136	1.134	1.132	1.130	1.127	1.125
1.133	1.132	1.131	1.130	1.128	1.126	1.124	1.122	1.120	1.117	1.114
1.123	1.122	1.121	1.120	1.118	1.116	1.114	1.112	1.110	1.107	1.104
1.113	1.112	1.111	1.110	1.108	1.106	1.104	1.102	1.100	1.097	1.094
1.103	1.102	1.101	1.100	1.098	1.096	1.094	1.092	1.090	1.087	1.084
1.093	1.092	1.091	1.090	1.089	1.087	1.086	1.083	1.081	1.079	1.077
1.083	1.082	1.081	1.080	1.079	1.077	1.076	1.073	1.071	1.069	1.067
1.073	1.072	1.071	1.070	1.069	1.067	1.066	1.064	1.062	1.060	1.058
1.063	1.062	1.061	1.060	1.059	1.057	1.056	1.054	1.052	1.050	1.048
1.053	1.052	1.051	1.050	1.049	1.047	1.046	1.044	1.042	1.040	1.038
1.043	1.042	1.041	1.040	1.039	1.037	1.036	1.034	1.032	1.030	1.028
1.033	1.032	1.031	1.030	1.028	1.027	1.025	1.024	1.022	1.020	1.018
1.023	1.022	1.021	1.020	1.018	1.017	1.015	1.014	1.012	1.010	1.008
1.013	1.012	1.011	1.010	1.008	1.007	1.006	1.004	1.002	1.000	0.998

POTASSIUM SALTS

GRAVITIES OF SOLUTIONS OF POTASSIUM CARBONATE.

55°.	60°.	65°.	70°.	75°.	80°.	85°.	90°.	95°.	100°.
1.556	1.558	1.550	1.546	1.542	1.538	1.534	1.530	1.526	1.521
1.548	1.545	1.541	1.537	1.533	1.530	1.526	1.522	1.518	1.513
1.539	1.536	1.532	1.528	1.525	1.522	1.517	1.513	1.509	1.505
1.530	1.527	1.524	1.521	1.518	1.513	1.509	1.504	1.501	1.498
1.520	1.517	1.514	1.511	1.508	1.504	1.500	1.497	1.494	1.490
1.509	1.507	1.504	1.500	1.497	1.494	1.491	1.488	1.485	1.481
1.499	1.497	1.494	1.490	1.487	1.484	1.481	1.478	1.475	1.471
1.489	1.487	1.484	1.480	1.477	1.474	1.471	1.468	1.465	1.461
1.479	1.476	1.474	1.470	1.467	1.464	1.461	1.458	1.455	1.451
1.469	1.466	1.464	1.460	1.457	1.454	1.450	1.447	1.444	1.441
1.459	1.456	1.454	1.450	1.447	1.444	1.440	1.437	1.434	1.431
1.449	1.446	1.444	1.440	1.437	1.434	1.431	1.428	1.424	1.421
1.439	1.436	1.434	1.430	1.427	1.424	1.421	1.418	1.414	1.411
1.429	1.426	1.423	1.420	1.417	1.414	1.410	1.408	1.405	1.402
1.419	1.416	1.413	1.410	1.407	1.404	1.400	1.396	1.396	1.392
1.409	1.406	1.404	1.401	1.398	1.395	1.391	1.388	1.385	1.382
1.399	1.396	1.394	1.391	1.388	1.385	1.381	1.378	1.375	1.372
1.390	1.387	1.384	1.380	1.377	1.374	1.371	1.368	1.365	1.362
1.380	1.377	1.374	1.370	1.367	1.364	1.361	1.358	1.355	1.352
1.370	1.367	1.364	1.361	1.358	1.355	1.351	1.348	1.345	1.342
1.360	1.357	1.354	1.351	1.348	1.345	1.341	1.338	1.335	1.332
1.350	1.347	1.344	1.341	1.338	1.335	1.332	1.329	1.326	1.323
1.340	1.337	1.334	1.331	1.328	1.325	1.322	1.319	1.316	1.313
1.330	1.327	1.324	1.321	1.318	1.315	1.312	1.309	1.306	1.303
1.320	1.317	1.314	1.311	1.308	1.305	1.302	1.299	1.296	1.293
1.310	1.307	1.304	1.301	1.298	1.295	1.292	1.289	1.286	1.284
1.300	1.297	1.294	1.291	1.288	1.285	1.282	1.279	1.276	1.274
1.290	1.287	1.284	1.281	1.278	1.276	1.273	1.270	1.267	1.264
1.280	1.277	1.274	1.271	1.268	1.266	1.263	1.260	1.257	1.254
1.270	1.267	1.264	1.261	1.258	1.256	1.253	1.250	1.247	1.244
1.260	1.257	1.254	1.251	1.248	1.246	1.243	1.240	1.237	1.234
1.250	1.247	1.244	1.242	1.239	1.236	1.234	1.231	1.228	1.225
1.240	1.237	1.234	1.232	1.229	1.226	1.224	1.221	1.218	1.215
1.230	1.227	1.224	1.221	1.218	1.216	1.213	1.210	1.208	1.205
1.220	1.217	1.214	1.211	1.208	1.206	1.203	1.200	1.198	1.195
1.212	1.209	1.206	1.203	1.198	1.196	1.194	1.192	1.188	1.186
1.202	1.199	1.196	1.193	1.190	1.187	1.184	1.182	1.178	1.176
1.192	1.189	1.186	1.183	1.180	1.178	1.175	1.172	1.169	1.167
1.182	1.179	1.176	1.173	1.171	1.168	1.165	1.162	1.159	1.157
1.172	1.169	1.166	1.164	1.161	1.158	1.155	1.152	1.149	1.146
1.162	1.159	1.156	1.154	1.151	1.148	1.145	1.142	1.139	1.136
1.152	1.150	1.147	1.144	1.141	1.138	1.135	1.132	1.129	1.126
1.142	1.140	1.137	1.134	1.131	1.128	1.125	1.122	1.119	1.116
1.132	1.130	1.128	1.125	1.122	1.118	1.115	1.112	1.109	1.106
1.122	1.120	1.118	1.115	1.112	1.108	1.105	1.102	1.099	1.096
1.112	1.110	1.108	1.105	1.102	1.098	1.095	1.092	1.089	1.086
1.102	1.100	1.098	1.095	1.092	1.088	1.085	1.082	1.078	1.076
1.092	1.090	1.087	1.084	1.082	1.079	1.075	1.072	1.069	1.067
1.082	1.080	1.077	1.074	1.072	1.069	1.065	1.062	1.059	1.057
1.074	1.071	1.068	1.065	1.063	1.060	1.057	1.054	1.050	1.048
1.066	1.062	1.059	1.056	1.054	1.051	1.048	1.045	1.041	1.038
1.056	1.053	1.050	1.047	1.045	1.042	1.039	1.036	1.032	1.029
1.046	1.044	1.041	1.038	1.036	1.033	1.030	1.026	1.023	1.020
1.036	1.033	1.031	1.028	1.025	1.022	1.019	1.016	1.013	1.010
1.026	1.023	1.021	1.018	1.015	1.012	1.009	1.006	1.003	1.000
1.016	1.014	1.012	1.009	1.006	1.002	0.999	0.996	0.993	0.990
1.007	1.004	1.002	0.999	0.996	0.993	0.990	0.987	0.984	0.981
0.996	0.994	0.992	0.989	0.986	0.983	0.980	0.977	0.974	0.971

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3. SPECIFIC GRAVITY OF SOLUTIONS OF POTASSIUM
 HYDROXIDE AT $\frac{15^{\circ}}{4^{\circ}}$. Calculated from the results
 obtained by Pickering (*Journ. Chem. Soc.*, lxiil., 890).

Specific Gravity.	Degrees Twaddell.	Degrees Baumé.	100 parts by weight contain		1 cb.m. contains kg.	
			K ₂ O.	KOH.	K ₂ O.	KOH.
1·000	0	0	0·00	0·00	0·00	0·00
1·005	1	0·7	0·50	0·60	5·03	6·03
1·010	2	1·4	0·99	1·18	10·00	11·92
1·015	3	2·1	1·45	1·73	14·72	17·56
1·020	4	2·7	1·91	2·28	19·48	23·26
1·025	5	3·4	2·37	2·82	24·29	28·91
1·030	6	4·1	2·82	3·36	29·05	34·61
1·035	7	4·7	3·27	3·90	33·84	40·37
1·040	8	5·4	3·73	4·44	38·79	46·18
1·045	9	6·0	4·19	4·99	43·79	52·15
1·050	10	6·7	4·64	5·53	48·72	58·07
1·055	11	7·4	5·10	6·08	53·81	64·14
1·060	12	8·0	5·54	6·60	58·72	69·96
1·065	13	8·7	6·00	7·15	63·90	76·15
1·070	14	9·4	6·45	7·68	69·02	82·18
1·075	15	10·0	6·90	8·22	74·18	88·37
1·080	16	10·6	7·35	8·76	79·38	94·61
1·085	17	11·2	7·79	9·28	84·52	100·69
1·090	18	11·9	8·24	9·82	89·82	107·04
1·095	19	12·4	8·68	10·37	95·05	113·22
1·100	20	13·0	9·13	10·87	100·43	119·57
1·105	21	13·6	9·62	11·46	106·30	126·63
1·110	22	14·2	10·00	11·92	110·00	132·31
1·115	23	14·9	10·44	12·44	116·41	138·71
1·120	24	15·4	10·88	12·96	121·86	145·15
1·125	25	16·0	11·32	13·48	127·35	151·65
1·130	26	16·5	11·76	14·01	132·89	158·31
1·135	27	17·0	12·21	14·53	138·58	164·92
1·140	28	17·7	12·63	15·04	143·98	171·46
1·145	29	18·3	13·06	15·56	149·53	178·16
1·150	30	18·8	13·50	16·08	155·25	184·92
1·155	31	19·3	13·92	16·58	160·78	191·50
1·160	32	19·8	14·36	17·10	166·58	198·36
1·165	33	20·3	14·79	17·62	172·30	205·27
1·170	34	20·9	15·22	18·13	178·07	212·12
1·175	35	21·4	15·65	18·64	183·89	219·02

SPECIFIC GRAVITY OF SOLUTIONS OF POTASSIUM

HYDROXIDE AT $\frac{15^{\circ}}{4^{\circ}}$ —Continued.

Specific Gravity.	Degrees Twaddell.	Degrees Baumé.	100 parts by weight contain		1 cb.m. contains kg.	
			K ₂ O	KOH.	K ₂ O.	KOH.
1·180	36	22·0	16·08	19·15	189·74	225·97
1·185	37	22·5	16·51	19·66	195·64	232·97
1·190	38	23·0	16·93	20·17	201·47	240·02
1·195	39	23·5	17·35	20·66	207·33	246·89
1·200	40	24·0	17·77	21·17	213·24	254·04
1·205	41	24·5	18·18	21·66	219·07	261·00
1·210	42	25·0	18·60	22·16	225·06	268·14
1·215	43	25·5	19·03	22·67	231·21	275·44
1·220	44	26·0	19·45	23·17	237·29	282·67
1·225	45	26·4	19·86	23·66	243·29	289·84
1·230	46	26·9	20·27	24·14	249·32	296·92
1·235	47	27·4	20·69	24·64	255·52	304·30
1·240	48	27·9	21·10	25·13	261·64	311·61
1·245	49	28·4	21·51	25·62	267·80	318·97
1·250	50	28·8	21·91	26·10	273·88	326·25
1·255	51	29·3	22·32	26·59	280·12	333·70
1·260	52	29·7	22·73	27·07	286·40	341·08
1·265	53	30·2	23·14	27·56	292·72	348·63
1·270	54	30·6	23·54	28·04	298·96	356·11
1·275	55	31·1	23·94	28·52	305·24	363·63
1·280	56	31·5	24·35	29·00	311·68	371·20
1·285	57	32·0	24·75	29·48	318·04	378·82
1·290	58	32·4	25·15	29·96	324·44	386·48
1·295	59	32·8	25·55	30·43	330·87	394·07
1·300	60	33·3	25·95	30·91	337·35	401·83
1·305	61	33·7	26·34	31·37	343·74	409·38
1·310	62	34·2	26·73	31·84	350·16	417·10
1·315	63	34·6	27·13	32·31	356·76	424·88
1·320	64	35·0	27·52	32·78	363·26	432·70
1·325	65	35·4	27·91	33·24	369·81	440·43
1·330	66	35·8	28·29	33·70	376·26	448·21
1·335	67	36·2	28·68	34·16	382·88	456·04
1·240	68	36·6	29·07	34·63	389·54	464·04
1·345	69	37·0	29·46	35·09	396·24	471·96
1·350	70	37·4	29·85	35·55	402·98	479·93
1·355	71	37·8	30·23	36·01	409·62	487·94
1·360	72	38·2	30·61	36·46	416·30	495·86

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SPECIFIC GRAVITY OF SOLUTIONS OF POTASSIUM HYDROXIDE AT $\frac{15^\circ}{4}$ —Continued.

Specific Gravity.	Degrees Twaddell.	Degrees Baumé.	100 parts by weight contain		1 cub. m. contains kg.	
			K ₂ O.	KO.	K ₂ O.	KO.
1.365	73	38.6	30.99	36.92	423.01	503.96
1.370	74	39.0	31.37	37.37	429.77	511.97
1.375	75	39.4	31.76	37.83	436.70	520.16
1.380	76	39.8	32.14	38.28	443.53	528.26
1.385	77	40.1	32.52	38.73	450.40	536.41
1.390	78	40.5	32.89	39.18	457.17	544.60
1.395	79	40.8	33.27	39.63	464.12	552.84
1.400	80	41.2	33.66	40.09	471.24	561.26
1.405	81	41.6	34.03	40.53	478.12	569.45
1.410	82	42.0	34.40	40.98	485.04	577.82
1.415	83	42.3	34.77	41.42	492.00	586.09
1.420	84	42.7	35.15	41.87	499.13	594.55
1.425	85	43.1	35.53	42.32	506.30	603.06
1.430	86	43.4	35.90	42.76	513.37	611.47
1.435	87	43.8	36.27	43.20	520.47	619.92
1.440	88	44.1	36.63	43.63	527.47	628.27
1.445	89	44.4	36.99	44.06	534.51	636.67
1.450	90	44.8	37.36	44.50	541.72	645.25
1.455	91	45.1	37.72	44.93	548.83	653.73
1.460	92	45.4	38.09	45.37	556.11	662.40
1.465	93	45.8	38.45	45.80	563.29	670.97
1.470	94	46.1	38.81	46.23	570.51	679.58
1.475	95	46.4	39.17	46.66	577.76	688.24
1.480	96	46.8	39.54	47.09	585.19	696.93
1.485	97	47.1	39.89	47.51	592.37	705.52
1.490	98	47.4	40.24	47.93	599.58	714.16
1.495	99	47.8	40.60	48.36	606.97	722.98
1.500	100	48.1	40.95	48.78	614.25	731.70
1.505	101	48.4	41.31	49.20	621.72	740.46
1.510	102	48.7	41.68	49.64	629.37	749.56
1.515	103	49.0	42.03	50.06	636.75	758.41
1.520	104	49.4	42.38	50.48	644.18	767.30
1.525	105	49.7	42.73	50.90	651.63	776.23
1.530	106	50.0	43.09	51.32	659.28	785.20
1.535	107	50.3	43.44	51.74	666.80	794.21
1.540	108	50.6	43.78	52.15	674.21	803.11

XI. AMMONIA MANUFACTURE.**A.—Gas-Liquor.**

This liquor generally contains the ammonia, principally in the state of carbonate and sulphide, which can be driven off by boiling, without employing lime or alkali, and which are indicated by alkalimetric testing (*volatile ammonia*). There is, however, always a certain quantity of ammonia present in the state of salts which are not appreciably volatilised by mere boiling, and not indicated by simple testing with standard acid. These are the chloride, thiocyanate, sulphite, thiosulphate, sulphate, ferrocyanide (*fixed ammonia*). No other salts need be enumerated.

For technical purposes, it is sufficient to make the following tests:—

1. *Volatile Ammonia*.—Dilute 20 c.c. of gas-liquor with 100 c.c. water, add 30 c.c. of normal hydrochloric acid, and boil till all CO_2 and H_2S is expelled. Titrate back with seminormal alkali, employing the ordinary indicators. If the liquor is too much coloured to see the change of the indicator, dilute it with water or employ litmus paper. Or else run 10 c.c. of the gas-liquor into a beaker containing 250 c.c. water, add 2 drops methyl orange solution (1:1000), and titrate at once in the cold with normal hydrochloric acid. If the indicator is destroyed by H_2S , add another drop of it. Each c.c. of normal acid corresponds to 0.01703 g. NH_3 or to 0.08515 parts NH_3 by weight in 100 vols. of gas-liquor; or to 0.4216 ounces of rectified oil of vitriol (of 93 per cent. SO_4H_2) per gallon of gas-liquor.

2. *Total Ammonia*.—Put 20 c.c. of gas-liquor, with about as much water, into the flask A, Fig. 16, and charge the receivers B and C with 30 c.c. of normal hydrochloric acid previously diluted to twice its volume. The greater portion of this mixture should be contained in the U-tube B. Make the connection and run 3 c.c. concentrated caustic soda solution into A through the pinch-cock funnel *a*. Apply heat and keep up a gentle distillation for one or two hours, when all NH_3 will be driven off and absorbed in B and C. Unite the contents of these vessels and titrate back with seminormal caustic soda. If *a* c.c. of this are used, $30 - \frac{a}{2}$ indicates the c.c. of acid corresponding to the total ammonia, and calculated as in test No. 1.

3. *Total Sulphur*.—Add bromine water to 100 c.c. of liquor till the colour and smell of bromine are distinct, acidulate with pure

HCl, boil till all bromine has been expelled, filter if necessary, neutralise the solution almost but not quite with pure sodium carbonate, and precipitate the SO_4H_2 formed with BaCl_2 , proceeding as described p. 110.

Sometimes it may be desirable to deduct from the total sulphur that originally present in the gas-liquor as sulphate, which is estimated by boiling the unoxidised gas-liquor with HCl and proceeding as above.

4. *Thiocyanate*.—Evaporate 50 c.c. of gas-liquor to dryness, heat the residue at 100°C . for three or four hours, digest it with strong alcohol, filter, wash on the filter with alcohol, evaporate all the alcoholic solutions to dryness, dissolve in water, filter from

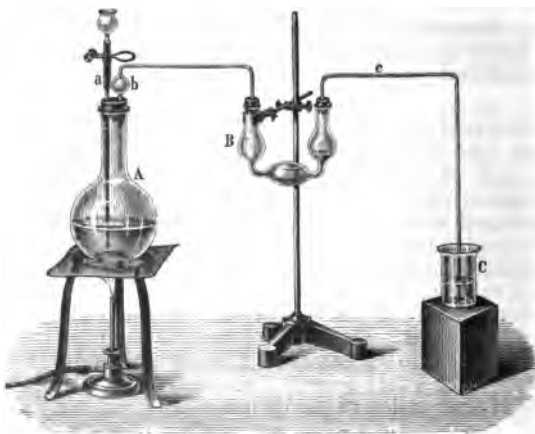


FIG. 16.

any residue, add a mixed solution of sulphurous acid and cupric sulphate, and heat gently, when cuprous thiocyanate will be precipitated. Wash the precipitate into a flask, dissolve it in nitric acid, boil for some time, and precipitate the Cu as CuO by NaOH . The weight of $\text{CuO} \times 0.9561 =$ the equivalent amount of $(\text{NH}_4)_2\text{CNS}$ (Dyson, *S.C.I.*, 1883, p. 231). Or else proceed by titration, employing a solution containing 6.236 g. $\text{CuSO}_4 \cdot 5\text{H}_2\text{O}$ per litre, 1 c.c. of which is equivalent to 0.00145 g. $\text{SCN} = 0.00190 \text{ g. } (\text{NH}_4)_2\text{SCN}$, which is added to a boiling solution, to which some sodium bisulphite has been added, till a drop of the mixture, brought into contact with a drop of a solution of potassium ferrocyanide in 20 parts of water, produces *immediately* a brown coloration (Barnes and Liddell, *S.C.I.*, 1883, p. 122).

B.—Sulphate of Ammonia.

1. *Estimation of Ammonia.*—The average sample, carefully drawn, is well ground up, passed completely through a sieve with 10 holes to the linear inch, and a smaller sample is taken from this. Weigh 17.03 g. of the latter sample in a stoppered tube, dissolve and dilute to 500 c.c., and place 50 c.c. of the solution without filtration into the apparatus, Fig. 16 (p. 216). The test is carried out exactly as in A, No. 2. Each c.c. of the quantity $30 - \frac{a}{2}$ is = 0.01703 g. NH_3 or = 1.0 per cent. The analysis of sulphate of ammonia is, however, best performed by the bromine method, in which the NH_3 is converted into nitrogen. This



FIG. 17.



FIG. 18.

method can be carried out in the "Azotometer," or in Lunge's gas-volumeter (p. 139), if the latter is provided with a "decomposing flask," as shown in Fig. 17. The necessary "brominated soda" is prepared by dissolving 100 g. 70 per cent. caustic soda in 1250 g. water, and cautiously adding 25 g. bromine. The reagent must be kept in a dark, cool place, but even then does not keep more than a few days. The ammonium salt, preferably dissolved in water, is introduced into the outer space of the decomposing flask *a*, Fig. 18, and 25 or 30 c.c. brominated soda poured into the inner vessel *b*. The cork *f*, having been already attached to the

volumeter-tube by means of a short rubber tube, is pressed tightly down into the flask *a*, taking hold of this only by the neck; the pressure thus produced is relieved by momentarily pulling out the stopper of the volumeter-tap *e*. If thereby the mercury in *A* should sink a little, it is brought back to the zero point by raising the "level-tube," while *A* communicates through *d* with the outer air. When the temperatures are equalised and the mercury is up to the tap, this is put in such a position that *a* communicates through *c* with *A*; then the flask *a* is tilted so that the contents of *b* run into the outer space; the flask is then shaken till no more gas is evolved. The mercury levels in *A* and the level-tube are made to coincide, after waiting a quarter, or better, half an hour, in order to cool down the flask. (This may be expedited by placing *a* both before and after the operation, in a large vessel filled with water of the temperature of the room.) When the levels have been exactly adjusted, as described p. 140, so as to bring the gas to the volume it would occupy at 0° and 760 mm. in the dry state, read off the number of c.c. of gas in *A*; each c.c. = 0.0012818 g. N = 0.0015582 g. NH₃ (this includes the necessary correction for absorption or incomplete evolution of N). In order to save all calculations, dissolve 1.558 g. sulphate of ammonia in 100 c.c. of water, and employ 10 c.c. = 0.1558 g. for each test; in this case each c.c. of gas contained in *A* = 1 per cent. NH₃.

2. *Thiocyanate*.—*Cf.* p. 216, *A*, No. 4.

C.—Liquor Ammonia.

This is mostly sold by specific gravity, the relation of which to the percentage of NH₃ is shown in the subjoined table, No. 1.

The *empyreumatic* substances in liquor ammonia are detected qualitatively by the smell on exact neutralisation with sulphuric acid. The *pyridine bases* (which do not redden phenolphthalein) can be tested for by the method of Pennock and Morton (*Journ. Amer. Chem. Soc.*, vol. xxiv., p. 377). Neutralise 100 c.c. of the liquor exactly by sulphuric acid, employing methyl orange as indicator and cooling the vessel used from the outside; distil into a flask charged with 30 c.c. water until this volume has increased to about 100 c.c., add phenolphthalein and a solution of mercuric chloride until the liquid is decolorised, then a few more drops of the mercury solution (thereby precipitating the NH₃), filter, and titrate with decinormal acid and methyl orange, each c.c. of which = 0.0079 g. pyridine.

The testing of *liquid ammonia*, as sent out in iron bottles, is described in *Tech. Meth.*, vol. ii.

**1. SPECIFIC GRAVITIES OF SOLUTIONS OF AMMONIA
AT 15°. (Lunge and Wiernik.)**

Specific Gravity.	Per cent. NH ₃ .	1 litre contains grams NH ₃ at 15°.	Correction of specific gravity for ± 1° C.
1·000	0·00	0·00	0·00018
0·995	1·14	11·34	0·00019
0·990	2·31	22·87	0·00020
0·985	3·55	34·97	0·00021
0·980	4·80	47·04	0·00023
0·975	6·05	58·99	0·00024
0·970	7·31	70·91	0·00025
0·965	8·59	82·89	0·00026 ₅
0·960	9·91	95·13	0·00029
0·955	11·32	108·11	0·00031 ₅
0·950	12·74	121·03	0·00034 ₅
0·945	14·17	133·91	0·00036 ₅
0·940	15·63	146·92	0·00039
0·935	17·12	160·07	0·00041
0·930	18·64	173·35	0·00042
0·925	20·18	186·67	0·00044 ₅
0·920	21·75	200·10	0·00047
0·915	23·35	213·65	0·00049 ₅
0·910	24·99	227·41	0·00052
0·905	26·64	241·09	0·00054 ₅
0·900	28·33	254·97	0·00057
0·895	30·03	268·77	0·00059 ₅
0·890	31·73	282·40	0·00061
0·885	33·67	297·98	0·00063 ₅
0·880	35·60	313·28	0·00066

2. SPECIFIC GRAVITIES OF SOLUTIONS OF COMMERCIAL AMMONIUM CARBONATE, AT 15° C. (Lunge and Smith.)

Degrees Twaddell.	Degrees Baumé.	Specific Gravity at 15°.	Per cent. Commercial Ammonium Carbonate.	Change of Specific Gravity for $\pm 1^\circ \text{C}$.
1	0·6	1·005	1·66	0·0002
2	1·4	1·010	3·18	0·0002
3	2·1	1·015	4·60	0·0003
4	2·7	1·020	6·04	0·0003
5	3·4	1·025	7·49	0·0003
6	4·1	1·030	8·93	0·0004
7	4·7	1·035	10·35	0·0004
8	5·4	1·040	11·86	0·0004
9	6·0	1·045	13·36	0·0005
10	6·7	1·050	14·83	0·0005
11	7·4	1·055	16·16	0·0005
12	8·0	1·060	17·70	0·0005
13	8·7	1·065	19·18	0·0005
14	9·4	1·070	20·70	0·0005
15	10·0	1·075	22·25	0·0006
16	10·6	1·080	23·78	0·0006
17	11·2	1·085	25·31	0·0007
18	11·9	1·090	26·82	0·0007
19	12·4	1·095	28·33	0·0007
20	13·0	1·100	29·93	0·0007
21	13·6	1·105	31·77	0·0007
22	14·2	1·110	33·45	0·0007
23	14·9	1·115	35·08	0·0007
24	15·4	1·120	36·88	0·0007
25	16·0	1·125	38·71	0·0007
26	16·5	1·130	40·34	0·0007
27	17·1	1·135	42·20	0·0007
28	17·8	1·140	44·29	0·0007
29	17·9	1·1414	44·90	0·0007

**XII. MANUFACTURE OF COAL-GAS
(ILLUMINATING GAS).**

A.—Coal-Gas.

For a satisfactory analysis of coal-gas the Orsat apparatus is not sufficiently accurate, and the gas-burettes of Bunte, Hempel, Drehschmidt, or Pfeiffer should be used. The following rules are

taken from the private notes, printed for Professor Bunte's students, with his permission.

The analysis is performed by means of Bunte burettes, which must satisfy the following conditions:—The capillary tube below the bottom tap must not allow any water to come out, even on shaking. The upper (three-way) tap must be made so as to shut off communication with any one of the three outlets. (The Greiner-Friedrichs patent tap, with two oblique bores, as shown in Fig. 15, admits of doing this without any difficulty.) The taps should be greased with a mixture of 2 parts para-gum, 2 parts bees' wax, and 10 parts tallow, and they must be tight even in a strong vacuum. The confining water must have the temperature of the room, and this must remain unchanged during the whole time occupied by the work. The burette must be held only at the top funnel or at the capillary tubes. The correctness of its graduation must be controlled by running out its contents of water in portions of 10 c.c., and weighing these. When one of the components of the gas has been absorbed, first allow the water to rise from below and then adjust the pressure by allowing water to run in from the top funnel. To do this, fill it to the mark, open the tap and wait a minute, until the surface of the water inside the burette remains constant.

To take a sample of the gas to be tested, employ either an empty burette, or one filled with water. In the former case, connect the top tap (the funnel being charged with water) sideways with the gas-holder or pipe, the bottom tap being open, and allow the gas to pass through, until it has driven out all the air; then shut first the bottom tap and immediately afterwards the top tap. In the second case fill the burette with water, connect the top tap with the gas-holder or pipe, open the bottom tap, until the water has sunk a little below the zero mark, then shut first the top tap and afterwards the bottom tap.

If the gas is at a lower pressure than the atmospheric pressure, take the sample by means of a rubber bellows, or a water aspirating bottle, or a water-pump, and connect then with the bottom capillary.

Measuring the gas in the burette.—Adjust the three-way tap so that all its bores are closed, fill the funnel with water up to the mark, connect the rubber tube of the pressure bottle (levelling bottle), previously entirely filled with water, with the bottom tap, and allow the water to rise up to about 0.2 c.c. above the zero mark. Now open the three-way tap, whereupon a little gas escapes and the pressures are equalised. The water then usually stands at the zero mark; if not, read the actual volume and calculate from this. Then turn the three-way tap, after having put a short rubber tube on its lateral outlet, so as to run a little water into this, and close the tube by a small piece of glass rod. As long as the tap is not used, it remains in this position.

Introduction of the absorbing liquids.—Draw off the confining liquid by means of the aspirating bottle, holding the bottom tap fast in its position, and shutting it at once when the water has got down to the capillary. Take the rubber tube off and draw the liquid back into the aspirating bottle, lest it should syphon itself off. Then pour the absorbing liquid into a small porcelain capsule, and allow it to rise in the burette.

The individual constituents are estimated, *seriatim*, as follows:—

1. *Carbon Dioxide*, CO_2 , by absorption with a solution of caustic potash, 1 in 3 water—that is, specific gravity 1.23. Of this 1 c.c. takes up 90-100 c.c. CO_2 . It is sufficient, if the inside of the burette is once wetted with the solution. Afterwards water is allowed to enter from below and to run in from the top, to wash the glass; then the normal pressure is re-established and the volume read off. In the case of crude gas the H_2S must be first removed by a tube containing pumice soaked with cupric sulphate.

2. *Heavy hydrocarbons*, C_mH_n .—Draw off the confining water as completely as possible, rinse off the potash solution with a little water (which is also drawn off), allow about 10 c.c. of water, saturated with bromine, to enter, and shake the burette. When the space above the liquid ceases to show the brown colour of the bromine, draw off the liquid and replace it by fresh bromine water. Finally, in order to absorb the bromine vapour, draw about 1 c.c. of caustic potash solution into the burette, shake this up in the burette, allow a little water to run in at the top, establish the normal pressure, and read off the volume. Thus all the illuminants are absorbed—*i.e.*, ethylene and the other unsaturated hydrocarbons, also benzene vapour.

3. *Oxygen* is absorbed by drawing in about 2.5 c.c. of a solution of pyrogallol (1 to 5 water) and after this 7.5 c.c. caustic potash solution (1:3). Shake well for five minutes, run in water through the funnel until the pressure is equalised, shake again, and continue this until no more water will enter the burette. Run off the dark liquid at the bottom, allowing water to run in at the top, so that a layer of clear water remains at the top, which allows a correct reading after re-establishing the pressure.

Accurate estimations of oxygen are made by titration with potassium iodide, manganous chloride, and thiosulphate, as described in *Tech. Meth.*, vol. ii.

4. *Carbon monoxide*.—Draw off the confining water, wash with more water, draw in 10 c.c. ammoniacal solution of cuprous chloride (made by dissolving 200 g. commercial cuprous chloride and 250 ammonium chloride in 750 water, placing a copper spiral in the bottle and before use mixing 3 vols. of this solution with 1 vol. liquor ammoniæ specific gravity 0.905), shake for one minute, draw off the solution, replace it by a fresh quantity, shake again, and repeat this procedure at least twice. After the last removal

of the absorbent run through the funnel 3 or 4 c.c. concentrated hydrochloric acid, and then a little water, which forms a layer at the top. Draw off the liquid, wash with water, draw in 1 or 2 c.c. concentrated potash solution, shake up, allow some water to enter, re-establish the normal pressure, and take the reading.

5. *Hydrogen*.—The gas now contains nothing but H, CH₄, and N. The hydrogen is estimated by fractional combustion, for which purpose a second burette (B) is needed. Measure in the first burette (A) 22 to 25 c.c. of the residual gas under normal pressure, and mix with air for burning the hydrogen. For this purpose open first the bottom tap, then the top tap, so as to communicate outwards, whereupon water will run out and air enter. When the level of the water has gone down to about 5 c.c. below 0, quickly shut the top tap and after this the bottom tap, mix the gases by shaking, regulate the pressure to that of the atmosphere plus that of the column of water in the funnel, and read the volume. Now fill burette B up to the capillary and connect both three-way taps, interposing a *palladium tube* C between them. C is a tube of glass of high melting point, 10 c.c. long, 3 mm. bore, and 5 mm. thick. It contains 100 mm. of palladium wire, 0.3 mm. thick, folded into four and introduced into the central part of tube C. By heating this part of the tube, it is made to collapse and to hold the wire fast; the remaining portion of C is loosely filled with long fibrous asbestos. The connection between C and the capillaries of A and B is made by short, thick-walled rubber tubing.

Now turn both three-way taps so that both are closed, fill the funnel of burette A with water, lower the pressure by opening the bottom tap for a moment, turn both three-way taps at the same time and quickly, so that C communicates with the interior of both burettes, and heat C. The air in C thus increases its volume, and forces the water in the capillaries back into both burettes. Now connect the rubber tube of the pressure bottle with the lower tap of A, open this tap, heat C at its narrowed part until the small flame turns yellow, and open the lower tap of B, so that the gas passes from A through C into B in a moderately quick current. The water should issue from B in a continuous jet, not in single drops, and the palladium wire should not become red-hot on the side where the gas enters; otherwise some methane would be burnt together with the hydrogen. As soon as the water has got to the top of burette A, quickly shut first the bottom tap of A and then that of B, and syphon the gas back from B to A as described above. After cooling, the pressure in A is made equal to the normal; the volume is then read, and the contraction ascertained.

Example: 100 c.c. coal gas, taken for analysis, after absorbing CO₂, heavy hydrocarbons, O and CO, left 85 c.c. Of this 22.2 c.c. were transferred to burette A, and diluted with air to 105.3.

After the combustion the volume was 86.3, showing a contraction of 19.0. Calculating this upon 100 c.c. of the original gas, we find $\frac{19.0 \times 85.0}{22.2} = 72.8$.

Therefore the hydrogen amounts to $\frac{2 \times 72.8}{3} = 48.5$ per cent.

As a final control, estimate the oxygen left after combustion; it must be less than that originally employed by two-thirds of the contraction observed.

6. *Methane* is estimated, together with hydrogen, by burning another portion of the gas remaining after the operations 1 to 4, in the "explosion burette." For this, measure off 12 to 15 c.c. of this gas, draw in an excess of air, shake up, ascertain the volume, draw off the confining water, explode by means of an electric spark (generated by a battery and induction coil), ascertain the contraction, let 1 or 2 c.c. potash solution run down inside the burette, and after this, slowly, some water, adjust the pressure and ascertain the total contraction, which is equal to $H_2O + CO_2$. From this deduct the amount corresponding to the hydrogen found in No. 5; one-third of the remaining contraction corresponds to the methane, for 1 vol. $CH_4 + 2$ vols. $O_2 = 0$ vols. $CO_2 + 0$ vols. H_2O .

Example: Residual gas employed 12.7 c.c. (forming part of the 86 c.c. remaining after the absorption of CO_2 , C_mH_n , O_2 , and CO); after addition of air = 104.1, therefore air employed = 91.4. After the explosion 78.9 c.c. gas; therefore contraction = 25.2; calculated upon the total gas $\frac{85 \times 25.2}{12.7} = 168.8$. From this deduct

the contraction due to hydrogen, according to No. 5, = 72.8; this leaves for the methane a contraction of $168.8 - 72.8 = 96.0$, or one-third of it = 32.0 per cent. methane.

7. *Nitrogen* is represented by the deficit from 100 after estimating all the other constituents. Suppose we have found:—

From No. 1,	2.0	per cent.	(by volume	CO)
" "	2,	4.0	"	heavy hydrocarbons
" "	3,	0.4	"	O_2
" "	4,	8.6	"	CO
<hr style="width: 20%; margin: 0 auto;"/>				
Together	15.0	"		
From No. 5,	48.0	"	H_2	
" "	6,	32.0	"	CH_4
<hr style="width: 20%; margin: 0 auto;"/>				
Leaving	95.0	"		
	5.0	"	for	N_2

The estimation of ethylene, benzene, acetylene, naphthalene, hydrogen sulphide, total sulphur, ammonia, cyanogen, etc., is described in Lunge-Keane's *Tech. Meth. of Chem. Anal.*, vol. ii.

The calorific power of coal-gas is best ascertained by means of the Juncker's calorimeter, which is always sold with instructions for use.

B. Purifying Material (Spent Oxide).

1. *Cyanogen* (Bueb).—Boil 20 g. of an average sample of spent oxide (from which the sulphur has been previously extracted as below) or the same quantity of pressed "cyanide mud" with 100 c.c. caustic potash solution (specific gravity 1.26) and 200 c.c. water for half an hour, dilute to 1010 c.c. (reckoning 10 c.c. for the volume of the solid substance) and pass through a dry filter. Take 25 c.c. of the filtrate, add 50 c.c. water and 10 c.c. dilute sulphuric acid (1:10), and titrate with *zinc solution*. This solution is made as follows:—Dissolve 10.2 g. of pure crystallised zinc sulphate ($\text{ZnSO}_4 \cdot 7\text{H}_2\text{O}$), together with 10 c.c. sulphuric acid of specific gravity 1.7 in water, and make up to 1 litre, and compare this with a freshly made solution of 10 g. pure crystallised potassium ferrocyanide in 1 litre, in the following manner: To 25 c.c. of the ferrocyanide solution add 50 c.c. water and 10 c.c. dilute sulphuric acid. This mixture is titrated with the zinc solution, testing for the completion of the reaction by drops put on to filter paper (preferably Schleicher and Schüll's, No. 601, mark S) soaked with a 1 per cent. solution of ferric chloride. The end of the reaction is reached when no blue coloration is produced on the paper.

Other methods for the estimation of cyanides (described by Knublauch and by Drehschmidt) are given in *Tech. Meth.*, vol. i. and vol. ii.

2. *Sulphur*.—Extract 15 g. of the air-dried mass in a Soxhlet apparatus with 100 c.c. carbon disulphide in a 200 c.c. round-bottomed flask of known weight. Heat on a water-bath, condensing the vapours by a reflux condenser, until twenty extractions have been made. Distil off the CS_2 , remove the last portions by hot air, and after cooling again weigh the flask. The difference between the weighings = S.

Sometimes it is desirable to know the amount of S which on burning the oxide forms SO_2 , since a certain quantity of S is always retained by lime, etc., on burning the spent mass. For this purpose Pfeiffer burns 1 g. of the sample, by putting a piece of tinder in a litre flask filled with oxygen and previously charged with 25 or 30 c.c. of normal caustic soda solution. Finally he adds 1 c.c. neutral 30 per cent. hydrogen peroxide and titrates back with standard HCl and methyl orange. Each c.c. of the normal soda solution consumed corresponds to 1.6 per cent. of S burnt.

Processes for estimating all the essential constituents of spent oxide are described in *Tech. Meth.*, vol. ii.

XIII. CALCIUM CARBIDE AND ACETYLENE.

A.—Raw Materials.

- (a) *Coke*, see p. 95.
 (b) *Limestone*, see p. 155.

B.—Technical Calcium Carbide.

(a) *The sampling* in this case has to be done with special care, since it is anything but easy to obtain a small sample representing the real average quality. The sample is quickly crushed in an iron mortar, provided with a rubber cover, or in a coffee-mill, and the powder must be kept free from contact with air.

(b) *The estimation of the yield of gas* should always be made by actual measurement of the gas, not by loss of weight. Take 50 g. carbide, and put it into a glass tube, 2 or 3 cm. wide inside, which is connected with the gas-generating flask (250 c.c.) by a rubber tube so that the carbide can be dropped in small quantities into the flask. 150 c.c. water, previously saturated with acetylene, are first placed in the flask, the cork of which is also provided with an exit-tube connected with a measuring bottle. This bottle holds 20 litres, and has a division on which $\frac{1}{4}$ litre can be read off. It is connected by means of a lateral neck just over the bottom and by a rubber tube with a level-bottle of the same size, filled with water saturated with acetylene. By raising the level flask, the water is forced into the measuring flask up to its neck; during the time the gas is given off, the level flask is lowered, so that there is never any notable pressure in the measuring bottle. When all the gas has been collected in the latter, the level-bottle is placed so that the water is exactly at the same level in both bottles, and about two hours are allowed for the temperature to reach that of the surrounding air. Read the thermometer and barometer, and reduce the volume of the gas by the table, pp. 38 to 44, to the normal state, regarding it as saturated with moisture. If, as usual, the reduction is to be made not to 0°, but to 15° C., this can be done with sufficient accuracy by the formula:—

$$V = \frac{v}{100} (140.2 - 0.6 t) \frac{B}{100}$$

where V is the volume at 15°, v the volume at t° , and B the (corrected height) of the barometer. (Cf. *Tech. Meth.*, vol. ii.)

(c) *Impurities*.—It is best to test for these, not in the carbide, but in the acetylene given off from it. Put 70 or 80 g. carbide, crushed to the size of a pea, into a previously weighed, well-dried,

half-litre flask, and weigh it on an ordinary balance which turns to 0.1 g. The cork of this flask is fitted with a dropping funnel, contracted at the outlet, with glass tap, and with a side tube connected with a ten-bulb tube, like that shown in Fig. 8, p. 120. The latter contains 75 cm. of a 2 to 3 per cent. solution of sodium hypochlorite. Run from the funnel three to seven drops of water on to the carbide, and shake the flask gently from time to time. The gas should all be liberated in three or four hours; it may, if required, be measured, or else allowed to escape. Then the flask is filled up to its neck, so as to drive all the gas into the bulb-tube, and in the contents of the latter the phosphoric acid which has been formed by the hypochlorite from the *hydrogen phosphide* contained in the gas, is estimated by the ordinary magnesia method.

If it is required to estimate the *sulphur* also, which escapes principally as H_2S , divide the contents of the bulb-tube in two portions, estimate in one of these the phosphoric acid as above, and in the other the sulphuric acid, formed from the H_2S , as $BaSO_4$.

XIV. EXAMINATION OF THE RAW MATERIALS AND PRODUCTS OF THE MANUFACTURE OF FERTILISERS.

N.B.—This section is based on the resolutions agreed to at the Fifth International Congress of Applied Chemistry at Berlin (1903).

A.—Sampling.

Samples must be taken out of every tenth sack in the case of shipments in bulk, in at least ten places, by means of the sampling-auger, described on pp. 249, 250; in the case of ship cargoes, from every fiftieth tub; the total weight to be about 300 g. for each of the three normal samples. In the case of unequal composition, the samples must be ground and mixed; in the case of moist fertilisers, this must be done by hand.

B.—Moisture.

Moisture in crude phosphates, bone charcoal, etc., is estimated by drying 10 g. at 100° up to constancy of weight; in the case of gypsum, during three hours. If the substance alters its percentage of moisture during grinding, the moisture must be determined both in the coarsely crushed and in the finely ground sample, and the

result of the analysis is to be calculated on the original coarsely crushed sample.

C.—The Insoluble Matter.

The insoluble matter is determined in 10 g. of the sample, (a) When dissolving in mineral acids, after rendering the silica insoluble by heating on the water-bath during several hours, or on the air-bath to 120° ; the residue must be ignited. (b) When dissolving in water the residue must be dried at 100° up to constancy of weight.

D.—Phosphoric Acid.

1. Preparation of the Solutions.

(a) *Phosphates soluble in water*.—Shake 20 g. in a litre flask with about 800 g. water for half an hour, and fill up to the mark. Solutions of so-called double superphosphates must be boiled with addition of nitric acid (10 c.c. concentrated nitric acid to 25 c.c. of the solution) before precipitating the phosphoric acid, in order to convert any pyrophosphoric acid present into orthophosphoric acid.

(b) *Phosphates soluble in Ammonium Citrate* are treated according to Petermann's method. With superphosphates containing upwards of 20 per cent. P_2O_5 , take 1 g., when containing 12 to 20 per cent. P_2O_5 , 2 g.; if there is less than 10 per cent., P_2O_5 , and, in the case of composite fertilisers, 4 g. for each sample. Grind it first dry, then with 20 to 25 c.c. water, decant on to a filter, and wash with water until the volume of the filtrate is about 200 c.c. If the filtrate is not quite clear, add a drop of nitric acid. Put the filter and residue into a 250 flask, add 100 c.c. of the ammonium citrate solution (prepared as below), digest about fifteen hours at the ordinary temperature, with frequent shaking, then one hour at 40° , allow to cool, fill up to the mark, take 50 c.c. of the filtrate and 50 c.c. of the above aqueous solution, mix these, boil with 10 c.c. concentrated nitric acid for ten minutes, and estimate the total phosphoric acid soluble in water and in citrate by the molybdenum or the citrate method.

Preparation of the Ammonium Citrate solution.—Dissolve 500 g. citric acid in water, neutralise with ammonia, allow to cool, reduce the specific gravity to 1.09, and add to a litre of this solution 50 c.c. liquor ammoniæ, specific gravity 0.92. The specific gravity of the final solution should be from 1.082 to 1.083.

(c) *Total Phosphoric Acid*.—Boil 5 g. with a mixture of three parts hydrochloric acid, specific gravity 1.12, and 1 part nitric acid, specific gravity 1.20, or with 20 c.c. concentrated nitric acid and 50 c.c. concentrated sulphuric acid for half an hour and make up to 250 c.c.

(d) In *Thomas-Slag Phosphates* the phosphoric acid is estimated in the portion which passes through a 2 millimetre sieve, but the result is calculated upon the whole sample, including the coarser portion. The following estimations are made:—

1. *Phosphoric acid soluble in citric acid.*—Shake 5 g. Thomas phosphate in a half-litre flask, previously charged with 5 c.c. alcohol, with a 2 per cent. solution of pure citric acid during half an hour at $17\frac{1}{2}^{\circ}$, in a revolving agitator which makes thirty to forty revolutions per minute.

2. *Total phosphoric acid.*—Soak 10 g. Thomas phosphate (for the analysis of fine flour passed through sieve No. 100 = 0.19 mm. mesh) in a half-litre flask with 5 c.c. water, then boil with 50 c.c. concentrated sulphuric acid half an hour, stirring frequently, and fill up to the mark.

2. Examination of the Solutions.

For phosphoric acid, according to one of the following methods:—

(a) *Molybdenum method*, according to Wagner. To 25 or 50 c.c. solution, free from silica and containing from 0.1 to 0.2 g. P_2O_5 , add so much concentrated solution of ammonium nitrate (750 g. per litre) and so much molybdenum solution (150 g. ammonium molybdate, dissolved in 1 litre water and poured into 1 litre nitric acid of specific gravity 1.2) that the total liquid contains 15 per cent. ammonium nitrate, and for each 0.1 g. P_2O_5 , not less than 50 c.c. molybdenum solution. Heat to 80° or 90° for ten minutes, put aside for an hour, filter, wash the precipitate with dilute solution of ammonium nitrate (150 g. $(NH_4)NO_3$ + 10 c.c. nitric acid in 1 litre) until there is no reaction for calcium, pierce the filter, wash the precipitate into a beaker by means of a $2\frac{1}{2}$ per cent. liquor ammoniæ, dissolve it by stirring, and add so much ammonia that the total volume is 75 c.c. Then add for each 0.1 g. P_2O_5 , 10 c.c. of magnesium mixture (55 g. crystallised magnesium chloride + 70 g. ammonium chloride, dissolved in 1 litre of 2.5 per cent. liquor ammoniæ), in single drops, stirring constantly, cover the beaker, allow to stand for two hours, filter the precipitate, wash it with 2.5 per cent. ammonia until the reaction for chlorine ceases, and dry at 100° . Detach the precipitate from the filter, place it in a platinum crucible, add the rolled-up filter, and carbonise it in a covered crucible; then heat the crucible for ten minutes in an upright position over the Bunsen flame and for five minutes on the blow-pipe.

(b) *Citrate method.*—In the case of aqueous solutions of superphosphate, employ 50 c.c. citrate solution for 50 c.c. of the phosphate solution, corresponding to 1 g. substance; in that of acid solutions of bone meal, fish guano, Thomas-slag, flour, etc., take 100 c.c. of the citrate solution for 50 c.c. of the phosphate solution ($=\frac{1}{2}$ g. substance). The *citrate solution* is made by dissolving 1100

g. pure citric acid in water, adding 4 litres of 24 per cent. liquor ammoniæ, and making up to 10 litres. After adding the citrate solution, add *at once* 25 c.c. magnesium mixture (550 g. magnesium chloride + 1050 ammonium chloride, dissolved in $6\frac{1}{2}$ litres water + 3½ litres 27 per cent. liquor ammoniæ), and shake or stir for half an hour. Filter the precipitate, preferably by means of a Gooch or Neubauer crucible (see below), rinse the beaker with 5 per cent. liquor ammoniæ, and wash the precipitate five or six times with the same solution, using a filter pump. Dry the crucible on a hot plate until the mass begins to crack, ignite for three to five minutes (preferably in a Roessler furnace), and allow to cool in a desiccator. After weighing, the crucible may at once be used for a fresh determination, without removing the precipitate, and thus thirty or forty estimations can be made in it without renewing the asbestos filter.

This method involves several errors, which, however, compensate one another, so that when the above details are strictly adhered to, the final result is perfectly correct. According to the resolutions of the Union of the German Agricultural Research Stations in 1903, the citrate method is the only one admissible for all fertilisers, except crude phosphates.

The preparation of a Gooch crucible—that is, a platinum crucible with platinum sieve and asbestos filter—is a little troublesome; it is described in *Tech. Meth.*, vol. i.

The Neubauer crucible (sold by N. L. C. Heræus, Hanau), is similar to the Gooch crucible, but contains a platinum sponge filter on the sieve. It is ready for use, as obtained from the dealers, and is much more convenient than a Gooch crucible.

E.—Free Acids.

(a) The total free acid is estimated by titration with caustic soda solution and methyl orange.

(b) Free phosphoric acid is estimated gravimetrically in the alcoholic extract, as described above.

F.—Ferric Oxide and Alumina.

In Germany the accepted method is that of E. Glaser. Dissolve 5 g. phosphate in 25 c.c. nitric acid (specific gravity 1·2) + 12·5 c.c. hydrochloric acid (specific gravity 1·12), and dilute to 500 c.c. Put 100 c.c. (= 1 g. of the phosphate) in a 250 c.c. flask, add 25 c.c. concentrated sulphuric acid (specific gravity 1·84); after five minutes' shaking add 100 c.c. 95 per cent. alcohol, allow to cool, fill up to the mark with alcohol, shake well, and fill up again. After waiting for half an hour, filter, heat 100 c.c. of the filtrate in a platinum dish until the alcohol is driven off, transfer to a beaker, add 50 c.c. water, and heat to boiling. Remove the flame, add NH_3 till the reaction is alkaline, boil off the excess of NH_3 , allow

to cool, filter, wash with hot water, ignite, and weigh. The weight found is assumed to be aluminium phosphate + ferric phosphate, or 50 per cent. of it = $\text{Fe}_2\text{O}_3 + \text{Al}_2\text{O}_3$.

G.—Nitrogen.

1. *Nitric-nitrogen* is estimated gas-volumetrically by the nitrometer (pp. 136 and 139), or by Schloesing-Grandeau's method (*Tech. Meth.*, vol. ii.), or by one of the methods for reducing it to NH_3 . The following method is due to Ulsch. Into a flat-bottomed half-litre flask put 25 c.c. of the aqueous nitrate solution (which ought to contain at most 0.5 g. $\text{KNO}_3 = 0.4$ g. NaNO_3) and 10 c.c. dilute sulphuric acid (1 vol. concentrated acid + 2 vols. water), add 5 g. commercial "ferrum hydrogenio reductum" (iron reduced by hydrogen), and close the flask with a pear-shaped glass vessel of 25 c.c. capacity filled with water, which at the same time serves as a reflux condenser. Heat first cautiously, then more strongly, at least for half a minute to full boiling (altogether five minutes), dilute with 50 c.c. water, add 20 c.c. caustic soda solution (specific gravity 1.25), and distil the NH_3 formed into titrated hydrochloric or sulphuric acid. The distillation may be finished in five to seven minutes after the commencement of the boiling. By titrating back the excess of acid the quantity of NH_3 is ascertained; each c.c. normal acid saturated = 0.01401 g. N or 0.06302 HNO_3 or 0.10116 KNO_3 or 0.08506 NaNO_3 .

2. *Ammoniacal nitrogen*, cf. p. 217. Preferably distil with freshly calcined magnesia, 3 g. to 1 g. NH_3 . In the case of ammoniacal superphosphates, the solution prepared as on p. 228 should be used.

3. *Total nitrogen* is estimated in presence of nitrates by Kjeldahl-Jodlbauer's method. Place 1 g. substance in a 350 c.c. flask of difficultly fusible glass, slowly add 30 c.c. phenolsulphuric acid (made by dissolving 200 g. P_2O_5 in 500 c.c. concentrated sulphuric acid, and 40 g. phenol in 500 c.c. concentrated sulphuric acid, and uniting the two solutions, after cooling), shaking continuously, and cooling by placing the flask in cold water. When finished, agitate for another half-hour or hour, add a drop of mercury (about 1 g.), and then gradually 2 to 3 g. dried zinc dust, with good agitation and cooling. Allow to stand for one or two hours; then boil until the solution has become clear and colourless, allow to cool, wash with water into a distilling flask, add 110 c.c. of caustic soda solution of specific gravity 1.285 (which must be free from nitrogen compounds), distil the NH_3 into normal hydrochloric acid, and estimate it by retitrating. The calculation is made as above, *sub G*, 1.

Damp substances are ground up with a little gypsum before adding the phenolsulphuric acid.

4. *Organic nitrogen*, in the absence of nitrates and ammonium salts, is estimated according to Kjeldahl-Wilfarth's method. Put 1 g. substance in a 150 c.c. long-necked flask of Bohemian glass, add a drop of mercury and 25 c.c. of concentrated sulphuric acid, to a litre of which 200 g. P_2O_5 and 15 g. K_2SO_4 have been added. Heat at first slowly, then to violent boiling, putting the flask, or several flasks, on a wire gauze in a slanting position. The whole is best placed on a sheet of lead with turned-up edges, covered with a thick layer of sand and placed under a hood, so that no damage is done if a flask is cracked. In the case of badly frothing liquids put a little paraffin in the flask and close this loosely by a Kreuzler's stopper, i.e., a glass tube drawn out below into a long point, and sealed at the bottom. Continue the boiling until the contents of the flask are quite clear, which may take half an hour to three hours. Then wash its contents by the aid of 200 c.c. water into a half-litre flask, add 25 c.c. caustic soda solution of specific gravity 1.285 (free from N) and 1 to 1.5 g. zinc dust, and distil into titrated HCl, proceeding just as in No. 1.

In the case of substances which cannot be finely ground, prepare a good average sample by weighing off 3 to 5 g., boil with 50 to 60 c.c. sulphuric acid and 2 to 3 g. mercury, wash, after cooling, into a 300 c.c. flask, filling this up to the mark, mix by shaking, and take 100 c.c. for the distillation with caustic soda and zinc dust.

H.—Potash.

Potash is estimated as in potassium chloride containing sulphate, p. 203, or by the perchloric acid method, *Tech. Meth.*, vol. i. and vol. ii.

Details for the examination of the various fertilisers, *ibid.*

XV. ALUMINA PREPARATIONS.

A.—Raw Materials.

1. *Kaolin (china clay)*, see p. 236, sub "Clay."
2. *Bauxite (a)*.—Dry 2.500 g. at 100° for eight hours, boil with 30 c.c. of a mixture of 1 part concentrated sulphuric acid + 1 water with good agitation, until vapours of SO_3 begin to escape, allow to cool, run the paste slowly into 300 c.c. cold water so as to prevent heating (which would cause a precipitation of TiO_2), add 10 c.c. hydrochloric acid, digest six hours with agitation, filter the solution (a) from the precipitated crude silica and make it, with the washings, up to 500 c.c. Ignite the crude silica, weigh it, evaporate with 2 c.c. hydrofluoric acid and three drops of dilute

sulphuric acid, and ignite; the residue is weighed as Al_2O_3 , and by deducting it from the crude silica we obtain the pure SiO_2 .

(b) Take 200 c.c. of the solution (a) (= 1.000 g. bauxite), neutralise with sodium carbonate until a slight precipitate begins to appear, bring this again into solution by adding a few drops of dilute sulphuric acid, reduce the contained iron to the ferrous state by NaHSO_3 or gaseous SO_2 , dilute to 400 or 450 c.c., boil for two hours, replacing the evaporated water by an aqueous solution of SO_2 . The *titanic acid* is thus precipitated. Allow to cool, make up to 500 c.c., pour through a dry filter and wash the TiO_2 with warm water, containing a little ammonium chloride, but keep the washings separate from the first filtrate. Dry, ignite, and weigh the TiO_2 .

(c) Boil 125 c.c. of the first filtrate obtained in (b) (= 0.250 g. bauxite) till the SO_2 has been removed, add a little zinc, dilute strongly, and estimate the *iron* by titration with permanganate, after having rendered the solution slightly acid by sulphuric acid, as described p. 152.

(d) *Alumina, Ferric oxide, and Titanic acid* together are estimated in the first solution (a). Take 25 c.c. of this solution (= 0.125 g. bauxite), add a little fuming nitric and hydrochloric acid, dilute considerably, add NH_3 in slight excess, boil up for a moment, filter, dissolve the precipitate again in hydrochloric acid, precipitate again with NH_3 , wash, filter, dry, and weigh. By deducting the SiO_2 found in (a), the TiO_2 in (b), and the ferric oxide in (c), we obtain the remainder = *Alumina*.

(e) Ignite a fresh sample of dried bauxite for a quarter of an hour by means of the blow-pipe; the loss of weight is = chemically combined water + organic matter.

B.—Control of Working Conditions.

1. The *residue* from decomposing the bauxite is tested by boiling 2 g. with 3 c.c. concentrated sulphuric acid + 3 c.c. water until the red colour is destroyed, diluting a little, filtering, and making the filtrate up to 100 c.c. In this we estimate:

(a) *Iron* in 10 c.c. by reducing it to the ferrous state and titrating with KMnO_4 , p. 152.

(b) *Ferric oxide + Alumina* by precipitation with NH_3 .

(c) *Soluble soda* by boiling 20 c.c. with a solution of ammonium chloride and absorbing the NH_3 set free in titrated hydrochloric acid.

2. *Aluminate solution*.—In this we estimate Na_2O and Al_2O_3 in the same operation, as described below for sodium aluminate.

C.—Commercial Products.

1. *Sulphate of Alumina and Alum*:—

(a) *Estimation of Alumina*—(a) *Gravimetric estimation*, Dis-

solve 10 g. in water, dilute to $\frac{1}{2}$ litre, take 50 c.c. of the clear solution = 1 g. of the substance, add ammonia in slight excess, boil up for a moment, filter, wash, dry the precipitate, ignite, and weigh the Al_2O_3 . It is slightly contaminated with traces of iron, silicate, and phosphoric acid, which may be neglected.

(β) *Volumetric Analysis*.—Dissolve 5 g. in water, dilute to $\frac{1}{2}$ litre, take out 50 c.c. = 0.5 g. substance, neutralise the free acid by dilute solution of caustic soda (indicator: methyl orange, till the pink changes to yellow), then add phenolphthalein and titrate with standard caustic soda solution until the red colour appears. Each c.c. of the NaOH solution corresponds to 0.1704 g. Al_2O_3 .

N.B.—This method gives only approximate results, unless a number of precautions, detailed in *Tech. Meth.*, vol. i., are observed.

(b) *Iron* cannot be estimated either gravimetrically or by titration, on account of its small quantity. Hence it is estimated colorimetrically by Lunge and Kéler's method. We require for this a number of small stoppered cylinders of white glass, 13 mm. internal diameter, 17 cm. high, containing 25 c.c. divided in 0.1 c.c., and a free space of 5 c.c. above the 25 c.c. mark. Also the following reagents:—(1) a 10 per cent. solution of potassium thiocyanate; (2) pure ether; (3) a solution of 8.630 g. ammonium-iron-alum and 5 c.c. concentrated sulphuric acid in 1 litre; (4) a solution prepared from (3) by diluting it in the proportion of 1:100, so that this solution contains 10 mg. Fe per litre. It should be kept protected from sunlight, but even then keeps only for a few days, whereas solution (3), when protected from air and light, keeps a long time without getting turbid; (5) pure nitric acid. It is hardly possible to obtain nitric acid absolutely free from iron, but this does not matter, if it gives only a slight pink colour with potassium thiocyanate, since very little of it is used, and an equal quantity for the check test as for the actual test.

Dissolve 1 or 2 g. of the aluminium sulphate, weighed exactly, in a little water, add exactly 1 c.c. of the pure nitric acid (5), heat a few minutes, allow to cool, and dilute to 50 c.c. Put 5 c.c. of this solution into one of the colorimeter cylinders, A. (*N.B.*—If this method is applied to estimate traces of iron in sulphuric acid, this is diluted in the same way.) Into a second cylinder, B, put 5 c.c. of dilute nitric acid, obtained by diluting 1 c.c. of (5) to 50 c.c., and a certain, accurately measured quantity of the iron-alum solution (3), e.g., 1 c.c. Add as much pure water to cylinder A as you put iron solution in B, so as to always have the same degree of dilution in A and B. Then add to both A and B 5 c.c. of the thiocyanate solution (1) and 10 c.c. of the ether (2), put the stopper in and shake thoroughly, until the aqueous layer has become colourless and the red colour has passed over entirely into the ether. The comparison of the colours in A

and B is most accurate after a few hours, since they deepen a little on standing, but marked differences can be observed at once, so that three cylinders will suffice, of which A receives the solution to be tested, B and C the quantities of iron most nearly approaching to A. The comparison is made by holding the cylinders a little distance from a white surface (not putting them down upon it!) and looking at them from the top downwards. It is then quite easy to estimate differences of ± 0.1 c.c. of the iron-alum solution (5), that is of ± 0.001 mg. Fe in the 5 c.c. employed for analysis, but only when the total quantity of iron does not exceed 2 c.c. of the solution, that is = 0.02 mg. Fe. If there should be more than this present, the permanganate method, p. 113, is applicable.

(c) *Free acid* in aluminium sulphate cannot be directly titrated by any of the hitherto known indicators. Beilstein and Grosse proceed as follows:—Dissolve 1 or 2 g. of the sulphate in 5 c.c. water, add 5 c.c. of a cold saturated solution of ammonium sulphate, stir fifteen minutes, and precipitate with 50 c.c. 95 per cent. alcohol. Wash the precipitate with 50 c.c. alcohol, evaporate the alcohol from the mixed filtrate and washings on the water-bath, and titrate the acid in the residue by decinormal soda solution and phenolphthalein.

(d) *Zinc* only occurs occasionally in commercial sulphate of alumina, but is very injurious. Estimate it by adding to the solution of the sulphate a sufficient quantity of barium acetate to precipitate all the sulphuric acid, and precipitating the zinc in the filtrate as ZnS.

2. *Aluminate of Soda*:—

(a) *Soda and Alumina*.—Dissolve 2 g. in water, dilute to 100 c.c. and titrate 10 c.c. (= 0.2 g. substance) quite hot, with phenolphthalein as indicator, with fifth normal hydrochloric acid until the red colour has vanished. The soda only is saturated at this stage, and each c.c. of the acid corresponds to 0.00621 g. Na_2O . Now add a single drop of methyl orange and continue the titration with the same acid, but at a temperature of 30° , until the alumina first precipitated has been redissolved and the red colour has appeared. Each c.c. of acid used in this second titration corresponds to 0.003407 g. Al_2O_3 . The percentage is obtained directly when employing 0.200 g. substance by multiplying the c.c. used in the first titration (a) by 3.105 = per cent. Na_2O and those used in the second titration (b) by 1.704 = per cent. Al_2O_3 .

(b) *Insoluble matter* is estimated in 10 to 20 g. substance in the usual manner, but employing "hardened" filtering paper, since ordinary filter paper would not stand the strongly caustic solution.

(c) *Silica* is estimated by evaporating with hydrochloric acid, digesting the residue with dilute HCl, filtering, washing, igniting, and weighing the residue.

3. *Commercial Alumina* is either the hydrate or anhydrous,

In this the *silica* occurring as an impurity is estimated as in 2 (c); *total soda* by igniting at a red heat, digesting with water, heating with normal HCl, and titrating back the excess of acid; *soluble soda* by boiling with 100 c.c. water and titration with normal HCl and phenolphthalein; *iron* in the hydrochloric acid solution as in No. 1 (b); *loss of weight on ignition* ($=\text{H}_2\text{O} + \text{CO}_2$) by heating for fifteen minutes over the blow-pipe.

XVI. CEMENT INDUSTRY.

A.—Portland Cement.

1. Raw Materials.

(a) *Limestone*.—(a) Estimate *carbon dioxide*, as described, p. 156, by titration or by volumetric estimation of CO_2 , p. 169. It is calculated as CO_2 . In the presence of considerable quantities of magnesia (which is considered as an injurious constituent of cement), estimate it in the hydrochloric acid solution, as on p. 147, calculate it as MgCO_3 , and calculate the excess of CO_2 as CaCO_3 .

(β) *Argillaceous residue* is the difference between 100 and the carbonates found in (a). If there is much present, it may be examined like clay, No. (b).

(b) *Clay*.—The percentage of coarse sand (quartz) is found by elutriation. Weigh 50 g. of the *coarsely* ground, dried average sample into a rather large porcelain dish, pour over it 100 c.c. dilute hydrochloric acid (1 concentrated acid + 8 water), boil for about three hours, allow to cool, pour off the acid and direct a jet of water on to the mass, carefully rubbing it up with the fingers, so that only clay goes away with the water and pure sand remains behind. This plan is better than the application of mechanical elutriating apparatus.

The sand may be sorted by sieves into different sizes, viz., fine dust (down to 0.025 mm.), dust (0.040 mm.), fine sand (0.20 mm.), coarse sand (above this).

Complete analysis of clay (cf. *Tech. Meth.*, vol. i., p. 568, *et seq.*).

1. *Decomposition by means of alkaline carbonate, i.e.*, a mixture of equal parts potassium carbonate and sodium carbonate, of which 6 to 10 g. are required for one part of clay. Dry the clay at 120°, grind it very finely, mix it intimately with the alkaline carbonate in the platinum crucible itself by means of a platinum or glass spatula (which is afterwards cleaned with a little carbonate), and heat in the covered crucible, first slowly, then up to full, quiet fusion. A good Bunsen or Fletcher burner is preferable to the blow-pipe for the heating. After cooling heat the bottom of the crucible by a small flame to a low red heat twice succes-

sively, in order to facilitate the separation of the fused mass, allow to cool, pour in a few c.c. of water, and heat gently with a small flame, until the cake detaches itself from the crucible. Wash it into a good-sized platinum dish, cover this with a large watch-glass and heat on the water-bath until the mass has softened and fallen to powder. Then add an excess of hydrochloric acid, remove the watch-glass, wash its under-surface, and evaporate to dryness on the water-bath. During the evaporation the mass is stirred with a glass rod, so as to render the residue powdery. Then heat the dish in an air-bath to 120° for an hour, moisten it, after cooling, with moderately strong hydrochloric acid, allow to stand for an hour, heat up with water, pour the clear portion through a filter, and continue this treatment until the residue ceases to yield a colour with hydrochloric acid. Then transfer it to a filter, wash, dry, and ignite it first over a small flame, then to constancy of weight, and weigh it as *silica*. It may still contain some *titanic acid*. This is separated by evaporating with hydrofluoric acid and concentrated sulphuric acid on the water-bath as a residue which should be tested whether it yields the purple microcosmic salt bead of TiO_2 .

The filtrate from the titanic acid is divided in two halves. In one of these estimate *alumina + ferric oxide* by adding pure liquor ammoniæ (free from carbonate) in slight excess, boiling up for a moment, filtering, washing, and igniting. In the other half estimate the *iron* by reducing with zinc and titrating with permanganate, cf. p. 113.

In the filtrate from the precipitate of $Al_2O_3 + F_2O_3$, estimate *calcium* by precipitation with ammonium oxalate (p. 147), and in the filtrate from this *magnesium* by ammonium phosphate (p. 147).

2. *The Alkalies* can be estimated, if desired, by decomposing about 5 g. clay with hydrofluoric acid; cf. *Tech. Meth.*

3. *Sulphur*, present as sulphates or pyrites, is estimated by oxidation with aqua regia and precipitating the hydrochloric acid solution with barium chloride, cf. p. 110.

4. *Carbon dioxide*, as in the case of limestone, pp. 156 or 169.

5. *Loss of weight on ignition* over the blow-pipe or a powerful gas burner gives water + organic matter + CO_2 + sulphur present as pyrites, etc.

(c) *Separation of silica present as quartz, and that present in the form of silicates.*—The separation of these two kinds of silica is frequently demanded in so-called "rational analysis of clay." It can be effected by the process of Lunge and Millberg (*Z. angew. Chem.*, 1897, p. 393), on the basis of the observation that extremely finely divided *quartz* is dissolved by concentrated caustic soda solution, but not by a 5 per cent. solution of sodium carbonate, whilst the latter dissolves the silica, separated from *silicates* by strong acids in an *amorphous* state, when heated on the water-bath for half an hour. This is applied to the separation

of the two modifications of silica as follows. Heat 5 g. of clay (dried at 120°) with dilute sulphuric acid (50 c.c. concentrated acid + 100 c.c. water) to boiling in a porcelain or platinum dish, covered with a watch-glass, until the water has been driven off and fumes of SO_3 begin to escape, allow to cool, dilute with water, pour off the liquid, moisten the residue with hydrochloric acid, heat for a quarter of an hour, filter, and wash. Wash the moist residue, which contains a mixture of both modifications of SiO_2 , into a porcelain dish, make up the solution to about 250 c.c., add about 12.5 g. pure anhydrous sodium carbonate, and heat on the water-bath for half an hour. Then pour off the clear liquid and repeat the treatment with 5 per cent. solution of Na_2CO_3 three times. Finally, wash the insoluble matter on to a filter and wash it thoroughly with water containing a little alcohol. The dried and ignited residue consists of the SiO_2 present as quartz; the difference between this and the total SiO_2 found in (b) 1 is the SiO_2 present as silicates.

2. Control of the Working Conditions.

The *crude mixture* is tested for its percentage of clay and calcium carbonate like limestone; compare A, 1. Usually the estimation of CO_2 (pp. 156 or 169) is sufficient.

The *clinker* is analysed like the finished cement, if this is required.

3. Commercial Cement.

Ignite 1 g. cement in a platinum crucible over the blow-pipe for fifteen minutes, decompose with hydrochloric acid, filter from the insoluble matter, fuse this with sodium carbonate, dissolve the melt in water, and unite this solution with the filtrate previously obtained. In this solution the following estimations are made:—

(a) *Silica* is determined by boiling down the united solutions and filtering off the precipitated SiO_2 . The filtrate is again concentrated by boiling, and any SiO_2 that separates is united with the first portion. Dry the total (crude) silica, heat on the blow-pipe for half an hour, and weigh. Then heat with 10 c.c. hydrofluoric acid and four drops concentrated sulphuric acid till fumes cease to be given off, and deduct the residue from the crude SiO_2 ; the portion thus removed by volatilisation represents the real SiO_2 .

(b) Divide the united filtrates in two halves. In one of these estimate the *Sesquioxides*, $\text{Al}_2\text{O}_3 + \text{Fe}_2\text{O}_3$, by precipitation with pure liquor ammoniæ, as on p. 237.

(c) *Ferric oxide* is estimated in the second half of the filtrate from (a), by reducing to the ferrous state by means of zinc or H_2S and titrating with permanganate; cf. p. 113.

(d) *Calcium* is estimated in the filtrate obtained in (b) by precipitation with ammonium oxalate, p. 147.

(e) *Magnesium* in the filtrate from (d), by precipitation with ammonium phosphate, p. 147.

(f) *Sulphates* are determined in a special sample by dissolving 1 g. in hot hydrochloric acid, filtering, and precipitating with barium chloride, p. 110.

(g) *Total sulphur*.—Fuse 1 g. cement with sodium carbonate and a little potassium nitrate, dissolve in hot water, filter, acidify, and precipitate with barium chloride.

(h) The estimation of *alkalis* is rather troublesome, and is only carried out in exceptional cases; cf. *Tech. Meth.*, i.

(i) The *physical tests for fineness of grinding, time of setting, breaking strain*, etc., are described *ibid.*

B.—Hydraulic Lime and Roman Cement.

The raw material for these are *marls*. In these usually only CO₂ and argillaceous residue are estimated, as in the case of limestone, p. 236.

An accurate analysis can be made as described for clay, p. 236, more especially the separation of the silica present as quartz from that of the silicates.

C.—Puzziolanas, Trass, Granulated Blast-Furnace Slag.

1. *Hygroscopic water* is estimated by drying 10 g. at 110°.

2. *Chemically combined water*.—Ignite 1 g. of the substance dried in No. 1 in a platinum crucible by means of the blow-pipe, a Hempel gas-furnace, or other suitable means. The temperature ought to be raised gradually, so as to attain a red heat in about ten minutes, in order to avoid mechanical losses by dust being carried away through a sudden liberation of steam. After this continue the heating for half an hour to a yellow heat, and then transfer at once to the desiccator. The loss of weight is an important criterion for the hydraulicity.

3. *Silica present as silicates* should be estimated as well as that of quartz as an important hydraulic factor, as described p. 237.

4. *Mechanical tests* for fineness of grinding, etc., as for cement.

XVII. PREPARATION OF STANDARD SOLUTIONS.

Introduction.

The analytical methods given in the foregoing pages are based upon the metric system of weights and measures. As there are still some laboratories in which the English system is used, the following remarks on the relation of the metric to the English system may prove useful.

The unit of weight of the English system is the grain. All normal solutions are prepared so that 1000 grains by volume (100 decems) contain one equivalent of the reagent in grains, and consequently all normal solutions prepared on the English system are identical in concentration with those prepared on the metric system.

English burettes usually hold 1000 grains, and are divided into 100 parts of 10 grains each, called one decem. The decem corresponds to the cubic centimetre. As, however, this unit, the decem, is ten times the unit of weight, the following rules must be observed when any of the data are to be changed from the metric to the English system :—

- Instead of Litre read 10,000 grains.
 „ Cubic centimetre read decem, or 10 times the number of grains.
 „ Grams read 10 times the number of grains.

If, for instance, we are told to prepare a standard solution of permanganate by dissolving 15·820 g. of potassium permanganate in 1 litre of water, and that 1 c.c. of such a solution corresponds to 0·028 g. of iron, we shall obtain a solution of equal strength by dissolving 158·20 grains in 10,000 grains of water, and 1 decem of this solution will correspond to 0·28 grains of metallic iron. No errors can possibly occur if the reader will always substitute ten times as many grains for any number of grams, ten times as many grains, or an equal number of decems for any number of cubic centimetres, and 10,000 grains for every litre. Where we are directed to measure out by means of a pipette 50 c.c., we take 500 grains instead, etc., but when speaking of the number of cubic centimetres on the burette, we substitute exactly the same number of decems.

It will also be useful to remember that :

Grams per litre	= grains per 1000 grains.
„ „	= ounces per 1000 ounces.
„ „	= ounces per cubic foot (approximately).
Grams per litre ÷ 16	= lbs. per cubic foot.
Grams per litre × 70	= grains per 70,000 grains.
„ „ „	= grains per gallon.
0·4375 × grams per cub. metre	= grains per cubic foot.
Kilograms per cubic metre	= lbs. per 1000 lbs.
„ „ „	= lbs. per 16 cubic feet.
<u>Kilograms per cubic metre</u> 16	= lbs. per cubic foot.
16 × cub. metres per kilogram	= cubic feet per lb.
Kilograms per square metre	= 0·205 lb. per square foot.
Kilograms per sq. metre × 4·89	= lbs. per square foot.

A.—Normal Acid and Alkali.

As basis of Alkalimetry and Acidimetry, we employ *chemically pure sodium carbonate*. This is tested for purity by dissolving 5 g. in water, which ought to yield a perfectly clear, colourless solution; if, after acidifying this solution with nitric acid, no opalescence is caused by barium chloride, or silver nitrate, the salt may be taken as sufficiently pure. Before using it, the sodium carbonate must be heated in a platinum crucible, which is half-filled with it and is placed on a sand-bath, the sand reaching to the same level outside as the carbonate inside. A thermometer is put in, which at the same time serves as a stirrer. The temperature is raised to 270° to 300° for about half an hour; the contents are then emptied hot into a stoppered weighing-bottle, which is kept in a desiccator up to the time of weighing. Then weigh off, for normal acid, four portions of about 2 g. each into the beakers in which the titration is to take place; for one-fifth normal acid the single portions ought not to exceed 0·4 g. The balance ought to turn to at least 0·5 mg.

As normal acid we prefer *hydrochloric acid*, which has the following advantages over sulphuric and oxalic acid, viz. :—1st, It is more generally applicable, *e.g.*, for alkaline earths; 2nd, its strength, after being fixed by pure sodium carbonate, can be most accurately checked by silver nitrate, far more accurately than that of sulphuric acid by barium chloride; 3rd, it does not change on keeping, like oxalic acid.

Normal HCl (36·46 g. HCl per litre) is prepared as follows:—Dilute pure hydrochloric acid to 1·020 specific gravity (4° Tw.). Such an acid will be rather too strong. Fill a burette with this acid, and titrate with it one of the weighed samples of sodium carbonate, the weight of which is w grams. Suppose that x c.c. of this acid are required. As the acid is sure to be too strong, x will always be smaller than $\frac{w}{0\cdot05305}$, and we shall have to add to every x c.c. of the acid $\frac{w}{0\cdot05305} x$ c.c. of water, and if the total quantity of acid of specific gravity 1·020 amounts to V c.c., the amount of water to be added thereto to render it correct will be n c.c., where $n = V \left(\frac{w}{0\cdot05305 x} - 1 \right)$. For one-fifth normal acid the above factor would be $= \frac{w}{0\cdot01061}$.

If accurate normal alkali is at hand, it may be similarly employed, for examining the provisional acid, and then adjusting it to the normal strength.

In any case, the mixed normal acid must be checked by titrating new samples of sodium carbonate, when x ought to be $= \frac{w}{0\cdot05305}$

A further check is afforded by estimating the chlorine gravimetrically by silver nitrate; 10 c.c. (= 0.3646 HCl) ought to yield 1.4338 g. AgCl.

The ordinary *indicator* in alkalimetry and acidimetry used to be tincture of litmus, which must be kept in open vessels, to avoid its being spoiled. When employing litmus, the liquid to be tested must be kept boiling for some time, in order to expel all CO_2 , and normal acid must be added as long as, on further boiling, the colour changes back from red to purple, or blue. This prolonged boiling causes some alkali to be dissolved from most kinds of glass, which makes the tests inaccurate. A test with litmus rarely lasts less than half an hour, usually more. Phenolphthalein has exactly the same drawbacks. Even the action of the carbon dioxide contained in the air, which comes into contact with the liquid on cooling, may cause trouble in very accurate work. On the other hand, a test is finished in a few minutes, if litmus is replaced by a very dilute solution of *methyl orange* (dimethylaminoazobenzene sulphonic acid), but in this case the liquids must not be hot, but at the ordinary temperature, and only mineral acids, not oxalic acid may be employed. The cold solution of sodium carbonate is coloured just perceptibly yellow by adding a drop or two of the solution of methyl orange, preferably by means of a pipette; if the colour is too intense, it will cause the transition into red on neutralisation to be less sharp. CO_2 does not act in the least upon methyl orange; a change of colour only takes place when all Na_2CO_3 has been decomposed. When the Na_2CO_3 has been exactly converted into NaCl, the colour turns from yellow to *brownish*, which is due to the action of free CO_2 on the indicator. At this point the reading is made, preferably by means of a Goeckel screen. Just *one* drop of acid is then added, when the colour ought now to become distinctly *pink*. If it remains brownish, another drop of acid is added, and so forth. Exactly the same course is followed in titrating acids with caustic soda solution; in this case also the reading is taken at the brownish transition colour, before the change to yellow has taken place. The results obtained in this way are identical with those obtained by the *proper* application of litmus or phenolphthalein, that is, working with these indicators under complete exclusion of air, with prolonged boiling, and in porcelain or silver vessels. The great advantage of methyl orange over the last-named indicators is the saving of time, the working at ordinary temperatures, and the possibility of employing glass vessels without any danger of error caused by the use of this material.

Another advantage of methyl orange is that it is not affected by *sulphuretted hydrogen* (which destroys litmus); hence it can be employed, *e.g.*, for the direct titration of black-ash liquors. *Sulphur dioxide* acts upon it like the stronger mineral acids, but only to the extent of one-half of its equivalent; that is, the point

of neutrality is reached when the compound NaHSO_3 has been formed. In the presence of *nitrous acid* methyl orange is gradually destroyed, but it is quite easy to employ it even in this case by proceeding as described on p. 135.

The above description of the transition from yellow through brownish to pink applies only to more accurate work, *e.g.*, when employing fifth normal acid and alkali. With normal or semi-normal liquids this intermediate colour is hardly observed, the change passing directly from yellow to pink, and *vice versa*.

It is generally agreed that methyl orange is the best indicator for titrating *bases* by means of strong mineral acids, and this holds good also for the titration of the *strong acids*—sulphuric, hydrochloric, and nitric acid. In these cases, indeed, its advantage over litmus or phenolphthalein is even more marked, because a slight percentage of CO_2 in the standard alkali employed has no effect. But *organic acids* cannot be titrated with methyl orange.

Some authors have recommended, in lieu of methyl orange, the unsulphonated compound, dimethylaminoazobenzene, but this is only soluble in alcohol, and cannot be recommended. This is also the case with ethyl orange.

To prepare *standard alkali*, dissolve about 50 g. of the best commercial caustic soda in 1 litre of pure water and titrate 50 c.c. of this solution with standard acid. More than 50 c.c. of acid will be required; we call this x c.c. The fraction $\frac{50000}{x}$ shows the number of c.c. of the first solution, which must be diluted with pure water to 1 litre in order to obtain a really normal alkali. The solution thus prepared is again checked by titration with normal acid.

The normal alkali, when intended to be used with litmus, should be as free as possible from carbonate, and should be protected against absorption of CO_2 from the air, because otherwise the change of colour does not take place sufficiently rapidly, and markedly in cold solutions. A solution of sodium hydroxide *entirely* free from carbonate is difficult to prepare and to preserve when in constant use. When employing methyl orange as an indicator, an ordinary caustic soda solution may be employed without any special precautions. The caustic soda employed should not contain more than a very small proportion of alumina; ordinary strong caustic nearly always fulfils this condition, or it may even be replaced by a solution of 53.05 g. pure sodium carbonate in 1 litre water, which is employed cold, and which yields as accurate results as NaOH , no notice being taken of the CO_2 which escapes with effervescence. The general use of this solution is, however, inconvenient on account of the efflorescence on the burettes, necks of bottles, etc. Weaker (*e.g.*, fifth normal, or even seminormal) solutions have not this drawback.

All standard solutions must be prepared and employed as

nearly as possible at a certain *temperature*. Mohr prescribes 15°; some prefer 18° C., as being more suitable for laboratories. When the solutions have stood for some time in bottles, a little water is evaporated and recondensed in the upper part of the bottles; the contents must then be properly mixed by shaking.

If the temperature of the laboratory differs more than 2° or 3° from that employed for preparing the standard solutions, a correction should be made by means of the following table. In order to reduce the volumes read off at t° to 15°, deduct per 100 c.c. the following amounts:—

t° .	c.c.	t° .	c.c.
15	0	23	0·135
16	0·013	24	0·156
17	0·027	25	0·179
18	0·043	26	0·202
19	0·059	27	0·227
20	0·076	28	0·252
21	0·095	29	0·278
22	0·114	30	0·305

B.—Potassium Permanganate.

The ordinary solution is seminormal, *i.e.*, it yields 0·004 g. oxygen per c.c. It serves, *e.g.*, for estimating nitrous acid in vitriol, for testing the nitrogen acids in the chamber exits, for testing manganese ore, for testing Weldon mud, etc.

Since iron only occurs in very small quantity in the products of alkali manufacture, it is best estimated by means of a tenth or twentieth normal solution made from the seminormal solution by dilution, and corresponding to 0·00559 or 0·002795 g. Fe per c.c. respectively.

The solution is made by dissolving pure crystallised potassium permanganate, and is then quite stable, if protected from dust and direct sunlight. With perfectly pure KMnO_4 , and with absolutely pure water, it would be necessary to dissolve 15·815 g. per litre. Since, however, there is no certainty of the absolute purity either of the salt or of the distilled water, we dissolve 16 g. of well-crystallised permanganate in 1 litre of distilled water, and allow to stand for a week before standardising it, so that the KMnO_4 may complete its action upon the impurities contained in the water. Only then is the titre of the solution checked as below, and eventually brought to exactly seminormal by adding a little water. Prepared in this manner, and protected against dust and direct sunlight, the solution keeps for any length of time.

None of the methods formerly employed for standardising permanganate (by means of metallic iron, or oxalic acid, or hydrogen peroxide, etc.), is entirely free from objections (*cf. Tech. Meth.*, vol. i.). No such objection exists to the employment of Kahlbaum's *pure sodium oxalate*, first proposed by Sørensen.

This salt need only be kept for a few hours in a drying oven at 100° , and then allowed to cool in a desiccator over calcium chloride. Dissolve about 1.3 g. of this (exactly weighed) in about 200 c.c. water, heated to 60° to 70° , add dilute sulphuric acid, and run in the permanganate solution from a burette, first quickly, then drop by drop, until a permanent red colour is produced. If a be the weight of sodium oxalate, b the c.c. of permanganate solution used, the fraction $\frac{29.828 a}{b}$ gives the quantity of oxygen given off per c.c. of the permanganate solution.

If a brown precipitate (of MnO_2) should be formed during the titration, the experiment must be rejected, but this occurs only when the solutions are too concentrated or too hot (*i.e.*, above 70°).

Permanganate is best employed in a burette with a lateral hollow glass-tap. Any change in its titre (due to dust, etc.) is perceptible by a deposition of MnO_2 in the bottle. It is advisable to check the solution once every three months.

Permanganate can be used with perfect accuracy in the presence of free hydrochloric acid, if the solutions contain a considerable quantity of manganese salts; in other cases the same effect is produced by adding, say 1 g. of manganese sulphate free from iron.

C.—Iodine Solution.

Weigh exactly 12.697 g. of pure resublimed iodine (either bought as such or prepared by grinding up commercial iodine with 10 per cent. of potassium iodide and resubliming) on a balance turning at least with 5 mg.; put it into a litre flask containing a concentrated solution of 15 to 18 g. KI, close the flask, agitate till the iodine is completely dissolved, and fill up to the mark. This decinormal solution is checked by the arsenite solution (No. 4). Both solutions ought to be precisely equivalent, c.c. per c.c.

For estimating very small quantities of sodium sulphide a special iodine solution is sometimes made, by dissolving 3.249 g. of pure iodine with 5 g. of potassium iodide in a litre, to correspond to 0.001 g. Na_2S per c.c.

Solutions of iodine, especially the more dilute ones, keep a long time in well-stoppered bottles in a cool place, but they ought to be checked once a month by the arsenite solution.

Preparation of the starch solution.—Grind up 3 g. potato starch with a little water to a homogeneous paste; introduce this gradually into 300 g. of boiling water, contained in a porcelain dish, and continue the boiling till an almost clear liquid has been produced. Allow this to settle in a tall beaker, pour the clear portion through a filter, and saturate it with common salt. This solution, when kept in a cool place, is stable for some time; as soon as fungoid growths are noticed in it, it is thrown away.

A very convenient form of soluble starch is that made by

Zulkowsky's method, by heating 100 parts of concentrated glycerine with 6 parts of starch to 190° C. for about an hour, pouring into water and precipitating the soluble starch with alcohol and filtering. This is kept in the state of a thick paste, not to be allowed to dry, and a small quantity is taken out for each test by means of a glass rod. There are also other forms of soluble starch, *e.g.*, "ozone-starch."

D.—Sodium Arsenite Solution.

This serves for standardising the iodine solution, and as its volumetrical complement, especially in testing bleaching powder. Employ commercial pure powdered arsenious acid; test its purity by subliming a little from a small dish into a watch-glass, when no yellow sublimate of As_2S_3 (which volatilises more easily than As_2O_3) should result initially; on heating more strongly it should leave no residue. Before use the powdered As_2O_3 is kept for some time over sulphuric acid in a desiccator, and can then be weighed out without any special precautions, since it is not hygroscopic. For preparing a decinormal solution, weigh out exactly 4.950 g. As_2O_3 , boil it with 10 g. of pure sodium bicarbonate and 200 g. water till completely dissolved; add another 10 g. bicarbonate, and dilute on cooling to 1000 c.c. This solution is quite stable, and equivalent to 0.003545 g. chlorine or 0.012697 g. iodine per c.c.

If really pure and dry arsenious acid has been employed, the above solution will be correct at once. But when preparing large quantities, it ought to be checked by grinding up 0.5 g. iodine with 0.1 g. potassium iodide, heating this mixture in a small dish on a sand-bath or upon an asbestos board till abundant vapours arise, covering with a dry watch-glass, allowing the major portion, but not the whole, of the iodine to sublime into the watch-glass, covering this with a second watch-glass which fits air-tight upon the former, and has been weighed with it, and weighing. Slip the watch-glasses into a solution of 1 g. of potassium iodide (free from iodate), in 10 g. water, wait a little till the iodine is dissolved, dilute with 100 c.c. water, and titrate with the arsenite solution. When the colour is only a light yellow, add a little starch solution, and titrate exactly till the blue colour has just vanished. The c.c. of arsenite solution used, multiplied by 0.012697, ought to correspond exactly with the weight of iodine taken. Or the dry, sublimed iodine is transferred directly from the upper watch-glass into a tared stoppered weighing-bottle, weighed, and dissolved in KI solution in the same bottle.

E.—Silver Solution.

Weigh out exactly 16.994 g. of pure crystallised silver nitrate, preferably kept in a desiccator for a few hours, and dissolve in 1 litre. This gives a decinormal solution, corresponding per c.c. to

0.003545 g. Cl., or 0.003646 g. HCl., or 0.00585 g. NaCl. By dissolving 2.905 g. AgNO₃ in 1 litre, a solution is obtained corresponding to 0.001 g. NaCl per c.c.

Ammoniacal silver solution, for Lestelle's estimation of alkaline sulphides, is obtained by dissolving 13.810 g. of pure silver in pure nitric acid, adding 250 c.c. liquor ammoniæ, and diluting to 1 litre. Each c.c. of this corresponds to 0.005 g. Na₂S.

F.—Copper Solution.

Copper solution, for testing ferrocyanide, is obtained by dissolving 12.488 g. pure crystallised, not effloresced, cupric sulphate, in 1 litre water. (Cf. p. 168.)

G.—Oxalic Acid Solution.

Oxalic acid solution is employed for testing the "base" of Weldon mud, and caustic soda or lime in the presence of carbonate (pp. 155 and 156). Dissolve 63.03 g. pure, not effloresced, crystallised oxalic acid in 1 litre water, and check with normal alkali. This solution is not quite stable, especially when exposed to daylight; nor can it be employed for alkalimetry, when using methyl orange as an indicator.

XVIII. RULES FOR SAMPLING.

A.—Fuel.*

Take a shovelful of each wheelbarrow, basket, etc., throw it into a cask or tub closed by a lid, coarsely grind up the whole without delay, mix the contents, spread them out in a flat, square heap, divide this diagonally into four quadrants, remove two opposite quadrants, grind up the other two more finely and mix them again and continue in this manner until the weight has been reduced to about $\frac{1}{4}$ cwt. Put this into a tin box which is soldered up and sent to the testing-laboratory. There this sample is ground again, mixed up, and divided into twelve or sixteen portions in the manner of a chess-board. Take out a teaspoonful from each of these portions and grind them in a porcelain mortar to a powder as fine as dust. This powder is kept in a stoppered bottle, and is well mixed up before taking out a fresh sample for testing.

For separate *moisture tests*, a number of samples are taken during the first sampling, and kept in air-tight vessels.

B.—Ores and Minerals (Pyrites, Manganese, Salt, etc.).

(a) *Smalls, slack, salt, or other substances not requiring to be crushed.*—Take a sample of about 1 lb. of each weighing-tub, cart,

* According to the rules laid down for the German Official tests of steam-boilers and steam-engines.

or the like, by means of a scoop, so as to obtain about the same quantity each time. Of railway trucks, which are tipped directly into the warehouse, take three samples, one from the middle and one from each end.* All these single samples are put in a cask and kept covered, to prevent the evaporation of moisture. When the large sample is taken, empty the contents of the cask on a level, clean, and hard place, spread it flat, heap it up in a cone at the centre by going regularly round with a spade; spread this heap again flat, and take a sample of about a quarter of the mass, by taking out with a spade two strips crossing each other at right angles, and adding a little from the centre of each remaining quadrant. Treat this reduced sample exactly like the larger one, so that a third sample of about 5 lbs. is obtained. Mix this again thoroughly, and fill it into four (or more) wide-necked bottles of 4 ounces capacity, placed close together on a sheet of paper, so that a portion of each handful gets into each of the four bottles. When these are full, they are at once closed with tight-fitting corks; these are cut off straight above the necks of the bottles and well covered with sealing wax, putting on the seals of both buyer and seller, or any other party concerned. The mixing and filling must be done as quickly as possible, in order to prevent the evaporation, or the absorption of appreciable quantities of moisture during the operation.

The above sample bottles are handed over to the laboratory chemist, who has to pulverise their contents till they pass *completely* through a sieve with holes 1 mm. ($=\frac{1}{2}$ in.) wide; no coarse material must be left behind. From this, after thorough mixing, a smaller sample is taken and reduced to the degree of division necessary for analysis, by grinding in a steel or agate mortar, in the case of softer substances in a porcelain mortar. Manganese samples should not be treated in iron mortars. Moisture is estimated in an unground portion of the sample.

(b) *Ores in pieces requiring to be crushed.*—Large-sized samples must be taken if the lumps of the ore are very coarse. If the pieces are not above the size of an apple, and not too unequal, it is sufficient to take a sample from each tub, etc., as in (a), but with a shovel or scoop holding about 10 lbs. In the case of larger lumps, and of very unequal sizes, it is preferable to tip each tenth or twentieth tub or cart into a separate place, where the whole average sample is collected. In any case, the proportion between the large and small must be represented as accurately as possible in the average sample. This is then crushed to the size of a walnut, either by hand or by machinery, leaving no larger lumps behind. The crushed material is thoroughly mixed by turning it over with a spade several times;

* At some factories very unsatisfactory results have been obtained with this mode of sampling; they prefer that described later on (in b), of taking a certain number of entire tubs, barrows, or carts as sample.

it is then spread out in a flat heap and a smaller sample of about $\frac{1}{4}$ cwt. is taken, by lifting out two strips crossing each other at right angles, adding something from the centre of each remaining quadrant. The reduced sample is crushed further, either in a large metal mortar, or preferably with a sledge-hammer on a flanged cast-iron plate about 3 ft. square, bedded on a solid foundation; the latter process is much more convenient and cleanly than grinding in a mortar. The coarse portions are sifted out by a riddle of $\frac{1}{8}$ -in. holes and crushed again, till all has passed through. The product is reduced as in (a), by mixing, etc., to a quantity of 2 or 4 lbs., from which the sample bottles are filled as described above.

C.—Chemicals.

Saltcake, soda-ash, etc., if in bulk, are sampled as in No. 1, (a). If packed in casks, each third, fifth, or tenth cask, according to the size of the parcel, is bored at one of its bottoms and sampled by means of an *auger* (Fig. 19), which is inserted up to the centre of



FIG. 19.

the cask, turning it round its axis all the while. The single cask samples are put into a large wide-mouthed bottle, as drawn, till the sampling is over. Then empty the whole on to a large sheet of paper, mix thoroughly, crush any lumps with a spatula, and fill the 4-ounce bottles, previously prepared, exactly as described in No. 1 as for ores, observing the same rules for corking and sealing.

Bleaching powder, potash, and any other substances which are liable to be quickly spoilt in contact with the air by attracting moisture, or from other reasons, are treated like the foregoing substances, but operating with the greatest possible speed, and keeping the large bottle for collecting the cask samples well closed. The sampling is still more safely performed by taking away the upper end of the cask, removing the top layer to a depth of about 2 inches, taking a handful of the material from the interior as far as it is possible to reach in, which should be nearly at the centre of the cask, and placing it in the large bottles. In this way there is the least contact with air. Or else a sample-auger is employed, like that shown in Fig. 20, p. 250. It is made of a piece of gas-pipe of $1\frac{1}{2}$ -inch bore, cut open for part of its length, so that a longitudinal slot of 1 inch width, *a*, is formed. One side of this slot is sharpened, as well as the tip *b*, which is driven into the bleaching powder, etc. The upper part of the pipe is left uncut, and is provided with a handle, *c*. Before introducing the auger the cask is well shaken up; then it is placed in an upright

position and the auger is driven in as deeply as possible, in case of need by the aid of a hammer. This is done either after opening the cask, or by boring a hole in the end which is afterwards closed by a piece of tin, with paper underneath. After driving in the auger, it is turned several times round its axis so that it cuts through the bleaching powder with its sharp side and is thus filled up with it. The sample drawn out is put on paper, and is crushed on this as quickly as possible, preferably by means of a small hand-roller, it is then mixed and spread out flat. Small samples are finally taken from various parts by means of a spatula, as quickly as possible, and are put into bottles which are tightly closed and kept in a dark place. Bleaching powder samples should be always tested with as little delay as possible.



FIG. 20.

Caustic soda.—Since the samples attract moisture and carbonic acid on their surface, even in well-closed bottles, the outer opaque crust must be removed by scraping before weighing out the samples (*cf.* p. 191). It should be borne in mind that the centre of the drum is of weaker strength than the remainder, because the foreign salts accumulate in the portion which remains liquid the longest. The average strength is best represented by the portions next to the bottom and sides of the drum, which solidify quickest. This is most conveniently done while the contents are still in the liquid state. For the control of the manufacture itself it is best to take samples out of every pot during the time its contents are ladled out, from the top, the centre, and the bottom. These are poured out on to a metal plate, where they quickly solidify. The centre sample is the most important one for judging of the quality of each pot.

Solid sulphuric anhydride cannot be sampled directly for analysis. An auger cannot be employed, as the mass is too firm and tough; melting the mass in the drums themselves is out of the question, on account of the clouds of fumes. The following process is, therefore, employed:—A large sample of the solid anhydride is mixed with so much exactly analysed "monohydrated" sulphuric acid that an acid of about 70 per cent. is formed, which is liquid at ordinary temperatures. This mixture is made in a stoppered bottle, and is gently heated to 30° or 40° C., the stopper being loosely put in, till the solution is complete, and a small sample then taken out by means of Lunge and Rey's glass-tap pipette (p. 144).

COMPARISON OF HYDROMETER DEGREES 251

XIX. COMPARISON OF THE HYDROMETER DEGREES ACCORDING TO BAUMÉ AND TWADDELL, WITH THE SPECIFIC GRAVITIES.

B.	T.	Spec. Gravity.	B.	T.	Spec. Gravity.	B.	T.	Spec. Gravity.
0	0	1.000	15.4	24	1.120	29.3	51	1.255
0.7	1	1.005	16.0	25	1.125	29.7	52	1.260
1.0	1.4	1.007	16.5	26	1.130	30.0	52.6	1.263
1.4	2	1.010	17.0	26.8	1.134	30.2	53	1.265
2.0	2.8	1.014	17.1	27	1.135	30.6	54	1.270
2.1	3	1.015	17.7	28	1.140	31.0	54.8	1.274
2.7	4	1.020	18.0	28.4	1.142	31.1	55	1.275
3.0	4.4	1.022	18.3	29	1.145	31.5	56	1.280
3.4	5	1.025	18.8	30	1.150	32.0	57	1.285
4.0	5.8	1.029	19.0	30.4	1.152	32.4	58	1.290
4.1	6	1.030	19.3	31	1.155	32.8	59	1.295
4.7	7	1.035	19.8	32	1.160	33.0	59.4	1.297
5.0	7.4	1.037	20.0	32.4	1.162	33.3	60	1.300
5.4	8	1.040	20.3	33	1.165	33.7	61	1.305
6.0	9	1.045	20.9	34	1.170	34.0	61.6	1.308
6.7	10	1.050	21.0	34.2	1.171	34.2	62	1.310
7.0	10.2	1.052	21.4	35	1.175	34.6	63	1.315
7.4	11	1.055	22.0	36	1.180	35.0	64	1.320
8.0	12	1.060	22.5	37	1.185	35.4	65	1.325
8.7	13	1.065	23.0	38	1.190	35.8	66	1.330
9.0	13.4	1.067	23.5	39	1.195	36.0	66.4	1.332
9.4	14	1.070	24.0	40	1.200	36.2	67	1.335
10.0	15	1.075	24.5	41	1.205	36.6	68	1.340
10.6	16	1.080	25.0	42	1.210	37.0	69	1.345
11.0	16.6	1.083	25.5	43	1.215	37.4	70	1.350
11.2	17	1.085	26.0	44	1.220	37.8	71	1.355
11.9	18	1.090	26.4	45	1.225	38.0	71.4	1.357
12.0	18.2	1.091	26.9	46	1.230	38.2	72	1.360
12.4	19	1.095	27.0	46.2	1.231	38.6	73	1.365
13.0	20	1.100	27.4	47	1.235	39.0	74	1.370
13.6	21	1.105	27.9	48	1.240	39.4	75	1.375
14.0	21.6	1.108	28.0	48.2	1.241	39.8	76	1.380
14.2	22	1.110	28.4	49	1.245	40.0	76.6	1.383
14.9	23	1.115	28.8	50	1.250	40.1	77	1.385
15.0	23.2	1.116	29.0	50.4	1.252	40.5	78	1.390

N.B.—The Baumé degrees are calculated by the formula $d = \frac{144.8}{144.8 - n}$, water of 15° C. being put = 0° and sulphuric acid of 1.842 at 15° C. = 66°; compare *Lunge's Sulphuric Acid and Alkali*, vol. 1., p. 20. This is the Baumé's hydrometer, mostly used on the Continent of Europe, but other scales are in use there as well, and quite another scale for Baumé's hydrometer is used in America.

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COMPARISON OF THE HYDROMETER DEGREES ACCORDING TO BAUMÉ AND TWADDLELL, WITH THE SPECIFIC GRAVITIES—*Continued.*

B.	T.	Spec. Gravity.	B.	T.	Spec. Gravity.	B.	T.	Spec. Gravity.
40·8	79	1·395	50·9	109	1·545	59·5	140	1·700
41·0	79·4	1·397	51·0	109·2	1·546	59·7	141	1·705
41·2	80	1·400	51·2	110	1·550	60·0	142	1·710
41·6	81	1·405	51·5	111	1·555	60·2	143	1·715
42·0	82	1·410	51·8	112	1·560	60·4	144	1·720
42·3	83	1·415	52·0	112·6	1·563	60·6	145	1·725
42·7	84	1·420	52·1	113	1·565	60·9	146	1·730
43·0	84·8	1·424	52·4	114	1·570	61·0	146·4	1·732
43·1	85	1·425	52·7	115	1·575	61·1	147	1·735
43·4	86	1·430	53·0	116	1·580	61·4	148	1·740
43·8	87	1·435	53·3	117	1·585	61·6	149	1·745
44·0	87·6	1·438	53·6	118	1·590	61·8	150	1·750
44·1	88	1·440	53·9	119	1·595	62·0	150·6	1·753
44·4	89	1·445	54·0	119·4	1·597	62·1	151	1·755
44·8	90	1·450	54·1	120	1·600	62·3	152	1·760
45·0	90·6	1·453	54·4	121	1·605	62·5	153	1·765
45·1	91	1·455	54·7	122	1·610	62·8	154	1·770
45·4	92	1·460	55·0	123	1·615	63·0	155	1·775
45·8	93	1·465	55·2	124	1·620	63·2	156	1·780
46·0	93·6	1·468	55·5	125	1·625	63·5	157	1·785
46·1	94	1·470	55·8	126	1·630	63·7	158	1·790
46·4	95	1·475	56·0	127	1·635	64·0	159	1·795
46·8	96	1·480	56·3	128	1·640	64·2	160	1·800
47·0	96·6	1·483	56·6	129	1·645	64·4	161	1·805
47·1	97	1·485	56·9	130	1·650	64·6	162	1·810
47·4	98	1·490	57·0	130·4	1·652	64·8	163	1·815
47·8	99	1·495	57·1	131	1·655	65·0	164	1·820
48·0	99·6	1·498	57·4	132	1·660	65·2	165	1·825
48·1	100	1·500	57·7	133	1·665	65·5	166	1·830
48·4	101	1·505	57·9	134	1·670	65·7	167	1·835
48·7	102	1·510	58·0	134·2	1·671	65·9	168	1·840
49·0	103	1·515	58·2	135	1·675	66·0	168·4	1·842
49·4	104	1·520	58·4	136	1·680	66·1	169	1·845
49·7	105	1·525	58·7	137	1·685	66·3	170	1·850
50·0	106	1·530	58·9	138	1·690	66·5	171	1·855
50·3	107	1·535	59·0	138·2	1·691	66·7	172	1·860
50·6	108	1·540	59·2	139	1·695	67·0	173	1·865

XX. VALUE OF ALKALI PER TON.

Price per unit.	1 per cent.			2 per cent.			3 per cent.			4 per cent.			5 per cent.		
Pence.	£	s.	d.	£	s.	d.	£	s.	d.	£	s.	d.	£	s.	d.
$\frac{3}{4}$	0	1	3	0	2	6	0	3	9	0	5	0	0	6	3
$1\frac{1}{8}$	0	1	$4\frac{1}{2}$	0	2	$8\frac{1}{2}$	0	4	$0\frac{3}{4}$	0	5	5	0	6	$9\frac{1}{2}$
$\frac{7}{8}$	0	1	$5\frac{1}{2}$	0	2	11	0	4	$4\frac{1}{2}$	0	5	10	0	7	$8\frac{1}{2}$
$1\frac{3}{8}$	0	1	$6\frac{3}{4}$	0	3	$1\frac{1}{2}$	0	4	$8\frac{1}{4}$	0	6	3	0	7	$9\frac{3}{4}$
1	0	1	8	0	3	4	0	5	0	0	6	8	0	8	4
$1\frac{1}{16}$	0	1	$9\frac{1}{2}$	0	3	$6\frac{1}{2}$	0	5	$3\frac{3}{4}$	0	7	1	0	8	$10\frac{1}{2}$
$1\frac{1}{8}$	0	1	$10\frac{1}{2}$	0	3	9	0	5	$7\frac{1}{2}$	0	7	6	0	9	$4\frac{1}{2}$
$1\frac{1}{16}$	0	1	$11\frac{1}{4}$	0	3	$11\frac{1}{2}$	0	5	$11\frac{1}{4}$	0	7	11	0	9	$10\frac{3}{4}$
$1\frac{1}{4}$	0	2	1	0	4	2	0	6	3	0	8	4	0	10	5
$1\frac{5}{16}$	0	2	$2\frac{1}{4}$	0	4	$4\frac{1}{2}$	0	6	$6\frac{3}{4}$	0	8	9	0	10	$11\frac{1}{4}$
$1\frac{3}{8}$	0	2	$3\frac{1}{2}$	0	4	7	0	6	$10\frac{1}{2}$	0	9	2	0	11	$5\frac{1}{2}$
$1\frac{7}{16}$	0	2	$4\frac{3}{4}$	0	4	$9\frac{1}{2}$	0	7	$2\frac{1}{4}$	0	9	7	0	11	$11\frac{3}{4}$
$1\frac{1}{2}$	0	2	6	0	5	0	0	7	6	0	10	0	0	12	6
$1\frac{9}{16}$	0	2	$7\frac{1}{4}$	0	5	$2\frac{1}{2}$	0	7	$9\frac{3}{4}$	0	10	5	0	13	$0\frac{1}{2}$
$1\frac{5}{8}$	0	2	$8\frac{1}{2}$	0	5	5	0	8	$1\frac{1}{2}$	0	10	10	0	13	$6\frac{1}{2}$
$1\frac{1}{8}$	0	2	$9\frac{3}{4}$	0	5	$7\frac{1}{2}$	0	8	$5\frac{1}{2}$	0	11	3	0	14	$0\frac{3}{4}$
$1\frac{3}{4}$	0	2	11	0	5	10	0	8	9	0	11	8	0	14	7
$1\frac{7}{16}$	0	3	$0\frac{1}{4}$	0	6	$0\frac{1}{2}$	0	9	$0\frac{3}{4}$	0	12	1	0	15	$1\frac{1}{2}$
$1\frac{1}{2}$	0	3	$1\frac{1}{2}$	0	6	3	0	9	$4\frac{1}{2}$	0	12	6	0	15	$7\frac{1}{2}$
$1\frac{5}{8}$	0	3	$2\frac{1}{4}$	0	6	$5\frac{1}{2}$	0	9	$8\frac{1}{2}$	0	12	11	0	16	$1\frac{3}{4}$
2	0	3	4	0	6	8	0	10	0	0	13	4	0	16	8
$2\frac{1}{16}$	0	3	$5\frac{1}{4}$	0	6	$10\frac{1}{2}$	0	10	$3\frac{3}{4}$	0	13	9	0	17	$2\frac{1}{4}$
$2\frac{1}{8}$	0	3	$6\frac{1}{2}$	0	7	1	0	10	$7\frac{1}{2}$	0	14	2	0	17	$8\frac{1}{2}$
$2\frac{3}{16}$	0	3	$7\frac{3}{4}$	0	7	$3\frac{1}{2}$	0	10	$11\frac{1}{4}$	0	14	7	0	18	$2\frac{3}{4}$
$2\frac{1}{4}$	0	3	9	0	7	6	0	11	3	0	15	0	0	18	9
$2\frac{5}{16}$	0	3	$10\frac{1}{4}$	0	7	$8\frac{1}{2}$	0	11	$6\frac{3}{4}$	0	15	5	0	19	$3\frac{1}{4}$
$2\frac{3}{8}$	0	3	$11\frac{1}{2}$	0	7	11	0	11	$10\frac{1}{2}$	0	15	10	0	19	$9\frac{1}{2}$
$2\frac{7}{16}$	0	4	$0\frac{3}{4}$	0	8	$1\frac{1}{2}$	0	12	$2\frac{1}{4}$	0	16	3	1	0	$3\frac{3}{4}$
$2\frac{1}{2}$	0	4	2	0	8	4	0	12	6	0	16	8	1	0	10

To find the value of intermediate strengths not given in the table, for instance—
 86 per cent. at $1\frac{1}{16}$ per unit, find for 80 per cent. £3 5 7 $\frac{1}{2}$
 then for 6 „ „ 0 18 1 $\frac{1}{2}$

The sum gives value per ton of 86 „ £3 18 9

VALUE OF ALKALI PER TON—*Continued.*

Price per unit.	6 per cent.			7 per cent.			8 per cent.			9 per cent.			10 per cent.		
Pence.	£	s.	d.	£	s.	d.	£	s.	d.	£	s.	d.	£	s.	d.
$\frac{3}{4}$	0	7	6	0	8	9	0	10	0	0	11	3	0	12	6
$\frac{1}{8}$	0	8	$1\frac{1}{2}$	0	9	$5\frac{1}{2}$	0	10	10	0	12	$2\frac{1}{2}$	0	13	$6\frac{1}{2}$
$\frac{7}{8}$	0	8	9	0	10	$2\frac{1}{2}$	0	11	8	0	13	$1\frac{1}{2}$	0	14	7
$\frac{1}{8}$	0	9	$4\frac{1}{2}$	0	10	$11\frac{1}{2}$	0	12	6	0	14	$0\frac{1}{2}$	0	15	$7\frac{1}{2}$
1	0	10	0	0	11	8	0	13	4	0	15	0	0	16	8
$1\frac{1}{16}$	0	10	$7\frac{1}{2}$	0	12	$4\frac{1}{2}$	0	14	2	0	15	$11\frac{1}{2}$	0	17	$8\frac{1}{2}$
$1\frac{1}{8}$	0	11	3	0	13	$1\frac{1}{2}$	0	15	0	0	16	$10\frac{1}{2}$	0	18	9
$1\frac{3}{16}$	0	11	$10\frac{1}{2}$	0	13	$10\frac{1}{2}$	0	15	10	0	17	$9\frac{1}{2}$	0	19	$9\frac{1}{2}$
$1\frac{1}{4}$	0	12	6	0	14	7	0	16	8	0	18	9	1	0	10
$1\frac{5}{16}$	0	13	$1\frac{1}{2}$	0	15	$3\frac{1}{2}$	0	17	6	0	19	$8\frac{1}{2}$	1	1	$10\frac{1}{2}$
$1\frac{3}{8}$	0	13	9	0	16	$0\frac{1}{2}$	0	18	4	1	0	$7\frac{1}{2}$	1	2	11
$1\frac{7}{16}$	0	14	$4\frac{1}{2}$	0	16	$9\frac{1}{2}$	0	19	2	1	1	$6\frac{1}{2}$	1	3	$11\frac{1}{2}$
$1\frac{1}{2}$	0	15	0	0	17	6	1	0	0	1	2	6	1	5	0
$1\frac{9}{16}$	0	15	$7\frac{1}{2}$	0	18	$2\frac{1}{2}$	1	0	10	1	3	$5\frac{1}{2}$	1	6	$0\frac{1}{2}$
$1\frac{5}{8}$	0	16	3	0	18	$11\frac{1}{2}$	1	1	8	1	4	$4\frac{1}{2}$	1	7	1
$1\frac{11}{16}$	0	16	$10\frac{1}{2}$	0	19	$8\frac{1}{2}$	1	2	6	1	5	$3\frac{1}{2}$	1	8	$1\frac{1}{2}$
$1\frac{3}{4}$	0	17	6	1	0	5	1	3	4	1	6	3	1	9	2
$1\frac{7}{8}$	0	18	$1\frac{1}{2}$	1	1	$1\frac{1}{2}$	1	4	2	1	7	$2\frac{1}{2}$	1	10	$2\frac{1}{2}$
$1\frac{9}{8}$	0	18	9	1	1	$10\frac{1}{2}$	1	5	0	1	8	$1\frac{1}{2}$	1	11	3
$1\frac{11}{8}$	0	19	$4\frac{1}{2}$	1	2	$7\frac{1}{2}$	1	5	10	1	9	$0\frac{1}{2}$	1	12	$3\frac{1}{2}$
2	1	0	0	1	3	4	1	6	8	1	10	0	1	13	4
$2\frac{1}{16}$	1	0	$7\frac{1}{2}$	1	4	$0\frac{1}{2}$	1	7	6	1	10	$11\frac{1}{2}$	1	14	$4\frac{1}{2}$
$2\frac{1}{8}$	1	1	3	1	4	$9\frac{1}{2}$	1	8	4	1	11	$10\frac{1}{2}$	1	15	5
$2\frac{3}{16}$	1	1	$10\frac{1}{2}$	1	5	$6\frac{1}{2}$	1	9	2	1	12	$9\frac{1}{2}$	1	16	$5\frac{1}{2}$
$2\frac{1}{4}$	1	2	6	1	6	3	1	10	0	1	13	9	1	17	6
$2\frac{5}{16}$	1	3	$1\frac{1}{2}$	1	6	$11\frac{1}{2}$	1	10	10	1	14	$8\frac{1}{2}$	1	18	$6\frac{1}{2}$
$2\frac{3}{8}$	1	3	9	1	7	$8\frac{1}{2}$	1	11	8	1	15	$7\frac{1}{2}$	1	19	7
$2\frac{7}{16}$	1	4	$4\frac{1}{2}$	1	8	$5\frac{1}{2}$	1	12	6	1	16	$6\frac{1}{2}$	2	0	$7\frac{1}{2}$
$2\frac{1}{2}$	1	5	0	1	9	2	1	13	4	1	17	6	2	1	8

To find the value of intermediate strengths not given in the table, for instance—
 86 per cent. at $1\frac{1}{16}$ per unit, find for 80 per cent. £8 5 7 $\frac{1}{2}$
 then for 6 " 0 13 1 $\frac{1}{2}$

The sum gives value per ton of 86 £8 18 9

VALUE OF ALKALI PER TON—Continued.

Price per unit.	20 per cent.	80 per cent.	40 per cent.	48 per cent.	50 per cent.
Pence.	£ s. d.	£ s. d.	£ s. d.	£ s. d.	£ s. d.
$\frac{3}{4}$	1 5 0	1 17 6	2 10 0	3 0 0	3 2 6
$1\frac{1}{8}$	1 7 1	2 0 7 $\frac{1}{2}$	2 14 2	3 5 0	3 7 8 $\frac{1}{2}$
$\frac{7}{8}$	1 9 2	2 3 9	2 18 4	3 10 0	3 12 11
$1\frac{1}{8}$	1 11 3	2 6 10 $\frac{1}{2}$	3 2 6	3 15 0	3 18 1 $\frac{1}{2}$
1	1 13 4	2 10 0	3 6 8	4 0 0	4 3 4
$1\frac{1}{16}$	1 15 5	2 13 1 $\frac{1}{2}$	3 10 10	4 5 0	4 8 6 $\frac{1}{2}$
$1\frac{1}{4}$	1 17 6	2 16 3	3 15 0	4 10 0	4 13 9
$1\frac{3}{8}$	1 19 7	2 19 4 $\frac{1}{2}$	3 19 2	4 15 0	4 18 11 $\frac{1}{2}$
$1\frac{1}{2}$	2 1 8	3 2 6	4 3 4	5 0 0	5 4 2
$1\frac{5}{8}$	2 3 9	3 5 7 $\frac{1}{2}$	4 7 6	5 5 0	5 9 4 $\frac{1}{2}$
$1\frac{3}{4}$	2 5 10	3 8 9	4 11 8	5 10 0	5 14 7
$1\frac{7}{8}$	2 7 11	3 11 10 $\frac{1}{2}$	4 15 10	5 15 0	5 19 9 $\frac{1}{2}$
$1\frac{1}{2}$	2 10 0	3 15 0	5 0 0	6 0 0	6 5 0
$1\frac{9}{16}$	2 12 1	3 18 1 $\frac{1}{2}$	5 4 2	6 5 0	6 10 2 $\frac{1}{2}$
$1\frac{5}{8}$	2 14 2	4 1 3	5 8 4	6 10 0	6 15 5
$1\frac{1}{4}$	2 16 3	4 4 4 $\frac{1}{2}$	5 12 6	6 15 0	7 0 7 $\frac{1}{2}$
$1\frac{3}{4}$	2 18 4	4 7 6	5 16 8	7 0 0	7 5 10
$1\frac{7}{8}$	3 0 5	4 10 7 $\frac{1}{2}$	6 0 10	7 5 0	7 11 0 $\frac{1}{2}$
$1\frac{1}{2}$	3 2 6	4 13 9	6 5 0	7 10 0	7 16 3
$1\frac{5}{8}$	3 4 7	4 16 10 $\frac{1}{2}$	6 9 2	7 15 0	8 1 5 $\frac{1}{2}$
2	3 6 8	5 0 0	6 13 4	8 0 0	8 6 8
$2\frac{1}{16}$	3 8 9	5 3 1 $\frac{1}{2}$	6 17 6	8 5 0	8 11 10 $\frac{1}{2}$
$2\frac{1}{4}$	3 10 10	5 6 3	7 1 8	8 10 0	8 17 1
$2\frac{3}{8}$	3 12 11	5 9 4 $\frac{1}{2}$	7 5 10	8 15 0	9 2 3 $\frac{1}{2}$
$2\frac{1}{2}$	3 15 0	5 12 6	7 10 0	9 0 0	9 7 6
$2\frac{5}{8}$	3 17 1	5 15 7 $\frac{1}{2}$	7 14 2	9 5 0	9 12 8 $\frac{1}{2}$
$2\frac{3}{4}$	3 19 2	5 18 9	7 18 4	9 10 0	9 17 11
$2\frac{7}{8}$	4 1 3	6 1 10 $\frac{1}{2}$	8 2 6	9 15 0	10 3 1 $\frac{1}{2}$
$2\frac{1}{2}$	4 3 4	6 5 0	8 6 8	10 0 0	10 8 4

To find the value of intermediate strengths not given in the table, for instance—
 86 per cent. at $1\frac{1}{16}$ per unit, find for 80 per cent.....£3 5 7 $\frac{1}{2}$
 then for 6 ,, 0 18 1 $\frac{1}{2}$
 The sum gives value per ton of 86 ,,£3 18 9

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VALUE OF ALKALI PER TON—Continued.

Price per unit.	52 per cent.	54 per cent.	56 per cent.	57 per cent.	58 per cent.
Pence.	£ s. d.	£ s. d.	£ s. d.	£ s. d.	£ s. d.
$\frac{3}{4}$	3 5 0	3 7 6	3 10 0	3 11 3	3 12 6
$\frac{1}{2}$	3 10 5	3 13 1 $\frac{1}{2}$	3 15 10	3 17 2 $\frac{1}{2}$	3 18 6 $\frac{1}{2}$
$\frac{7}{8}$	3 15 10	3 18 9	4 1 8	4 3 1 $\frac{1}{2}$	4 4 7
$\frac{1}{8}$	4 1 3	4 4 4 $\frac{1}{2}$	4 7 6	4 9 0 $\frac{1}{2}$	4 10 7 $\frac{1}{2}$
1	4 6 8	4 10 0	4 13 4	4 15 0	4 16 8
$1\frac{1}{16}$	4 12 1	4 15 7 $\frac{1}{2}$	4 19 2	5 0 11 $\frac{1}{2}$	5 2 8 $\frac{1}{2}$
$1\frac{1}{8}$	4 17 6	5 1 3	5 5 0	5 6 10 $\frac{1}{2}$	5 8 9
$1\frac{3}{8}$	5 2 11	5 6 10 $\frac{1}{2}$	5 10 10	5 12 9 $\frac{1}{2}$	5 14 9 $\frac{1}{2}$
$1\frac{1}{4}$	5 8 4	5 12 6	5 16 8	5 18 9	6 0 10
$1\frac{5}{8}$	5 13 9	5 18 1 $\frac{1}{2}$	6 2 6	6 4 8 $\frac{1}{2}$	6 6 10 $\frac{1}{2}$
$1\frac{3}{4}$	5 19 2	6 3 9	6 8 4	6 10 7 $\frac{1}{2}$	6 12 11
$1\frac{7}{8}$	6 4 7	6 9 4 $\frac{1}{2}$	6 14 2	6 16 6 $\frac{1}{2}$	6 18 11 $\frac{1}{2}$
$1\frac{1}{2}$	6 10 0	6 15 0	7 0 0	7 2 6	7 5 0
$1\frac{9}{8}$	6 15 5	7 0 7 $\frac{1}{2}$	7 5 10	7 8 5 $\frac{1}{2}$	7 11 0 $\frac{1}{2}$
$1\frac{5}{4}$	7 0 10	7 6 3	7 11 8	7 14 4 $\frac{1}{2}$	7 17 1
$1\frac{11}{8}$	7 6 3	7 11 10 $\frac{1}{2}$	7 17 6	8 0 3 $\frac{1}{2}$	8 3 1 $\frac{1}{2}$
$1\frac{3}{2}$	7 11 8	7 17 6	8 3 4	8 6 3	8 9 2
$1\frac{7}{4}$	7 17 1	8 3 1 $\frac{1}{2}$	8 9 2	8 12 2 $\frac{1}{2}$	8 15 2 $\frac{1}{2}$
$1\frac{5}{2}$	8 2 6	8 8 9	8 15 0	8 18 1 $\frac{1}{2}$	9 1 3
$1\frac{9}{4}$	8 7 11	8 14 4 $\frac{1}{2}$	9 0 10	9 4 0 $\frac{1}{2}$	9 7 3 $\frac{1}{2}$
2	8 13 4	9 0 0	9 6 8	9 10 0	9 13 4
$2\frac{1}{16}$	8 18 9	9 5 7 $\frac{1}{2}$	9 12 6	9 15 11 $\frac{1}{2}$	9 19 4 $\frac{1}{2}$
$2\frac{1}{8}$	9 4 2	9 11 3	9 18 4	10 1 10 $\frac{1}{2}$	10 5 5
$2\frac{3}{8}$	9 9 7	9 16 10 $\frac{1}{2}$	10 4 2	10 7 9 $\frac{1}{2}$	10 11 5 $\frac{1}{2}$
$2\frac{1}{4}$	9 15 0	10 2 6	10 10 0	10 13 9	10 17 6
$2\frac{5}{8}$	10 0 5	10 8 1 $\frac{1}{2}$	10 15 10	10 19 8 $\frac{1}{2}$	11 3 6 $\frac{1}{2}$
$2\frac{3}{4}$	10 5 10	10 13 9	11 1 8	11 5 7 $\frac{1}{2}$	11 9 7
$2\frac{7}{8}$	10 11 3	10 19 4 $\frac{1}{2}$	11 7 6	11 11 6 $\frac{1}{2}$	11 15 7 $\frac{1}{2}$
$2\frac{1}{2}$	10 16 8	11 5 0	11 13 4	11 17 6	12 1 8

To find the value of intermediate strengths not given in the table, for instance—
 86 per cent. at $1\frac{1}{8}$ per unit, find for 80 per cent.....£8 5 7 $\frac{1}{2}$
 then for 6 " 0 13 1 $\frac{1}{2}$

The sum gives value per ton of 86 " £8 18 9

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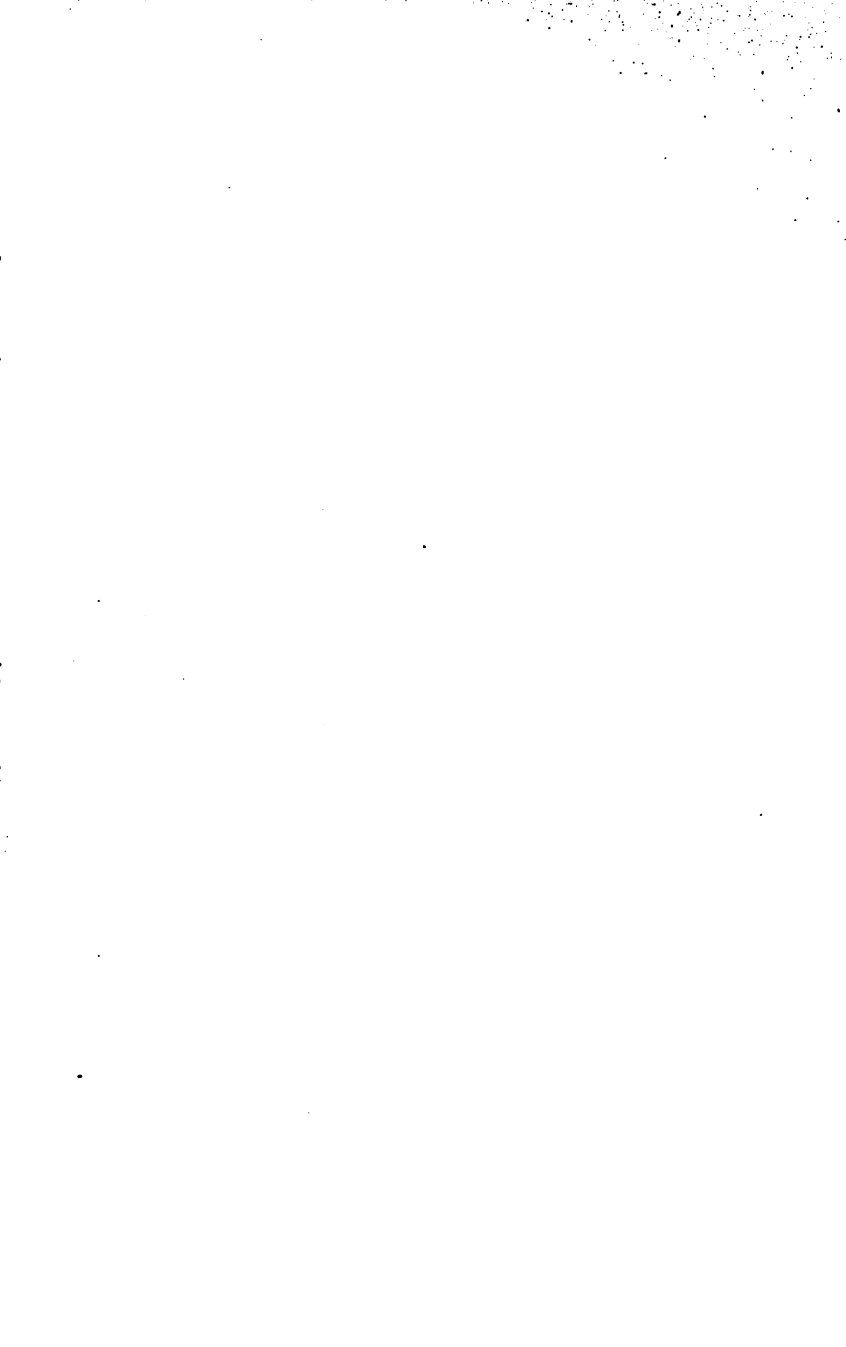
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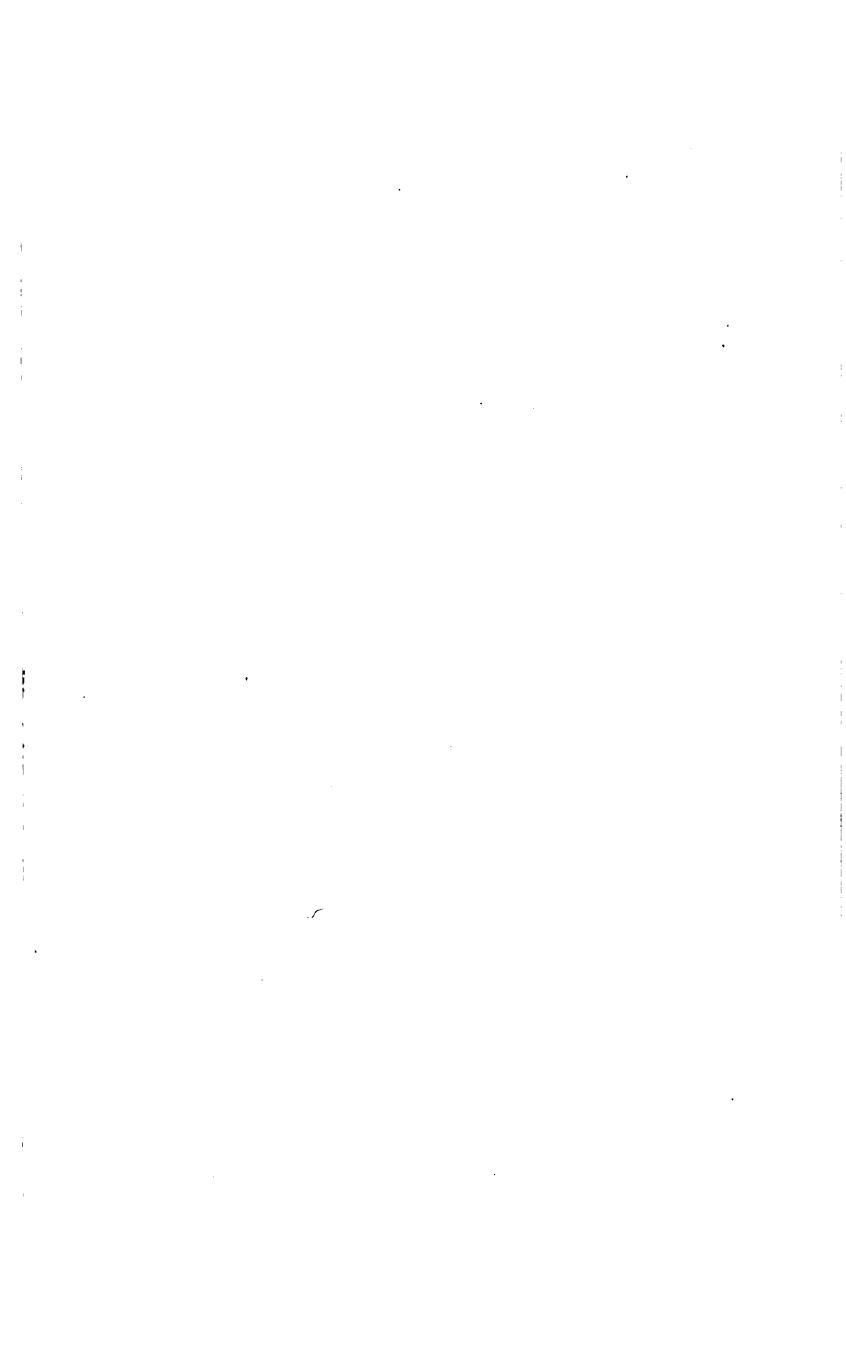
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